Impact to Underground Sources of Drinking Water and Domestic Wells from Production Well Stimulation and Completion Practices in the Pavillion, WY Field

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A - Regional and Local Geology

A.1 Structural Geology

The Pavillion Field is located in the west-central portion of the Wind River Basin (WRB) (Figure SI A1). The WRB is one of many structural and sedimentary basins that formed in the Rocky Mountain foreland (an elongate north-south structural depression flooded by a broad epicontinental sea referred to as the Western Interior Seaway) during the Laramide orogeny^{1,2} (Late Cretaceous through early Eocene). The WRB is fault-bounded by Laramide uplifts with Washakie Range, Owl Creek Mountains, and southern Bighorn Mountains to the north, the Wind River Range to the west, the Granite Mountains to the south, and Casper arch to the east^{1,4} (Figure SI A1).

Igneous and metamorphic rocks of Precambrian age comprise the core of the mountain ranges and underlie sedimentary rocks within the basin. Rocks from all geologic periods except Silurian age are present in the basin^{5,6}. Sedimentary strata dip 10°- 20° along the south and west margins of the WRB and are commonly vertical to overturned in the north and east margins of the WRB resulting in marked asymmetry with the deepest portion of the of the basin on the north and eastern margins³. The center part of the basin is filled with nearly horizontal fluvial and lacustrine Quaternary and Cenozoic Tertiary age sediment, overlying Paleozoic and Mesozoic age rocks. Surface deposits in the basin interior, where the Pavillion field lies, consists of Quaternary alluvium and coalluvum and lower Eocene rocks of the Wind River Formation³ in which over 1520 m of basin-fill strata was removed by post-lower Eocene erosion⁴. In the Pavillion area, the thicknesses of colluvial-alluvial deposits can be 6 m or more⁷.

Oil and gas wells in the WRB are generally associated with anticlines or more subtle closures, however, controls on confinement cannot be discerned for some basin-centered gas accumulations⁸. The Pavillion Field is situated on a structural closure that lies on the hanging wall of Circle Ridge/Maverick Springs thrust fault – one of three major northwest-trending thrust fault systems transecting the WRB^{3,9} (Figure SI A1). There is no publicly available information on the precise location of this fault in the Pavillion field. However, it appears to lie along the western portion of the field¹⁰.

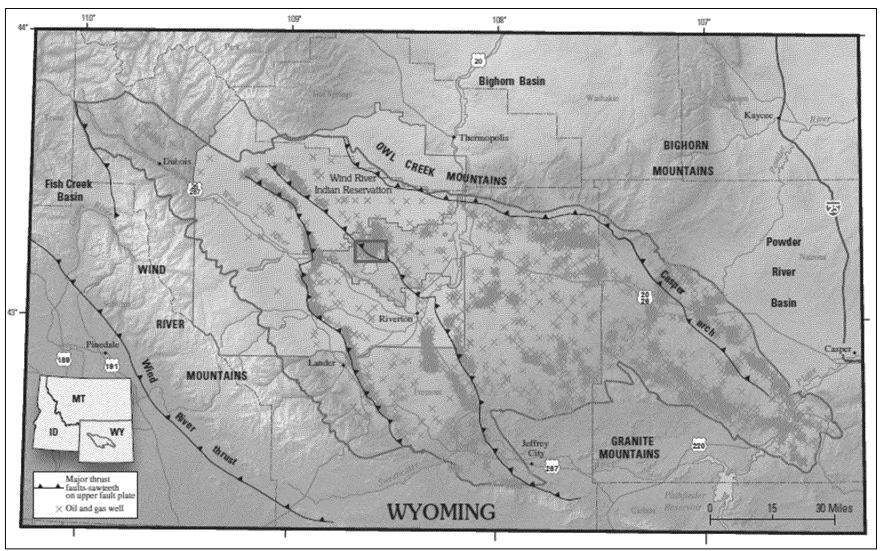


Figure SI A1. Boundaries of the Wind River Basin, identification of major faults, and the approximate location of the Pavillion Field (red square). Figure was modified from Nelson and Kibler⁸.

A.2 Identification of Source Rocks and Hydrocarbon Migration

Hydrocarbon production from the Pavillion Field is primarily gas from the Paleocene Fort Union and overlying Early Eocene Wind River Formation. However, oil has also been produced from a number of production wells in these formations, especially in western portion of the field in proximity to the suspected location of a fault. Source rocks for gas generation consist of marine rocks deposited from Early to Late Cretaceous time (~105-80 Ma) including the Thermopolis Shale, Mowry Shale, Belle Fourche Member of the Frontier Formation, and Cody Shale and non-marine source rocks deposited from Late Cretaceous to Paleocene time (~82-55 Ma) including coal and carbonaceous shale from the Mesaverde, Meeteetse, and lower member of the Fort Union Formation³ (Figure SI A2).

The source rock for oil production in the Pavillion Field is not explicitly identified in the literature. Oil was generated by source rocks in the Mowry Shale and lower shaly member of the Cody Shale throughout most of the deep basin but present day thermal maturities are too high for oil to be preserved in these source rocks except in marginal areas of the basin³. Oil generated by these source rocks may have migrated into shallow reservoirs but evidence is lacking³. The Waltman Shale Member of the Fort Union Formation is oil prone but absent at the Pavillion field^{4,8} or at its western boundary¹¹.

Light hydrocarbons from the Fort Union and Wind River Formations are isotopically similar and "dry." For example, methane (C_1) , $\delta^{13}C_1 = -38.04$ to -39.24% in Fort Union formation and $\delta^{13}C_1 = -39.24$ to -40.20% in Wind River Formation. The ratio of methane/methane to pentane $(C_1/C_{1-5}) = 0.95$ to 0.96 in Fort Union Formation and $C_1/C_{1-5} = 0.95$ and 0.96 in the Wind River Formation^{12,13}. The high level of thermal maturity of light hydrocarbons is incompatible with gas generation from these formations indicating extensive upward vertical migration from underlying mature and post-mature Upper Cretaceous source rocks¹³. Thermal maturities of coal beds in Fort Union are low indicating that any gas present is either of biogenic origin or is migrated thermogenic gas³.

In the Pavillion Field, light hydrocarbons are believed to have migrated and commingled in faulted and highly fractured zones along anticlines and structural noses^{3,13-15}. Light hydrocarbons migrated to the base of the Waltman Shale Member³ east of the Pavillion Field, and to Eocene Wind River Formation west of the pinchout of the Waltman Shale^{12,13} where the Pavillion field is present. As uplift and erosion proceeded in the Wind River Basin, ground water produced an alteration zone where microbial activity generated biogenic methane from source rocks and degraded ethane in preexisting gas accumulations³. Biodegradation of ethane has occurred at the Pavillion and East Riverton dome fields¹⁴.

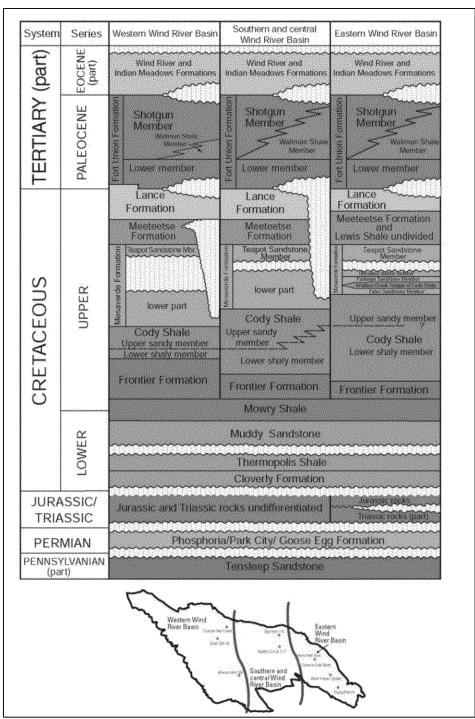


Figure SI A2. Generalized stratigraphic columns and correlations of Pennsylvanian through Eocene strata in the Wind River Basin, Wyoming. The Pavillion Field is located in the western portion of the Wind River Basin. From Johnson et al.³

Gas trapping in the Wind River and Fort Union Formations in the Pavillion field occurs in localized stratigraphic sandstone pinchouts on the crest and along flanks of a broad structural dome^{9,10,16}. A decrease in fracturing away from the crest of a fold rather than loss of gas saturation largely may control economic gas production³. During early development of the Pavillion field, Upper Cretaceous and Tertiary rocks were normally pressured (hydrostatic gradient) and had a low temperature gradient of 1.2°F/100 ft⁸. Cumulative water to gas ratios, measured in barrels (bbls) (1 bbl = 42 gallons = 159 liters) to million cubic feet (MMCF), for targeted production intervals in the Wind River and Fort Union are considered relatively low at 0.9 bbl/MMCF (n=84) and 2.4 bbl/MMCF (n=66), respectively⁸.

A.3 Lithology of the Fort Union Formation

The Fort Union Formation is divided into two general lithologic units. The lower unnamed member is characterized by conglomerates, white to gray fine- to coarse-grained, massive to cross-bedded standstone, interbedded with dark gray to black shale, claystone, and siltstone deposited under various fluvial depositional systems^{3,17-19}. The upper unit is divided into two laterally equivalent members – the Waltman Shale and the Shotgun members²⁰. The Waltman Shale is a lacustrine deposit in the central portion of the WRB that formed from an extensive body of water that developed in the basin during late Paleocene time¹¹. The Waltman Shale is absent or at its western boundary at the Pavillion field^{4,8,11}.

The Shotgun Member is a marginal lacustrine deposit that formed in fluvial and shoreline areas that expanded during the late Paleocene²⁰ and is dominated by siltstones, mudstones, carbonaceous shales, coals, and subordinated sandstones¹⁸. The Shotgun Member directly overlies and lithologically merges with the lower member in areas where the Waltman shale is absent^{11,19}. The thickness of the Fort Union is relatively unaffected by upwarping and downwarping indicating that downfolding occurred after deposition of the formation. Conglomerates and sandstones of the lower member of the Fort Union were initially targeted as producing zones in the Pavillion Field¹⁸.

Based on gamma ray, resistivity, and combined gamma ray-resistivity logs, Flores and Keighin¹⁸ identified four fluvial depositional systems in the lower member of the Fort Union Formation in the Pavillion Field. Type I reservoirs were characterized as stacked sandstone (up to ~ 18 m thick) with internal scours marked by lag conglomerates formed by low sinuosity side and mid-channel bars. Type II reservoirs were characterized as multistory sandstones (~4 to ~ 9 m thick) separated by siltstone and mudstone seal rocks (~1 to ~6 m thick) formed by low sinuosity cut and fill channels. Type III reservoirs were characterized as multistory sandstones (~2 to ~ 14 m thick) interbedded with siltstones and mudstones (~2 to ~12 m thick) formed by high sinuosity meander channels. Type IV reservoirs were

characterized as sandstones (up to ~ 6 m thick) within mudstones and siltstones formed by crevasse splays.

A.4 Lithology of the Wind River Formation

Fluvial deposition of the Wind River Formation occurred during a time of intense folding and uplift during the later stages of the Laramide orogeny^{6,11,20,21} resulting in considerable lithological variation of the formation throughout the WRB²⁰. Thickness of the Wind River Formation in the basin varies from 0 to about 1524 m⁶. Information from well completion reports and drilling logs indicates that in the Pavillion Field, thickness of the Wind River Formation ranges from 853 to 1228 m. The underlying Paleocene Fort Union Formation ranges in thickness from 762 to 914 m in the area¹⁸.

Keefer^{19,20} stated that, in general, two facies predominate in the Wind River Formation throughout the WRB – a coarse boulder facies representative of deposition along mountain slopes and a fine-grained commonly brightly varicolored facies representative of deposition farther out in the basin with gradation of these two facies in overlapping mountain and basin areas. However, depending on the transport power of ancient streams, coarse grained sandstone and conglomerate extend several miles in to the basin in channel deposits.

McGreevy et al.⁶ stated that in the Wind River Indian Reservation (WRIR) (an area directly west of the Pavillion Field), oil well logs and test drilling indicated: (1) an upper fine-grained sequence at the surface in most of the eastern part of the reservation consisting primarily of gray and green siltstone, shale, and sandstone with numerous sheet and channel deposits of brown siltstone and sandstone with a maximum thickness of about 244 m in most of the area; (2) a sequence containing many coarse-grained, well sorted, loosely cemented, very porous, largely arkostic sandstone and conglomerated beds of thickness of ~ 305 m but thinning to the northeast part of the WRIR; and (3) a lower sequence consisting of fine-grained brown, maroon, red, and gray siltstone and shale with some sandstone of thickness of several thousand feet which intertongues with the coarse-grained sequence toward the south end of the WRIR.

A continuous sandstone unit, termed the Basal Wind River unit, lies at the base of the Wind River Formation in the Pavillion Field^{9,10}. This unit appears frequently in drilling and well completion reports. The continuity of this unit contrasts with substantial vertical and lateral stratigraphic variation in sandstone units over short distances in the Pavillion area^{9,10} and throughout the Wind River Formation in general^{18,22} precluding mapping of these units using conventional borehole log techniques. Sandstone units are generally characterized as lenticular, discontinuous, and separated by confining shale, mudstone, and siltstone units⁶.

Sandstone lenses in the Wind River Formation in the Pavillion field are reported to be generally fine to very fine grained, well sorted, have porosity in the range of 4 to 28 percent and permeability in the range of 0.1 to 300 millidarcies (md)⁹. Referring to development in 14 gas wells and 8 dry holes in the Wind River and Fort Union Formations, Single⁹ stated that on average 75 sandstone units (varying in thickness between ~1 to 21 m) were penetrated in each well of which 6 to 20 units were gas productive and the remaining had limited porosity and/or permeability, or were "water bearing". Drilling in the Pavillion field is complicated by the presence of water sensitive shales and petrophysical evaluation is complicated due to the presence of fresh water and pore-filling clays⁹.

The central part of the basin, is characterized by stream-valley fill and broad flood plains and that the presence of large quantities of overbank mudstones and near linear channel-sandstone ridges suggest that meandering streams of low sinuosity were dominant during deposition of the Wind River Formation²¹. The Eocene Wind River appears to have flowed directly through an area that is now the Pavillion Field in the vicinity of production well Tribal Unit 14X-11²¹. Maximum intervals of continuous sandstone deposits are greatest near the course of the Eocene Wind River where channel sandstone bodies can be as much as 40 meters thick, but most are much thinner²¹.

A.5 Lysite and Lost Cabin Members of the Wind River Formation

In the eastern and northeastern margins of the WRB (north and east of the Pavillion field), the Wind River Formation has been divided into the Lysite and overlying Lost Cabin Member based on lithological and faunal differences^{19,20}. Faunal distinction was largely based on the presence of the genus *Lambdotherium* in the Lost Cabin beds and its absence in Lysite beds²⁰. In the northeastern portion of the WRB, the Lysite Member consists of yellow to brown sandstone and conglomerate interbedded with red, gray, and greenish-gray sandy claystone and siltstone²⁰. The Lost Cabin Member consists of gray, yellow, and brown sandstone with locally prominent beds of conglomerate alternating with violet, red, purple, gray, and green sandy clayey sandstone²⁰. Both members contain an abundance of fine-grained strata¹⁹.

One of the primary differences between these two members is the composition of conglomerates. Conglomerate in the Lost Cabin Member contains abundant Precambrian rock fragments of granite and gneiss¹⁹. Conglomerate in the Lysite Member is derived almost exclusively from Paleozoic formations¹⁹ and contains an abundance of limestone, dolomite, and chert fragments²⁰. In the central part of the WRB (where the Pavillion Field is located), there is no sample or electric log basis to separate the Wind River Formation into Lysite and Lost Cabin Members²⁰. Throughout the WRB, the name Wind River Formation is applied to all lower Eocene rocks, including the Indian Meadows Formation and the Lost Cabin and Lysite Members of the Wind River Formation because there are no viable criteria for distinguishing individual members of the Wind River Formation from sample and well log data^{11,19,20}.

Stephens²³ and Itasca Denver Inc.²⁴ state that the Wind River Formation in the Pavillion field can be divided into the Lost Cabin member and underlying Lysite member and that the former is a source of potable water while the later has total dissolved solids (TDS) levels exceeding 10,000 mg/L. They state that EPA's monitoring well MW01 was completed in the Lower Lost Cabin member, and MW02 was completed in the Upper Lysite Member where elevated chloride was detected. However, neither Stephens²³ nor Itasca Denver Inc.²⁴ provide any justification (e.g., faunal or lithologic) for identification of these units outside established geographic areas in the WRB.

In available lithologic logs in the Pavillion Field, limestone and dolomite fragments characteristic of the Lysite member were not identified at Tribal 1-21, Tribal 1-22, Taylor Patented 1, Shell 33X-10, Mae H. Rhodes 1, Runners Herford 1, Roland Patented 34-13, Ocean Lake Tribal 1-15, John K. Coolidge 1-4, Unit 12-3, Govt Ocean Lake 1, Doles Unit 44-15, Tribal 21-9, and Tribal Pavillion 14-2 at or below the depth of MW02. Chert fragments were identified at 856 m below ground surface (bgs) at Shell 33X-10 and at 1036 m bgs at Taylor Patented 1.

Also, neither Stephens²³ nor Itasca Denver Inc.²⁴ provide references or documentation that, even where present, the Lysite member contains TDS levels exceeding 10,000 mg/L. In an evaluation of alternative water supply options for residents in the Pavillion field, Gores and Associates²⁵ identified three domestic wells of similar depth of MW02 in the immediate vicinity of the Pavillion field at 274, 305, and 322 m bgs with associated TDS concentrations of 631, 590 (775 duplicate), and 607 mg/L TDS respectively. Also, USGS reports (McGreevy et al.⁶, Plafcan et al.²⁶, and Daddow et al.⁵) relevant to the Pavillion area indicate no instance of TDS levels exceeding 10,000 mg/L in the Wind River Formation. Plafcan et al.²⁶ identified a water supply well at 674 m bgs having a TDS concentration of 1190 mg/L. A.6 EPA Lithologic Cross-Section through Pavillion Field

EPA²⁷ used borehole geophysical logs from 32 production wells to develop a lithologic cross-section in the vicinity of MW01 and MW02. Depending upon the specific production well, various combinations of natural gamma, resistivity, self-potential, density, and neutron porosity logs were utilized. No gradational/intermediate values between shale and sandstone (e.g. 80% shale, 20% sandstone) were used although they are known to exist throughout the Wind River Formation. This designation was maintained for consistency for near surface deposits where fine-, medium-, and coarse-grained sandstones could be differentiated from driller's logs. It was generally clear from the various logs whether a specific interval contained sandstone or shale, but not where each layer started or ended. Thus, assignment of boundaries was subjective. Each sandstone or shale layer was represented as having at least one meter in thickness since log resolution was insufficient to discern individual layers less than this resolution.

Data was used to populate a three-dimensional lithology model using a commercial software package Rockware 15. A lithologic cross-section (Figure SI A4) developed along a transect (Figure SI A3) represents a slice taken through this 3D model. In general, lithology was highly variable and difficult to correlate from borehole to borehole, even for boreholes in close proximity to one another consistent with the experience of others (e.g., Osiensky et al.²²). However, it is apparent that there are no laterally continuous confining layers above depths of well stimulation (Figure SI A4). Since the majority of geophysical logs from the oil and gas wells were run after installation of surface casing, the shallow lithology structure (upper 150-200 meters) in the model was dominated by information from the two EPA installed monitoring wells. Thus, the apparent existence of continuous shale units near the surface may be a result of insufficient data rather than physical reality.

The aspect ratio (length versus width) of sandstone lenses cannot be discerned from available data. Itasca Denver Inc.²⁴ used exposures from Upper Jurassic Salt Wash Sandstone Member of the Morrison Formation in the Henry Mountains area of southern Utah investigated by Robinson and McCabea²⁸ to define the aspect (length versus width) ratios of sandstone bodies in the Paleocene Fort Union and Eocene Wind River Formations. Justification for this comparison was not provided.

A plot of the entire Pavillion Field is provided in Figure SI A5.

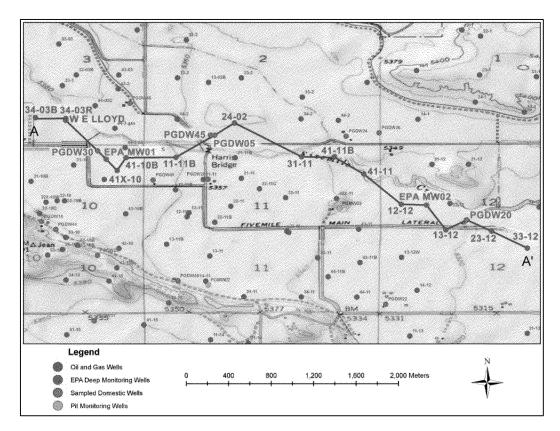


Figure SI A3. Map illustrating transect used to develop a lithologic cross section across the Pavillion Field. From EPA²⁷

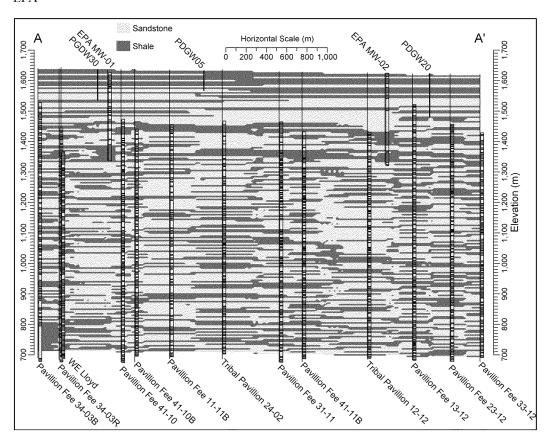


Figure SI A4. Lithologic cross-section along transect illustrating undifferentiated sandstone and shale units. From EPA²⁷

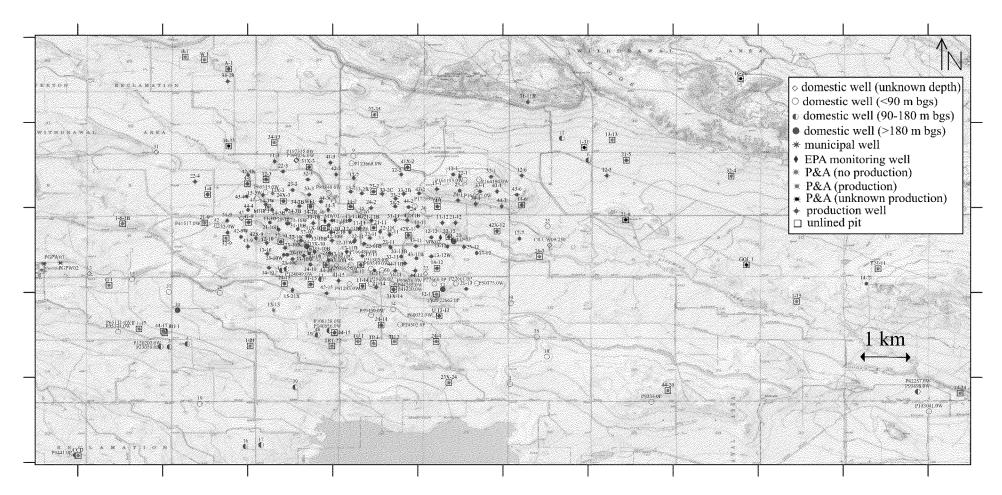


Figure SI A5. Pavillion Field plot illustrating locations of production wells, domestic wells, EPA monitoring wells (MW01 and MW02), and unlined pits. Domestic wells sampled by EPA identified by last two digits of PGDWXX series. Unsampled domestic wells having a Wyoming State Engineer's Office (SEO) permit number identified with the prefix "P." Unsampled domestic wells lacking SEO permits not identified. Depths of domestic well provided in Table SI B1. Full names of production wells, abbreviated here, are provided in Table SI C1. Locations of unlined pits are approximated by locations of associated production wells.

B – Locations, Depths, and Major Ion Concentrations of Domestic Wells in and Around the Pavillion Field

Table SI B1. Location and depth of domestic wells in and surrounding the Pavillion well field. Domestic wells with prefix PGDWXX were sampled by EPA. State Engineers Office (SEO) permit provided when available. PGDW01 and PGDW02 are municipal wells PGPW01 and PGPW02. Information compiled from EPA²⁷, EPA^{29,30}, Wyoming Oil and Gas Conservation Commission (WOGCC)^{31,32}and Gores and Associates²⁵

•	8					_
SEO Permit Number	EPA Well	Latitude	Longitude	Ground Elevation (m AMSL)	Well Depth (m bgs)	Completion Date
≅ Z	= =	ן ב		5EE	> 5	Öä
?	PGPW01/PGDW07 4				154.2 ?	
?	PGPW02/PGDW08 4		6840515 1641.0		157.0 ?	
?	PGDW01	43.2185	-108.5783	1610.0	?	?
?	PGDW02		08.5783117 1629		15.2	?
?	PGDW03		08.6584107 1629		137.2 ?	
? D22161 0W	PGDW04		08.6541901 1638		134.1 ?	02/02/1076
P32161.0W	PGDW05 PGDW06		08.6126556 1632 08.5599211 1663		64.0 115.8 ?	02/02/1976
?	PGDW09		08.615144 1635.6		9.1	?
?	PGDW10		8.6565018 1633.		225.6?	•
?	PGDW11		08.6228628 1636		220.0	?
?	PGDW12		08.5661502 1652		115.8 ?	
?	PGDW13	43.2444467 -10	8.6772771 1642.0	5	?	?
No permit on file I	PGDW14	43.25154027 -		642.3	57.9	?
?	PGDW15		08.6671791 1606		30.5	?
?	PGDW16		08.6405183 1610		164.6 ?	
?	PGDW17		08.6368713 1615		152.4 ?	
?	PGDW18		08.569651 1612.		67.1	?
?	PGDW19		08.651274 1622.		19.8	?
No permit on file I		43.25230026 -		624.0	140.2 ?	
No permit on file I		43.25437	-108.58919	1623.0	185.9 ?	?
<u> </u>	PGDW22		8.598175 1627.0			•
P24508.0P	PGDW23		8.6225891 1656.9		53.3 30.5	12/31/1964 ?
?	PGDW24 PGDW25		08.6015059 1622 08.5694867 1643		24.4	?
?	PGDW25 PGDW26		08.6132115 1649		19.8	?
?	PGDW28		08.6465688 1612		25.9	?
?	PGDW29		08.6288449 1634		121.9 ?	:
No permit on file I		43.25753	-108.62258	1637.1	79.2	?
?	PGDW31		08.6615302 1624		?	?
P64110.0W	PGDW32		08.5941391 1624		205.7 5/2	4/1983
P22662.0P	PGDW33		08.5964146 1626		9.1	12/31/1934
?	PGDW34		08.6058086 1634		30.5	?
?	PGDW35		08.6241763 1630		88.4	?
?	PGDW36	43.25905726 -	08.5987059 1641	.0	30.5	?
?	PGDW37		08.6585376 1615	.4	24.4	?
?	PGDW38		8.572037 1610.9		48.8	?
?	PGDW39		08.5781708 1615		17.4	?
?	PGDW40		08.6198273 1638		67.1	?
P66345.0W	PGDW41	43.262146	-108.6378479 16		21.3	1/31/1984
P41517.0W	PGDW42	43.25574493 -			61.0	11/29/1977
? P24506 OP	PGDW43	43.25749207 -		1645.0	?	?
P24506.0P	PGDW44		08.6261292 1645		228.6 12/	
No permit on file I	PGDW45 PGDW46	43.25888062 -	08.6130142 1 08.6157684 1638	632.5	30.5 14.6	?
?	PGDW46 PGDW47		08.615/684 1638		14.6	· ·
?	PGDW47		08.6235733 1633.	-2	115.8 ?	
No permit on file I		43.25505829 -		637.7	15.8 7	?
P166481.0W	PGDW50	43.2453	-108.6085	1633.1	61.0	4/7/2005
CR UW09/250	None	43.25114	-108.56899	1614.4	?	8/19/1977
P108128.0W	None	43.23104	-108.62085	1626.1	115.5 11/	
P120203.0W	None	43.22725	-108.66048	1628.2	137.2 11/	
P123668.0W	None	43.27042	-108.61556	1638.9	18.3	3/6/2000
P124049.0W	None	43.24552	-108.63087	1639.2	147.5 3/	6/2000
P146856.0W	None	43.23104	-108.62085	1626.1	115.8 9	/5/2002
P164192.0W	None	43.26372	-108.5862	1649.0	24.4	12/6/2004
P164193.0W	None	43.26653	-108.589	1654.1	30.5	12/6/2004

SEO Permit Number	EPA Well Identification	Latitude	Longitude	Ground Elevation (m AMSL)	Well Depth (m bgs)	Completion Date
P164194.0W	None	43.26658	-108.5856	1654.1	31.2	12/6/2004
P166480.0W	None	43.24909	-108.6163	1633.1	?	4/7/2005
P172899.0W P183041.0W	None None	43.26029 43.21207	-108.60075 -108.47977	1631.0 1567.9	30.5 73.2	10/19/2005 8/1/2007
P197335.0W	None	43.27103	-108.62861	1645.9	?	1/27/2012
P197336.0W	None	43.27115	-108.62854	1645.9	?	1/27/2012
P200885.0W	None	43.24642	-108.61915	1657.0	?	8/16/2013
P22660.0P	None	43.24208	-108.59609	1624.9	53.3	9/30/1938
P22661.0P P22662.0P	None None	43.24212 43.23844	-108.5911 -108.59611	1622.1 1625.5	14.6 9.1	8/31/1947 12/31/1934
P23056.0P	None	43.22725	-108.59011	1623.3	19.8	1/4/1960
P24502.0P	None	43.23248	-108.60418	1628.9	54.9	12/31/1942
P24506.0P	None	43.24918	-108.62593	1658.4	228.6 12	/31/1932
P24508.0P	None	43.2492	-108.62099	1637.1	53.3	12/31/1964
P29496.0P P30217.0W	None None	43.24198 43.24311	-108.61107 -108.62275	1633.1 1633.1	39.6 106.7 6/	3/31/1975 18/1975
P30217.0W P31805.0W	None	43.24562	-108.62273	1633.1	30.5	18/19/3
P34936.0W	None	43.24311	-108.62275	1633.1	106.7 9/	14/1976
P41320.0W	None	43.24201	-108.60608	1642.9	30.5	12/19/1977
P41517.0W	None	43.25628	-108.6507	1644.1	61.0	11/29/1977
P44255.0W P50375.0W	None	43.24201	-108.60608	1642.9	68.6 30.5	7/18/1978
P59499.0W	None None	43.24216 43.23471	-108.58612 -108.611	1618.0 1622.1	33.5	10/15/1979 2/3/1982
P60032.0W	None	43.2348	-108.59614	1618.0	26.2	3/23/1982
P65111.0W	None	43.23078	-108.67048	1645.0	27.4	8/3/1983
P66345.0W	None	43.26365	-108.6358	1642.9	21.3	1/31/1984
P69549.0W	None	43.24562	-108.61107	1633.1	30.5	2/25/1985
P82257.0W P89840.0W	None None	43.21668 43.26343	-108.48244 -108.62097	1571.8 1639.5	91.4 65.5	4/20/1990 9/17/1992
P91293.0W	None	43.24195	-108.61606	1631.0	3.0	4/5/1993
P9334.0P	None	43.21429	-108.54506	1625.5	6.1	12/31/1935
P93498.0W	None	43.21668	-108.48244	1571.8	69.5	11/15/1993
P9441.0P	None	43.20178	-108.68044	1634.9	177.4 1/1	/1944
P95171.0W P99671.0W	None None	43.23078 43.24201	-108.67048 -108.60608	1645.0 1643.0	25.9 16.7	5/9/1994 6/28/1995
P14914P	None	?	?	?	39.6	?
P98757W	None	?	?	1670.0	156.1	?
P58929W	None	?	?	1652.0	17.4	?
P34345W	None	?	?	1667.9	150.9	?
P59104W P24507P	None None	?	?	1667.9 1647.1	152.4 ? 228.6 ?	
P97501W	None	?	?	1624.0	?	?
P30217W	None	?	?	?	106.7 ?	
P182983W	None	?	?	1638.6	231.6?	
P46362W	None	?	?	1642.3	54.9	?
P62641W P53567W	None None	?	?	1662.7 1652.0	208.8 ? 42.7	?
P25636W	None	?	?	1632.0	12.5	?
P110443	None	?	?	1633.7	127.1 ?	
P28496W	None	?	?	1613.3	11.0	?
P26200W	None	?	?	1603.2	88.4	?
P40603W P76475W	None None	?	?	1619.1 1621.5	12.2 97.5	?
P14548P	None	?	?	1615.4	18.3	?
P30162W	None	?	?	1645.9	61.0	?
P32163W	None	?	?	1639.8	114.3 ?	
P9941P	None	?	?	1637.1	177.4 ?	
P116598W P25011W	None None	?	?	1629.8 1627.6	143.3 ? 88.4	?
P177246W	None	?	?	1611.5	304.8 ?	
P190223W	None	?	?	1618.2	321.6 ?	
P191733W	None	?	?	1606.9	274.3 ?	
Unidentified (16	None	?	9	?	9	?

Table SI B2. Major ion concentrations in water sampled from domestic wells.

Well Name	Date pH	SC (µS/cm)	Alkalinity (mg/L)	Na (mg/L)	K (mg/L)	Ca (mg/L)	Mg (mg/L)	Br (mg/L)	Cl (mg/L)	SO4 (mg/L)	F (mg/L)	NO ₃ (N) (mg/L)	Fe (mg/L)	TDS (mg/L)	Source
PGDW05	Mar-09 9 02 956		93.3 192		0.286 3.6	0 127 N	IN A		17.0 29	5	0.9		0.187		EPA ²⁹
GD WOS	Jan-10 8.22 900		88.4 189		<5.0	3 33 <	50	NM	16.5 2	87	0.9	<0.5 <0.3	0.167		EPA ³⁰
	Apr-11 9 06 820			190	<5.0 0.24	3.35.0	08	NM	16.8 2	76	1.2	<0.014 0.	124		EPA ²⁷
	Apr-12 9 30 837		91	190	0.47	3.33 < 3.35 0 3.17 0	07	<1.00 10	5.8	308	1.2 0.90	0.02	0.0666 124 <0.03		EPA ³³
	Jun-14 9.29 878		91 92 97	220	0.47 <0.1	3.4 <0	5	0.093 19)	310	1.0	< 0.005 < 0	D.1	560 W	YDEO ³⁴
	Aug-14 9.09 969		97	170	0.37	3.5 0.1	1	0.099 18	}	300	0.92	<0.005 <0.005 0.	034	560 W	YDEQ ³⁴
GDW06	Mar-09 10.2 1262		34.9 249)	0.344 7.1			NM	31.0 48	85	1.3	<0.5	NM		EPA ²⁹
GDW09	Mar-09 8 35 1128		254	233	2.05	16.64	.14	NM	10.5 2'	79	2.4	3.2	NM		EPA ²⁹
GDW11	Mar-09 7 17 3400		312	423	5.53	363 80	9	NM	15.3 1'	780 0.2		1.3	NM		EPA ²⁹
PGDW12	Mar-09 10.04 1344		37.1 250	\$	0.567 7.7	8 0.424		NM	30.8 49	7	1.5	< 0.5	0.695		EPA ²⁹
GDW14	Mar-09 7 85 2990		159	690	4.51	154 18	1.1	NM	26.1 18 23.7 1	320 0.4		0.7	NM <0.019 <0.1		EPA ²⁹
	Apr-11 7 73 3473	[156	753 820	3.52 3.5	154 18	6	NM	23.7 1	60 <0	.05 0.36		< 0.019		EPA^{27}
	Jun-14 7.65 3920	[160		3.5	170 19		0.29 29		2000 <	0.40 0.4	4	< 0.1	2930 V	VYDEQ ³⁴
	Aug-14 7.62 4110		160	700	4.4	140 18		< 0.15 28	}	1900	0.25	0.38	< 0.1	2910 V	VYDEQ 34
GDW20	Mar-09 8 76 2005		70.2 520	· · · ·	1.01	79.3 9		NM		70 0.8		<0.5	0.0342		EPA ²⁹
	Jan-10 8.89 2690	[67.9 550	j	< 5.0	71.78	.14	NM	32.6	1270 0.8		<0.3 <0.3 0.35 <0.03 0.1	0.300		EPA ³⁰
	Oct-10 8.85 2940		54	562	1.05	71.98	.12	NM	33	1320 0.9	0	0.35	0.221		EPA^{27}
	Apr-11 8 59 2430		102	562 520	0.780 63		6.86	NM NM NM <1.00 32	22.9 1	50 1.3	}	< 0.03 0.1	В7		EPA^{27}
	Apr-12 8 89 2429]	66 83	491 630	1.64	57.9 5 78	.93	<1.00 32	2.3 1	30 0.94]	U.U/3 \U.	03		EPA^{33}
	Apr-12 8 89 2429 Jun-14 8 84 2880		83	630	0.72	78	7.6	<0.15 33	5	1300	0.92	<0.03 0.1	2		/YDEQ ³⁴
	Aug-14 8 75 2980		83	520	0.91	82	8	0.13 35		1300 0.8	9	< 0.01 0.0	В8	2050 V	/YDEQ ³⁴
D02	Oct-10 8.94 1175		78	313	0.57	25.2 1	.43	NM	20.1 69	8	2.28	< 0.10 0.0	23		EPA ³⁰
	Jun-14 8.29 3610]	78 56 62	680	1.8	140 21		< 0.15 38	}	1700 1	.5	< 0.25	0.079 0076 2560 V	2500 V	VYDEQ ³⁴
	Aug-14 NM	NM	62	630	1.6	130 22	2	<0.15 3	7	1700 1.5	\$		0076 2560 V	VYDEQ	34
GDW22	Mar-09 6 93 6180		332	837	8.99	416 12	26	NM	79.92	720 < 0.2	<u> </u>	43.6	NM <0.1		EPA ²⁹
	Jan-10 7.06 4230		337	908	5.83	397 13		NM	74.6 2			40.7	< 0.1		E PA ³⁰
GDW23	Mar-09 9 43 816		61.4 203	\$	0.278 6.5	1 0.070	NM		19.8 30	55	1.2	< 0.5	NM		EPA ²⁹
	Jan-10 9.72 780 Apr-11 9 07 959		54.2 19	<u> </u>	<5.0 · 0.31 0.61	5.82 <	5.0	· NM NM <1.00 19	19.7-3	68	1.5	<0.3 <0.03 <0.	< 0.100		EPA^{30}
	Apr-11 9 07 959	<u> </u>	72	208	0.31	6.7 0.1 7.19 0	7	NM	19.9 30	55	1.6	<0.03 <0.	.019		EPA^{27}
	Apr-12 9 13 996		54.2 194 72 65 57	208 223 240	0.61	7.19 0	.09	<1.00 19) .0	397	0.98 1.5	0.05 0.03	NM <0.100 019 <0.03 <0.1	650 W	EPA ³³
	Jun-14 9.28 1110		57	240	0.11	6.2 <0		0.14 22		400		0.03	< 0.1	650 W	YDEQ 33
	Aug-14 9.09 1040		60	200	0.37		83 0.11 21			380	1.5	<0.005 <	₽.0076 650 V	VYDEQ	33
GDW24	Mar-09 7 65 4700		165	938	7.02	327 13		NM		200 0.6		<0.5	0.995		EPA 29
GDW25	Mar-09 8 68 972		205	249	1.05	10.9 1	.05	NM	8.4 35	,	4.1	<0.5	0.0517		EPA ²⁹
~~~~	Jan-10 7.94 1511		295	269	<5.0	70.1 9		NM	9.5 44	1	<0.2	1.7	< 0.100		EPA ³⁰
GDW26	Mar-09 7 13 2390		337	220	6.8	364 57		NM		240 0.7		1.5	NM		EPA ²⁹
CDWGG	Apr-11 6 95 2390	1170	196	232	5.15	334 56		NM	13.2 1		0.5	1.37	<0.019		EPA ²⁷
GDW28	Mar-09 8.3	1170	258	239	2.15	40.6 1		NM	16.7 29		0.5	3.7	NM		EPA ²⁹
GDW30	Mar-09 9 6	902	95.7 210 94.0 19:	<u> </u>	0.294 4.2	9 0.125 4.05 <	PM		16.3 33		0.9 0.9	<0.5 <0.3	0.117		EPA ²⁹ EPA ³⁰
	Jan-10 9.39 967				<5.0			NM	15.5 3	33		0.23	0.0441		
	Oct-10 9.24 1068		78.0 20		0.2 0.29	4.3 0.1	μ. 	NM	15.2 3	<u>'</u> /	1.0	0.23	<0.019 42 <0.03 <0.1		EPA ²⁷
	Apr-11 8 92 938		82 91 97 96	210 213 240 240	0.29	4.5 0.0		NM	16.1 32		1.1	<0.03 0.0	# <i>Z</i>		EPA ²⁷
	Apr-12 8 98 954		91	213	0.55	4.42 0	.l	<1.00 10	p.1 3	37	1.05	0.02	<0.03	620 117	EPA ³³
	Jun-14 9.19 1040		97	240	0.18	4.3 <0		0.11 17	l <del>,</del>	360	0.91	R	<0.1	630 W	Y DEQ
	Aug-14 8.84 1040	l · · ·	96	240	0.33	4.5 0.1	1	0.080 17	· ·	340	0.87	<0.005 <	0.0076 640 V	VYDEQ	34

Name			SC (µS/cm)	mity ) O30	(T/Bi	yL)	g/L)	ng/L)	g/L)	g/L)	SO4 (mg/L)	(F)	<b>2</b> c	g/L)	TDS (mg/L)	
Well Name	Date	Hd	SC (n	Alkalinity (mg/L) (CaCO3)	Na (mg/L)	K (mg/L)	Ca (mg/L)	Mg (mg/L)	Br (mg/L)	CI (mg/L)	SO4 (	F (mg/L)	NO ₃ (N) (mg/L)	Fe (mg/L)	TDS (	Source
PGDW31	Mar-09 8	.6	2006	82.5 435		0.901 31.	2 0.843 1	VМ		13.3 10	030 0.4		0.5	NM		EPA ²⁹
PGDW32	Mar-09 1			34.1 199		0.267 7.1	5 0.017 1	N	M	21.8 3		2.3	<0.5	0.412		EPA ²⁹
	Jan-10 9.	87 1018		31.5 193		<5.0 0.09	6.89 <		NM	21.4	368	2.4	<0.3 <0.03 0.0	0.125		EPA ³⁰
	Apr-11 9	3	885	46 30	198 230	0.09	7.2 0.0		NM	18.8 36		2	< 0.03 0.0	24		EPA ²⁷
	Jun-149.		<b></b>			<0.1		02 < 0.03 2	4 		400	2.5	<0.005 <	).1 	620 W	YDEQ 34
DCDW22	Aug-14 9	.88 1120		34	190	0.42	8	0.038 0.0		22.0.2	380	2.3	<0.005 <	0.0076 640 V	VYDEQ	54 FD 4 29
PGDW33	Mar-09 7 Jun-14 7.	05 1860	<b></b>	276 310	178 150	4.99 3.8 3	228 40 200 39	<u> </u>	NM <0.03 20	23.0 20	90 0.2 700	0.65	2.1 3.2	NM 0.087	1250 V	EPA ²⁹ VYDEQ ³⁴
	Jun-14 /. Aug-14 7		<del> </del>	260	160	3.8	150 27	}	0.043 18	<u> </u>	590	0.63	2.0	<0.0076 1		
PGDW34	Mar-09 7			373	786	7.4	325 11	3	NM	28	670	0.58	3.5	NM	100 W 11	EPA ²⁹
PGDW35	Mar-09 8			84.0 587	700	1.09	118 1.	F	NM		510 0.3	0.5	0.5	1.10		EPA ²⁹
PGDW36	Mar-09 7			232	41.7 2.5		89.5 2	8.9	NM	3.2 19:		1.0	1.2	NM		EPA ²⁹
PGDW37	Mar-09 8			342	187	0.887 12.	1 1.3		NM	8.7 89.		1,0	1.2	NM		EPA ²⁹
PGDW39	Jan-10 7.	79 6410		129	1110 5.2		389 14	7	NM	52.9 36	540 0.3		< 0.3	0.33		EPA ³⁰
PGDW40	Jan-10 9.	06 1229		86.3 244		< 5.0	6.57 <	5.0	NM	13.1 42	26	<0.2	<0.3	1.26		EPA ³⁰
PGDW41A Jur				320	1400 6.2		670 56	· · ·	< 0.30	710 32	00 0.15	• •	21	< 0.1		VYDEQ ³⁴
	Aug-14 7	.07 8080	]	340	1300 5.4		580 54		<0.30 8		0 0.1	7	17	0.0090 635	0 WYD	
PGDW41B Jar	-10 7.63 4	70		108	1030 2.6	8	270 57	.5	NM	31.4 20			< 0.3	1.88		EPA ³⁰
	Apr-11 7	05 4866	<u> </u>	112	896	3.18	452 46	.9	NM	97.6 20	54 0 <0	.05 17.5		< 0.019		EPA ²⁷
	Jun-147.			130	980	4.3	290 55		< 0.15 3	}	2800	0.44	< 0.03 0.5	1	4170 V	VYDEQ 33
D.C.D.VII.	Aug-14 7			140	920	3.4	270 61		< 0.30 3	1000	2700	0.39	0.18	0.55	4220 V	VYDEQ 33
PGDW42	Jan-10 9.			88.5 181	011	<5.0	5.06 <	0.0	NM	13.2 3	170.0.4	1.0	<0.3	0.0966		EPA 30
PGDW44	Jan-10 8.			113	911	<5.0	208 13	.7	NM		70 0.4 80 0.3		<0.3	0.403		EPA 30
PGDW44	Jan-10 8. Apr-11 8	17 4720	<del> </del>	100	994 1060 2.0 1100 2.2	<5.0 0	259 28 259 19	.3	NM NM		80 0.3 90 0 <0	05 <0.03.3	<0.3	2.07		EPA ³⁰ EPA ²⁷
·	Jun-14 8.	11 5690	<del></del>	94 81	1100 2.0	)	200 20	} [_]	<0.15 4:	32.1 2	3100	0.03 \0.03 2	.06		4420 V	YYDEQ ³⁴
·	Aug-14 8	28 5900	<del> </del>	80	1000 2.2		290 20 250 21	<u> </u>	<0.15 4	<u> </u>	2900	0.34 0.22	<0.03 2.4 <0.03 3		4420 V	YYDEQ 34
PGDW45	Jan-10 7.	63 1103		379	59.4 2.6	1	138 31		NM	14.5 2		1.9	0.3	< 0.100	4440 V	EPA ³⁰
105 1115	Apr-11 6	85 1085	<del> </del>	364	61.6 2.8		159 34		NM .	18.4 2		1.7.	0.64	< 0.019		EPA ²⁷
·	Jun-14 7.	17 1310		350	97		160 35		0.19 31	- 10:12:	330	2.0	1.4	< 0.0076.83	10 WYD	EO 34
	Aug-14 7	.01 1150	1	360	97 79	2.7	120 32	ļ	0.24 36		250	1.7	0.98	<0.0076 82 <0.0076 74	0 WYD	EQ 34
PGDW46	Jan-10 7.			329	91.1 1.8		90.3 9.	89	NM	8.4 120	5	0.5	2.3	< 0.100		EPA ³⁰
PGDW47	Jan-10 9.	52 970		44.1 183		< 5.0	6.87 <	5.0	NM	21.6 33	30	1.5	< 0.3	< 0.100		EPA ³⁰
PGDW48	Jan-10 8.			89.8 725		< 5.0	147 4.3	35	NM	24.1 18	840 0.3		<0.3	0.0491		EPA ³⁰
PGDW49	Jan-10 7.	66 5470		243	1210 11		486 15		NM		60 0.4		7.7	11.4		EPA ³⁰
	Apr-11 7	34 5333		296 330	982 990	9.66 10 11	417 12		NM	54.3 32		.05 8.75		2.41		EPA ²⁷
	Jun-147.	31 5840	ļ	330	990	10	430 14	0	0.20 68		3500 0	.58	6.0	0.084	5340 V	VYDEQ ³⁴
	Aug-14 7	.09 6190		310	960		420 13	0	0.19 61		3300 0	.46	4.4	0.18	5220 V	VYDEQ ³⁴
PGDW50	Apr-12 8			33	1290 3.0		314 12	.8		7.8 3470		008 < 0.03				EPA ³³
PGPW01	Mar-09 8	85 1016	<b></b>	60.6 213			5 0.0847	] 	NM	15.7 39	PO	1.2	<0.5	0.0793	ļ	EPA ²⁹
D C DVI 102	Jan-10	55.1000		74.7 173		<5.0	5.7 < 5	0	NM	15.3 30	<b>)</b> ()	1.2	<0.3	0.112		EPA ³⁰
PGPW02	Mar-09 8	57 1883	<b>{</b>	82.9 390	}	0.643 36.	7 0.240 1	<u>}</u>	M	8.9 85′ 8.5 84′	<u> </u>	0.5 0.5	<0.5 <0.3	0.283 0.255	<b>.</b>	EPA ²⁹
<b></b>	Jan-10	16 1956	<del> </del> -	82.8 393 77	1-414	<5.0 0.92	34.4 <	L	NM						<b></b> -	EPA ³⁰ EPA ³³
PGDW01	Apr-12 8 Mar-09	46 1836	1	234	414 808	6.15	34.7 0. 398 93		<1.00 8. NM	51 88 34.3 18		< 0.20 0.1	6.2	0.11 NM		EPA ²⁹
LODWOI	wiar-09		L	234	808	0.13	398 93	_{FO}	INIVI	34.3 1	pυ U U.2	<u>†                                    </u>	0.2	INIVI	<u> </u>	EFA

			l e		_						(7)				3	
Well Name	le le		SC (µS/cm)	Alkalinity (mg/L)	Na (mg/L)	K (mg/L)	Ca (mg/L)	Mg (mg/L)	Br (mg/L)	Cl (mg/L)	SO4 (mg/L)	F (mg/L)	NO ₃ (N) (mg/L)	Fe (mg/L)	TDS (mg/L)	Source
ž	Date	Hd	SC	7 5 9	Na Na	Ž	ථි	ž	Br	ן ד	SC	F(	월 5	Fe	=	
PGDW02	Mar-09 8	11 551		108	85.8 1.8		34.8 5.	32	NM	2.6 17:	5	0.7	<0.5	NM		EPA ²⁹
PGDW03	Mar-09 9			39.5 272		0.403 16.		V	M	25.1 54		0.9	<0.5	0.0147		EPA ²⁹
	Jan-10 8.	71 1390		28.0 25		< 5.0	16.3 <		NM	20.7	570	0.8	< 0.3	< 0.100		EPA ³⁰
PGDW04	Mar-09 9	.17 1370		28.7 270		0.384 18		0.12	NM	21.6 5		0.9	< 0.5	NM		EPA ²⁹
	Jan-10 9.			38.3 265		< 5.0	15.5 <		NM	23.3	532	0.9	< 0.3	< 0.100		EPA ³⁰
PGDW10	Mar-09 8	95 948		147	204	0.394 6.1				8.0 293	}	0.9	< 0.5	NM		EPA ²⁹
	Mar-09 8	162 985		147	204	0.400 6.1				8.0 2	89	0.9	<0.3 <0.3	NM	.	EPA ²⁹ EPA ³⁰
DCDW12	Jan-10 8.			147	195	<5.0	5.76 <		NM	7.5 293 6.2 343	<u> </u>	0.9 0.7		<0.100 NM		EPA ³⁰ EPA ²⁹
PGDW13 PGDW15	Mar-09 6 Mar-09 7			303	196 269	1.85	61 72.2 10	19.9	NM NM	9.9 520	P	0.7	1.0	0.274		EPA ²⁹
PGDW15	Mar-09 9		1011	145	188	0.312 6.4			INIVI	13.4 25		0.8	<0.5	NM		EPA ²⁹
PGDW16	Mar-09 9		1011	21.2 278	100		2 0.527	INIVI	M	49.5 58		2.0	<0.5	0.0204		EPA ²⁹
PGDW17	Mar-09 8			20.5 509		0.413 21.		J J	M		380 1.8	2.0	0.5	NM		EPA ²⁹
PGDW19	Mar-09 7			291	194	1.36	29	3.24	NM	6.9	196	0.9	2.6	NM		EPA ²⁹
PGDW29	Mar-09 9			52.3 298		0.417 19.		0.2.	NM	24.6 59		0.9	<0.5	NM		EPA ²⁹
PGDW38 ·	Mar-09 8			46.9 373		2.28	70	2.3	NM	46.9 90		1.3	5.9	0.018		EPA ²⁹
unidentified			1340		210						860				884 G	res & Assoc. 25
unidentified											300				580 G	
unidentified			2180		459						990					ores & Assoc. 25
P14914P			2810		362						945				2150 (	
P98757W			1261		255						439				813 G	
unidentified			1400		203						480					res & Assoc. 25
P58929W			1250		400						400				825 G	
P34345W					190						400				680 G	
P59104W unidentified			974		210 210						460 345				644 Go	res & Assoc. ²⁵ Gores & Assoc. ²⁵
P24507P			9/4		210					-	2900					ores & Assoc.
unidentified			913		174						320				570	Gores & Assoc. 25
unidentified .			713		447						1110				1750	Gores & Assoc. 25
P97501W	· ·				555						1161				4010 0	
unidentified			457		38						67				302 G	
P30217W											2700				4180 0	ores & Assoc. 25
unidentified											827				1290 (	or es & Assoc. 25
P182983W			886												585 G	res & Assoc. ²⁵
unidentified			1140												752 G	
P46362W					140						1100				1550 (	
P62641W					970						2200				3550 C	
unidentified											2140			1	3100 0	
unidentified	-										642					or es & Assoc. 25
P53567W					175						84				384 G	
P25636W			1500		200						750					ores & Assoc. ²⁵
P110443	<del> </del>		1539		298						570			-		or es & Assoc. ²⁵
unidentified '		-			454					-	620			-	1800 C	
P28496W P26200W		-								-	29 2610		-			res & As soc. 25
r20200W			<u> </u>					l			2010				1 2880 C	ores & Assoc.

<del>. . . . . .</del>

Well Name	Date	pH	SC (µS/cm)	Alkalinity (mg/L)	Na (mg/L.)	K (mg/L)	Ca (mg/L)	Mg (mg/L)	Br (mg/L)	Cl (mg/L)	SO4 (mg/L)	F (mg/L)	NO ₃ (N) (mg/L)	Fe (mg/L)	TDS (mg/L)	Source
unidentified			2160		445						988				1530 C	ores & Assoc. 25
unidentified			3790		339						2310				3510 C	ores & Assoc. 25
P40603W											210				710 Go	res & A ssoc. 25
P76475W			1320		260						540				808 Go	re s & Assoc. 25
P14548P											1049				1690 C	ores & Assoc.25
P30162W											169					Gores & Assoc. 25
P32163W											690				1130 €	ores & Assoc. ²⁵
P9941P			2720		579						1290				2040 0	or es & Assoc. 25
P116598W					229						119				376 G	
unidentified											296				930 Go	
P25011W											2400				3560 C	ores & Assoc. 25
P177246W			1180		248						457				775 Go	r es & Assoc. ²⁵
			1180		126	]			T		237				590 Go	res & As soc. 25
P190223W			920												607 G	res & Assoc. ²⁵
P191733W			956												631 Go	res & Assoc. ²⁵

NM – not measured

S22

## C – Summary of Production Well Construction and Stimulation

Table SI C1. Production well construction summary (listed in order of completion date). Information retrieved from well completion reports using API number

				te	જ	<u>5</u>			E		erval	
API Number Well Name	Abbreviation	Latitude	Longitude	Completion Date	Year Plugged & abandoned	Ground Elevation (m AMSL)	Total Depth (m)	Depth to Fort Union (m bgs)	Surface Casing (m bgs)	Top of Primary Cement (m bgs)	Mud Filled Interval Below Surface Casing (m)	Drilling Mud
200					C. 100 Co. 100	• •					CV2000000000000000000000000000000000000	
49-013-06388 Mae H. Rhodes 1	MHR 1	43.26009		31/1953 1953 1	642.0	1.622.0		041.8 156.7			2812	"Chem Gel"
9-013-06357 Ora Wells 14-12	14-12	43.24571	-108.59549 8/7			1622.8		048.5 190.5		160	1704	Invert
9-013-06359 Govt 23-7	23-7	43.24841	-108.57139 5/1			<u>'</u>	2,450 ?		176.2 19	60 B	1784	Q-Broxin Gel
9-013-06474 Wirth 1	W 1	43.29472	-108.65019 10/		61 1680			84.5 200.9 1			2698	"Gel"
9-013-06395 Tribal Pavillion 23-2	23-2	43.26371	-108.61039 12/		57.5	1631.9		027.5 195.1		one B	0	Invert
9-013-06451 Shell Govt 22-35	22-35	43.28179	-108.61019 2/2		57.5		1,676 ?	1100177	189.6 N	one ²	1486	Invert
9-013-06358 Govt-Ocean Lake 1	GOL 1	43.24649	-108.52271 6/1			1599.0 ^G		19.2 177.7		2	355	Invert
9-013-06389 Tribal Pavillion 14-1	14-1	43.26021	-108.59541 6/1			1631.6		141.2 205.4		2 E	17	Invert
9-013-06376 Govt 21-8	21-8	43.25711	-108.55111 7/1		1.000 =	1629.5 ^G		96.7 189.3			?	Invert
9-013-06413 21-5	21-5	43.27111	-108.55099 7/1		1626.7	G	1,524 1		192.3 65	12	463	Invert
9-013-06341 Unit 13-13	U 13-13	43.23449	-108.595	7/16/1963		G	1,411?		190.2 ?		?	Invert
9-013-06392 Tribal Pavillion 14-6	14-6	43.26056		6/1963 164			1,219 ?		184.7 ?		?	Invert
9-013-06402 Govt 32-4	32-4	43.26739	-108.52629 7/1			)	1,524 ?		188.1 N	one ^B	1336	Invert
9-013-06336 Unit 24-14	24-14	43.23231	-108.60861 1	1/22/1963				121.7 186.8		70	209	Invert
9-013-06273 Govt 44-20	44-20	43.21694	-108.54119 3	/16/1964 196		2 G	1524 ?		187.4 N		1337	Invert
9-013-06281 Woodring 23X-24	23X-24	43.21879	-108.59271 4/2				1,250 ?		184.4 N		1066	Invert
9-013-08017 Runner Herfords 44-17	44-17	43.23091	-108.65981 5/2		31.9		1,292 ?		183.8 N		1108	Invert
9-013-06424 Govt 34-33	34-33	43.27444	-108.64449 5	/27/1964 ?		1652.9 ^G	1,558 ?		183.8 ?	Е	?	Invert
9-013-06363 Govt Tribal 33X-10	33X-10	43.25019		26/1964 1983 1			5,863 1	025.7 67.4	0	23	2787 ^I	Invert
9-013-06387 Tribal Pavillion 24X-3	24X-3	43.26151		30/1965 164	$\overline{}$			002.2 188.	1 94		759	Invert
9-013-06355 14-11	14-11	43.24649	-108.61341 12/		- 1633.1	G	1,503 ?		185.3 ?	Е	?	Invert
9-013-06917 IND 13-13	13-13	43.27589	-108.55431 1/	20/1966 ?		1637.1 ^G	1,177 ?		186.8 ?	R	?	"Chem Gel"
9-013-20062 Tribal Pavillion 31-15	31-15	43.24194		6/1968 1631	-		1,050 ?		205.7 ?	N	?	Invert
9-013-20084 Maxson 32-9	32-9	43.25278	-108.64511 5	/27/1968 196			1,070 1		187.8 N		882	Invert
9-013-20298 W. E. Lloyd	WEL	43.26011	-108.62528 2/	23/1972 198		2		025.7 277.7		N	?	"Chem Gel"
9-013-20414 Unit 41X-10	41X-10	43.25511	-108.62201 1/2					024.1 188.7		P	229	Invert
9-013-20454 IND 14-20-258 41X-2	41X-2	43.26944	-108.60241 11/					072.9 185.0		A	?	Invert
9-013-20457 Tribal Pavillion 31X-3	31X-3	43.26949	-108.62556 12/					028.4 188.	4 35		0	Invert
9-013-20442 W.H. Paul Patent 42X-11 42		43.25349		9/1974 162′				016.5 183	.2 ?	A	?	Invert
9-013-20443 Unit 42X-12	42X-12	43.25444	-108.58139 1/1					54.6 184.4		A	?	Invert
9-013-20456 Unit 31X-14	31X-14	43.24071	-108.60569 1/1	9/1974 1629	9.2		1,569 1		185.0 ?	A	?	Invert
9-013-0491 Clair C Day	CCD	43.20167	-108.67991 5/1	6/1974 197	4 1634.	)	2445 10	30.2 194.5	None	В	2251	Invert
9-013-20581 TR1-22	TR1-22	43.22741	-108.62019 2/7		1986 1		1,280 1		186.5 79		607	Invert
9-013-20586 Tribal 1-21	1-21	43.22741	-108.63944 3	/17/1976 197	6 1627.	)		73.5 190.5		В	1019	Invert
9-013-20598 Taylor Patented 1	TP 1	43.22806	-108.61041 5/1			1610.0	1,222 ?		127.4 ?	N	?	Invert
9-013-20602 Tribal 1-31	1-31	43.27409	-108.56089 7	/23/1976 197		5		38.1 125.3		N	?	Invert
9-013-20654 Tribal Unit 1	TU 1	43.22849	-108.61409 11/				1,119 1	82.3 200.3	<549		<349	Invert
9-013-20668 Blankenship Fee 4-8	4-8	43.26556	-108.64009 3/2	5/1977 164	7.1		1,586 ?		135.3 56	4 R,P 42	9	Invert
9-013-20700 Roland Patented 34-13	34-13	43.27528	-108.63379 8/3			1615.4	1,981 1	228.3 147.2		N	?	Invert
9-013-20748 Shoshone-Arapahoe 24-11 T	24-11	43.24556	-108.49179 5/1	3/1978 1978 16	08.1	G	4,564 ?		457.8 N	one B	4106	Invert

ıber	me .	ntion		a	Completion Date	gged & ed	Ground Elevation (m AMSL)	pth (m)	Fort 1 bgs)	Surface Casing (m bgs)	rimary m bgs)	Mud Filled Interval Below Surface Casing (m)	Mud
API Number	Well Name	Abbreviation	Latitude	Longitude	Complet	Year Plugged abandoned	Ground El (m.AMSL)	Total Depth (m)	Depth to Fort Union (m bgs)	Surface ( ogs)	Top of Primary Cement (m bgs)	Mud Filled Below Surf Casing (m)	Drilling
*			42 22040		T. C.						В		
49-013-20775 T 49-013-20764 D		24-4 44-15	43.22849 43.23056	-108.59569 5 -108.61959 6/2	/22/1978 197	8 1622 162	00.5		99.7 120.7			1095 8	Invert
49-013-20764 D		21-11	43.25521	-108.61939 6/2 -108.61039 3			29.5	-	23.5 189.6 21.1 187.5			279	Invert Invert
	ribal Pavillion 12-13	12-13		-108.61039.3 08.595768.5/12/1	/14/1979			,	90.3 175	.6 29	0	114	
	ISA Tribal 258 41-9	41-9	43.25651		4/1979 1641			1,585 ?	190.3 173	184.1 27		90	Invert Invert
49-013-08274 T		TU 2	43.22841		4/1979 1641 4/1979 1979 16			1,309 ?		199.6 83		638	Invert
	ISA Tribal 258 22-10	22-10	43.22841		13/1979 164			-	24.1 185.3		550	365	Invert
49-013-20965 G		G 1	43.24167	-108.67261 10/			1	1,675 ?	24.1 165.5	200.9 No		1474	Invert
	ISA Tribal 258 21-15	21-15	43.24209		6/1979 1632		. 1	1,585 10	150	188.7 ?	A,R,P	?	Invert
49-013-20879 U		44-10	43.24649	-108.62161 1	2/17/1979				27.2 184.4			401	Invert
49-013-20879 U		22-12	43.253096 -10		17/1980 162		*	/	33.6 178.6		A	?	Invert
	ribal Unit 238 11-14	11-14	43.24151	-108.61299 2/5		162	98.5		31.1 184.1		N	9	Invert
	ribal Pavillion 16-28	16-28	43.29028	-108.52409 7/1		102	1612.7 ^G	1,386 ?	31.1 104.1	163.1 ?	N	9	KCl polymer
49-013-21026 F		F 1-17	43.23139	-108.52409 7/1		1980 1			21.7 190.5		В	1520	Invert
	ribal Pavillion 14-2	14-2	43.26021		8/1981 1634		G G		07.1 182.6		R,P 49	1 3 2 0	Invert
	Vest Pavillion 1-8-1B	1-8-1B	43.25619		9/1981 1981 16		G	1,577 10	07.1 102.0	183.5 N		1404	Invert
49-013-21130 T		21-9	43.25639	-108.65011 6	/24/1981 199				07.7 248.4		ne	70	Invert
49-013-21130 T		12-3	43.26659	-108.63569 7/8			1644.4 ^G		143.3 185.9		A	?	Invert
	unner Herfords 1	RH 1	43.23056		7/1981 1981 16		1044.4		18.6 185.9		В	1035	Invert
	ohn K. Coolidge 1-4	1-4	43.26306		0/1981 1981 10 0/1982 1641				72.3 200.6		96 <19		Invert
49-013-21302 T	S	14-24	43.21631	-108.04944 3/2 -108.4725	9/22/1982 198				92.6 315.5		90 \1:	<264	KCl polymer
49-013-21302 T		A-1	43.29259		0/1983 1671		3		10.1 184.7			330	Invert
	cean Lake Tribal 1-15	1-15	43.23789		4/1983 1990 15			4,807 11		304.8 <1	189 <8		Invert
49-013-21421 T		B-1	43.29539	-108.65472 9/1			<u> </u>	1,674?	43	181.4?	A 109 \0	9	Invert
	avillion Fee 33-11	33-11	43.24846	-108.6039	9/15/1993		,	,	51.6 190.8			0	KCl polymer
	avillion Fee 12-11	12-11	43.25227		19/1993 163				05.8 191.1		68	77	KCl polymer
	ribal Pavillion 11-10	11-10	43.25648	-108.6348	12/29/1993 10.				44.5 190.5	79		602	KCl polymer
	ribal Pavillion 42-10	42-10		98.620931 6/15/1		- 1042.0			09.5 190.5	.8 78		598	KCl polymer  KCl polymer
	ribal Pavillion 31-10	31-10		08.625138 6/25/1			1637.4		09.5 190	3 64	,	462	KCl polymer  KCl polymer
	ribal Pavillion 23-10	23-10	43.24889	-108.63068 7/1			1647.7		42.4 184.4		? ^T	?	KCl polymer
	ribal Pavillion 43-10	43-10		98.621267 9/21/1			1639.2	-	13.8 195.	4?	A	?	KCl polymer
	ribal Pavillion 33-2	33-2	43.26208	-108.60522 11/			1639.2	,	26.6 192.0			0	KCl polymer
	ribal Pavillion 23-1	23-1	43.26396	-108.59019 11/			1651.7		77.8 182.9		94	411	KCl polymer
	ribal Pavillion 41-15	41-15	43.24277	-108.61865 11/			1631.7		38.1 185.0		N N	?	KCl polymer
	ribal-Pavillion 43-6	43-6	43.26299	-108.5767	5/26/1995		1621.2		08.3 128.0		A	9	KCl polymer
	ribal Pavillion 23-11	23-11	43.25071	-108.60653 2/9		163			13.2 167.0		<152	0	KCl polymer
	ribal NP 31-11X	31-11X	43.2848	-108.57413 11/		10.	1677.6		58.2 705.9		E E	?	KCl polymer
49-013-21904 P		13X-3	43.26333		8/1999 1999 16	30.7	10//.0		38.1 192.0		T	?	PHPA/LSND
	avillion Fee 42X-9	42X-9	43.25278	-108.63806 2/1			1647.1		55.8 185.9			332	LSND
	avillion Fee 41-11	41-11	43.25556	-108.6000	2/12/1999	1627 3	20.7.1		32.7 169.2			0	LSND
	ribal Pavillion 33-10	33-10		08.626454 5/6/19		160	57.3		55.2 156	.7 20	7	50	PHPA/LSND
	ribal Pavillion 33-3	33-3	43.26306		5/1999 164			,	22.3 154.5		T	?	PHPA
	ribal Pavillion 44-3	44-3	43.25944		9/1999 163				10.4 171.6		71 R	499	PHPA/LSND
<u> </u>	ribal Pavillion 15-21X	15-21X	43.24055	-108.62952 7/2		16.	38.3	-	66.8 244.	8?	T	?	Invert
		32-10		08.630100 5/10/2		. 0.		19727 10	22.0 = . 1.	V .	0	419	LSND

												_	
					9		5			ш)		Mud Filled Interval Below Surface Casing (m)	100
		-			Completion Date	89 P	Ground Elevation (m AMSL)	Total Depth (m)	+ 3	Surface Casing (m bgs)	Top of Primary Cement (m bgs)	e at	_
Number	9	Abbreviation		ə	H0	Year Plugged abandoned	Slev (	隻	Depth to Fort Union (m bgs)	'asi	ĔΈ	등흔 =	Mud
5	(an	via	de	hud	leti	# 6 H	물절	l ag	<b>₽</b> ₺	) a	- L	Mud Filled Below Surf Casing (m)	[ 원
Z	=	bre	Latitude	igi	<b>P</b>	_ E	₩.	Ta	₹5	fac )	ne o		
API	Well Name	4P]	[at	Longitude	<u>5</u>	Vear Plugg abandoned	Š.E.	To	<u> </u>	Sal	<u> </u>	5 & 5	Drilling
49-013-22058 Pay		13-11	43.24861	109 61306 2/2	3/2001 1630	) 1			05.2 186.5		44	<58	PHPA
49-013-22057 Pay		21-13	43.24083		3/2001 1630 3/2001 1620			1,067 ?	05.2 180.5	134.7 ?	N N	?	DeepDrill®
49-013-22068 Tri		43-2	43.26333	-108.59972 3/1		16	84.6	1.036 ?		109.7 <1	07	0	Unknown ^R
49-013-22070 Tri		13-2	43.26371	-108.6158	3/8/2001	16		1,036 ?		123.1 19		75	DeepDrill®
49-013-22101 Tri		24-1	43.261667 -		3/2001 163		,,,,	1,036 ?		125.0 12		0	LSND
49-013-22026 Tri		32-1	43.26722		3/2001 165			1,030 ?		109.7 18		73	LSND
49-013-22072 Tri		34-2	43.26023		4/2001 163				22.9 118.0		5	0	LSND
49-013-22069 Tri		12-6	43.2675		9/2001 162				85.7 120.4		N	?	DeepDrill
49-013-22027 Tri		44-1	43.26027	-108.58027 3/3		,,,,	1638.0	1,067 ?	05.7 120.1	111.9 < 1	22	<10	LSND
	bal Pavillion 14-10	14-10	43.245833 -10		4/13/2001		1640.7		4.75 110.3	44		332	DeepDrill®
49-013-22104 Pay		13-15	43.23583		4/2001 2006 16	32.5	101017	1,113 ?	1170 11010	132.9 ?	N	?	PHPA
	villion Fee 12-11W	12-11W	43.25194	-108.615	5/3/2001		1632.5	991	?	131.1 59	4 R	463	LSND
49-013-22087 Pay		34-3R	43.26028	-108.62528 5/4			1638.6		15.0 110.3			558	PHPA
49-013-22059 Pay		11-11	43.255122 -1	08.613706 5/			1632.2		01.6 161.8		91 ^R	0	PHPA
49-013-22061 Tri		12-5	43.2675	-108.55555 5/2			1621.5	1,058 ?		112.2 49	4	382	PHPA
49-013-22060 Pay		13-12	43.250891 -1	08.593728 6/			1622.5	998	?	99.7 280		180	LSND
49-013-22103 Pay		34-11	43.24514	-108.60531 6/1			1628.5	1,024 ?		161.5 ?	A	?	"gel"
49-013-22128 Tri		13-1	43.26433	-108.59553 6/2			1652.3	1,071 ?		163.1 ?	N	?	LSND
	bal Pavillion 11-12	11-12	43.25639	-108.59422 8/3			1626.7	970	?	164.3 12	2	0	LSND
49-013-22125 Pay		21-10	43.25625	-108.63078 8/1			1641.0	1.807 10	15	201.2 69		491	LSND
49-013-22145 Tri		43-1	43.26378	-108.58139 9/1	/2001		1648.7	1,128 ?		162.2 15		0	PHPA
49-013-22144 Tril		33-1	43.26381	-108.58536 9/6			1646.8	1,059 ?		163.1 15		0	LSND
49-013-22126 Tri	bal Pavillion 12-7	12-7	43.25265	-108.57613 9/8	/2001		1621.8	1,021 ?		164.0 ?	N	?	LSND
49-013-22188 Pay	villion Fee 21-10W	21-10W	43.25625	-108.63039 9/1	5/2001		1640.4	1,341 10	11.9 189.0	4	42	253	LSND
49-013-22186 Pay	villion Fee 23-12	23-12	43.250699 -1	08.589188 9/	19/2001		1621.5	994	?	162.8 15		0	LSND
49-013-22147 Tri	bal Pavillion 44-2	44-2	43.26011	-108.60217 9/2	2/2001		1634.3	1,250 10	21.1 162.8	?	A	?	?
49-013-22172 Pay	villion Fee 31-9	31-9	43.25686	-108.64486 9/2	8/2001		1645.6	1,050 ?		162.8 61		0	LSND
49-013-22149 Tri	bal Pavillion 34-10	34-10	43.24658	-108.62526	10/6/2001		1646.5	1,747 10	46.4 197.5	<188		0	LSND
49-013-22146 Tri	bal-Pavillion 34-1	34-1	43.26083	-108.58639 10/	13/2001		1639.8	1,020 ?		162.8 ?	A	?	LSND
49-013-22150 Tri	bal Pavillion 21-12	21-12	43.25639	-108.59114 10/	20/2001		1629.2	1,128 ?		107.3 15	9	52	LSND
49-013-22141 Tri	bal Pavillion 12-10	12-10	43.25167	-108.63556 11/	7/2001		1645.0	1,496 ?		189.6 31		0	LSND
49-013-22181 Tri	bal Pavillion 12-1	12-1	43.26778	-108.59169 11/			1642.0	1,128 ?		162.8 73		0	LSND
49-013-22191 Tri	bal Pavillion 42-3	42-3	43.26778	-108.61922 11/	16/2001		1641.0	1,227 10	35.4 162.8	<	61	0	LSND
49-013-22180 Tri	bal-Pavillion 22-1	22-1	43.26725	-108.59011 11/	21/2001		1657.2	1,128 ?		162.5 46		0	LSND
49-013-22195 Tri	bal Pavillion 33-10W	33-10W	43.248702 -10	8.626805 12/6/2	001		1668.2	1,545 10	54.6 16	0.9 20		43	LSND
49-013-22153 Tri	bal Pavillion 41-3	41-3	43.27056	-108.62056 12/	7/2001		1643.8	1,228 10	37.2 157.6	?	A	?	LSND
49-013-22215 Pay	villion Fee 22-11	22-11	43.25283	-108.61128 12/	15/2001		1632.2	972	?	189.0 ?	A	?	LSND
49-013-22200 Pay		43-11	43.25089	-108.60044 12/			1627.0		26.3 162.5		22	0	LSND
49-013-22212 Pay		11-3	43.27083	-108.63369 1/9			1647.7		32.4 160.9		N	?	LSND
49-013-22198 Pay		41-10	43.255851 -1	08.620913 1/			1637.4	969	?	162.8 16	5	2	LSND
	villion Fee 13-12W	13-12W	43.2485	-108.59681 1/2			1624.3	,	44.9 159.7			0	PHPA
49-013-22229 Pay		24-3B	43.25947	-108.63089 2/8			1641.3		12.9 200.9			0	LSND
	Pavillion Fee 11-11B	11-11B	43.25697	-108.61594	2/16/2002		1635.3		04.3 170.7			0	LSND
49-013-22106 Pav		31-11	43.25703	-108.60528 2/2			1629.5		19.6 165.8			0	LSND
49-013-22207 Pay	villion Fee 23-3	23-3	43.26411	-108.62944 2/2	7/2002		1644.4	1,890 10	22	189.0 ?	A	?	?

					<b>.</b>		<b>n</b> c			E		Interval	
			100		Completion Date	Year Plugged & abandoned	Elevation L)	Fotal Depth (m)	<b>-</b> 0	Casing (m	Top of Primary Cement (m bgs)	e ute	
API Number	<u>o</u>	Abbreviation		43	<u> </u>	g G	llev )	Ę	Depth to Fort Union (m bgs)	asi	n p		Mud
<b> </b>	Name	/int	e	Longitude	etic	Year Plugg abandoned	Ground Ele (m AMSL)	)eb	9 E	o e	P. T.	Mud Filled Below Surfa Casing (m)	∑
ź	<u>Z</u>	ırev	Ĭ l	ji	de l	r P	ĒΨ	I	# #	lac	e of	H × gil	Ē
<b>[ [ [</b>	Well	rpp	Latitude	Ę	Jo.	ea ba⊥	iro m/	ţo,	) jii	Surface ( bgs)	, d , d	Mud F Below Casing	Drilling
				4.5	7								
	villion Fee 32-11	32-11	43.25356	-108.60664 3/2/			1630.7		16.8 175.0		A	0	LSND
	villion Fee 44-11	44-11	43.24513	-108.60059 3/6			1627.0		36.3 162.2		A	?	LSND
	villion Fee 42-9W	42-9W	43.25308	-108.64158 3/2			1642.9	1,042 ?		161.8 0		0	LSND
	villion Fee 32-9W	32-9W	43.25408 43.25328	-108.64472 3/2			1645.6	1,055 ?	12.0.190	162.2 0		0	LSND LSND
	ibal Pavillion 32-10B villion Fee 13-11B	32-10B 13-11B	43.25328	-108.62539 3/2 -108.61672 4/9/			1638.0 1633.7	1,783 10		6 55	5 R(4)	437	
	villion Fee 13-11B	13-11B 14-3W	43.24961	-108.61672 4/9/			1644.7		16.2 188.1 27.5 189.0		3-57	0	LSND LSND
	ibal-Pavillion 12-2	14-3 W 12-2	43.26694	-108.635/3 4/1			1634.9		36.3 159.0		.5	0	LSND
	ibal-Pavillion 23-10W	23-10W	43.24886	-108.63153 12/			1648.4	1,399 10		.80	.5	0	LSND
	ibal Pavillion 23-10C	23-10W 23-10C	43.24789	-108.62947 10/		56.1	1048.4	1,747 ?	41.6 102	175.6 ?		9	LSND
	villion Fee 34-3B	34-3B	43.26033	-108.62783 10/2					05.8 196.6		38 ^R	641	LSND
	ibal Pavillion 24-2	24-2	43.259882	-108.610983 11		10.1	1636.2		20.8 171.3	21		42	LSND
	ibal Pavillion 23-10B	23-10B	43.25047	-108.63122 11/			1649.0	1,721 10		4 29		104	LSND
	ibal Pavillion 33-10B	33-10B		08.624267 12/14/			1638.0	1,710 10		94.8 61		0	LSND
	villion Fee 12-11B	12-11B	43.254237	-108.615986 1/			1634.3	-	01.9 167.9	31	1 R	143	LSND
	ibal Pavillion 43-10B	43-10B		08.620928 1/20/2			1657.8	1,756 10		3.9 35		3	LSND
	ibal Pavillion 24-11	24-11	43.24517	-108.61017 1/20			1630.7		28.7 160.9		177	16	LSND
	villion Fee 31-10B	31-10B	43.25494	-108.62822 1/2			1639.2	,	11.3 192.0	4	11 ^R	219	LSND
	villion Fee 33-11B	33-11B	43.25061	-108.60636 1/2	1/2005		1629.8	1,212 ?		155.8 14	6	0	"water based"
49-013-22599 Pa	villion Fee 44-11B	44-11B	43.24686	-108.60303 1/20	5/2005		1627.6	1,203 10	33.3 193.5	1	83	0	LSND
49-013-22216 Tr	ibal Pavillion 21-14	21-14	43.24125	-108.60981 1/2	8/2005		1632.2	1,707 10	50	192.0 ?	T	?	LSND
49-013-22243 Pa	villion Fee 13-10	13-10	43.24911	-108.63539 2/3	2005		1642.6	1,739 10	45.5 193.2	?	Ñ	?	LSND
49-013-22269 Pa	villion Fee 21-10B	21-10B	43.25481	-108.63272 2/3	2005		1640.4	1,715 10	13.2 193.2	12	65 ^R	1072	"water based"
49-013-22600 Pa	villion Fee 43-11B	43-11B	43.24806	-108.60033 2/1	1/2005		1626.1	1,203 10	31.7 192.9	0		0	"water based"
49-013-22324 T	ibal Pavillion 42-10B	42-10B	43.25219	-108.62019 2/1	5/2005		1635.6	1,708 10	09.2 189.	3 0		0	LSND
	villion Fee 22-11B	22-11B	43.25147	-108.61264 2/1			1632.5		10.7 192.3			0	"water mud"
49-013-22419 T	ibal Pavillion 32-10C	32-10C	43.252211 -10	08.627491 2/18/2	005		1640.1	1,225 ?		190.8 3	1	0	LSND
	villion Fee 22-11C	22-11C	43.25431	-108.60886 2/2					5.55 193.5		$?^{N}$	?	LSND
49-013-22634 Pa		44-4	43.25944	-108.63994 3/1		1.1		1,737 ?		186.2 SI			LSND
	ibal Pavillion 12-12	12-12	43.253	-108.59683 3/1			1625.8		49.1 193.5	29	0 ^R	97	"water based"
	ibal Pavillion 33-2C	33-2C	43.26319	-108.60839 3/2			1632.2	-	27.2 194.8		15	0	LSND/PHPA
	ibal Pavillion 13-2B	13-2B	43.26333	-108.61317 3/2			1633.7	1,210 10		196.6 15		0	?
49-013-22633 Pa		43-4	43.262618 -10				1645.6		35.1 182.9			0	LSND
	ibal Pavillion 33-2B	33-2B	43.26322	-108.60333 4/5			1633.1	,	34.8 196.6		5	0	LSND
	villion Fee 14-3B	14-3B	43.25944	-108.63425 4/5			1642.6		28.7 189.0			0	DeepDrill®
	villion Fee 41-11B	41-11B	43.25703	-108.6025	4/14/2005		1628.5	/	17.1 196.0		4	78	?
	villion Fee 42-4B	42-4B	43.26764	-108.63994 4/10		9.5	1622.2	-	46.1 196.6		8	1	LSND
	ibal Pavillion 21-11B	21-11B		08.610928 4/19/2			1632.2	1,181 98		5.7 15		0	LSND
	villion Fee 13-3W	13-3W	43.262919 -1	08.636420 4/2			1645.6	1,403 10		185.3 19		0	LSND LSND
	villion Fee 41-10B	41-10B	43.256943 43.28969	-108.620175 5/ -108.64469 5/2			1637.1 1666.6		6.39 195.1		152 2 ^N		
	W Pavillion Fee 34-28 ibal Pavillion 32-3	34-28 32-3	43.28969	-108.64469 5/2			1643.5		18.9 196.0 13.8 196.3	9	7. ^A	?	DeepDrill® LSND
49-013-22259 11 49-013-22171 Pa		32-3 43-9	43.25081	-108.62586 6/1 -108.63997 6/1		2.0	1043.3		55.2 196.3			7	DeepDrill®
	ibal Pavillion 22-3	22-3	43.25081	-108.63997 6/10 -108.63169 7/10					33.2 196.0 29.6 196.0		183	0	"water based"
	ibal Pavillion 44-3C	22-3 44-3C	43.26844	-108.63169 //10		7.9	1640.7		29.6 196.0 04.9 196.0	_	46	0	?
1-19-013-22/21 If	ivai raviilivii 44-3C	44-3C	43.20130	-100.022/8 //1	7/2003		1040./	1,130 10	04.9 190.0		40	U	1

API Number Well Name	Abbreviation	Latitude	Longitude	Completion Date	Year Plugged & abandoned	Ground Elevation (m AMSL)	Total Depth (m)	Depth to Fort Union (m bgs)	Surface Casing (m bgs)	Top of Primary Cement (m bgs)	Mud Filled Interval Below Surface Casing (m)	Drilling Mud
49-013-22245 Tribal Pavillion 32-2	32-2	43.26949	-108.6039	3/30/2006	1640.1		1,609 10	52.8 195.1	0		0	"Gel-Chem"
49-013-22824 Pavillion Fee 33-12	33-12	43.24928	-108.58614 4/1	/2006	161	9.1	1,682 10	60.7 193.9	61		0	"Gel-Chem"
49-013-22819 Haymaker 14-21	14-21	43.24208	-108.49453 5/1	6/2006		1606.0	3,597 13	49.0 766.3	?	E	?	KCl polymer
49-013-22825 Pavillion Fee 22-4	22-4	43.26606	-108.65239 4/3	/2007		1651.4	1,674 10	74.7 158.5	61		0	PHPA
49-013-22100 Tribal Pavillion 42-15	42-15	43.23981	-108.62144 4/1	2/2007		1634.6	1,659 10	33	157.6 ?	A	?	PHPA
49-013-23068 Leonhardt 41-26	41-26	43.1249	-108.28517 6/5	/2007	2007 1	557.2	2,286 12	07	202.7 N	one ^B	2083	Water based

Coordinates for Tribal Pavillion 32-2 incorrect in well file -approximate coordinates provided.

#### Abbreviations

AMSL – Absolute mean sea level

 $bgs-Below\ ground\ surface$ 

? - Unknown

PHPA - partially hydrolized polyacrylamides

LSND - low solids non-dispersed drilling mud

DeepDrill® is a product of Newpark Drilling Fluids and is described as a buffered blend of polyhydroxyl alcohols. No MSDS on this product was provided to EPA.

#### Superscripts

- A Cement bond log (CBL) conducted at completion but not available
- B No apparent use of production casing in borehole
- E Either cement bond log not conducted at completion or not available
- G Ground elevation estimated from coordinates using "GPS Visualizer" located at: http://www.gpsvisualizer.com/elevation.
- I Invert mud below intermediate casing at 1236 m bgs at 33X-10
- N Well completion report indicates cement bond or temperature log not conducted at completion
- P Parted casing, leak in casing, or casing failure
- R Remedial cement squeeze(s) following primary cement. Number of CBLs in parenthesis
- T Top of cement difficult to discern high amplitude readings in cement bond log

Table SI C2. Description of stimulation stages in the Pavillion Field. Information obtained from well completion reports using API search number

Table	)1 C4, .	Desc	ripuon oi	sumu	lation	stag	es in	me Pa	VIIIIO	nrı	21a.	miorn	iation	obtaine	ed from well completion reports using API search number	****
Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during . Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls) .	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
MHR 1		MV													P&A after completion in 1953. "Water sands" at 5780'-5810', 7145'-7250', 7970'-8040', 9000'-9100', Filled with "heavy mud" from 2,141'-11,000'. Cement plug from 2017'-2141' Intermediate casing cut at 1700' and pulled. No production or stimulation.	Yes
14-12 63	.6 WR	2/20/	1999	8.76 9.	46 9 10	0.93		8.36		X 15				1,134 "P	umped 25# linear gel w/75 % CO2, 157 bbls fluid, 85 tons CO2"	No
ļ				15.93				I		X 31		3	I	[	"137 bbls 75% CO2 foam"	1
			./3/1964 .7/1980 6.89	,	10.34	10.69	<b>→</b>	4.83		X 5,	103				"Frac treated Wind River interval 3294'-3370' and Fort Union interval 3782'-3789'w/25000 gals 9.6#/gal salt wtrTotal load 947 bbls wtrwell flowed diesel and load wtr" "Lost 150 bbls KCl fluid" "Acidz w/2500 gal 12% i & Tylenesalt watertotal load 947 bbls wtrFlowing at rate16 bbls salt wtr and diesel oil/day." Sundry notice dated 2/15/1980 for workover using "a. 1000 gal 15% HCl containing 2 gals A-200 inhibitor, 2 gals M38W surfactant, 1 gal J-237 diverter, and 35 lbs L-41 iron sequestering agent b. 5500 gals 12% HCl, 3% HF mud acid containing 10% U-66 mutual solvent, 22 gals A-200 inhibitor, 11 gals surfactant, 195 lbs L-41 iron sequestering agent. c. 2500 gals 3% HCl with A-200 inhibitor, M38 surfactant, and 12.5 gals L-53 clay stabilizer. Displace with 17.5 bbls 3% ammonium chloride water	
	1618.5	OTT Q/4	/1060								<del>  </del>				containing surfactant and clay stabilizer."  "250 gallons of "breakdown acid" followed by cement squeeze.	
	1630.1 1875.7	TU 8/5	/1960					ļ ļ	 	X X X					"250 gal breakdown acid" followed by cement squeeze "250 gal breakdown acid" followed by cement squeeze "250 gal breakdown acid" followed by cement squeeze	
23-7	18/3./.	TU 8/3	71960							Λ					P&A after completion in 1961.Well history missing from well completion report.	No
23-7 W/ 1	1	<u>г</u> МТ			l 										P&A after completion in 1961. Wen instory missing from wen completion report.  P&A after completion in 1961. No apparent production well casing. No stimulation or production.	No
23-2 501	7 WR 6		01 9.38 7.58	30						X 1	3.6	05 (	•	130	"70Q CO2 foam"	No
23 2 301		R 6/1	6/2001 17.9	3	12.07 9.65 2	35 5					9,21	)			"70Q CO2 foam" "70Q CO2 foam" "70Q CO2 foam"	
	720.5 W 893.1 W	R 6/1 R 2/1	5/2001 /1965		12.76					X 2 X	1,95				"70Q CO2 foam" "Frac all zones"	
	1035.4	TU 2/1	/1965					†	·	X					"Frac all zones"	
22-35		FU													P&A after completion in 1963. No apparent production well easing. Well history missing from well completion report. No record of production or stimulation.	No
GOL 1		FU													Completed in 1963. Perforated in three intervals in WR Formation. Put into production on 6/11/1963. P&A in 1974. No information on stimulation.	No
14-1 322					4.76	6.96				X 2	17 sl	s	0	2,735 "T	otals pumped 54 tons CO24360 gals w/meth anol."	No
	618.4 W			ļ				ļ		X			ļ	ļ	"1500 gal 15% HCL"	
	713.8 W 925.4 W			22.75	16.55	43 17	.24	10.34		X X				ļ 	"1500 gal 15% HCL"  "Injected 12,000 gallons #2 diesel into intervals 3036'-3045' and 3744'-3780'. In sundry notice dated 3/25/1993 plan to "plug back water bearing perforation in the Fort Union at 3744-3780."	
21-8		WR													Perforated in WR Formation. Completed in 1963 as a shut-in well and P&A unknown time later. Well history and completion information missing.	No
21-5 352	.0 WR 1	2/8/19	99							X			0	898	Recompletion in 1999. "HES 70Q foam, 4 gal/M HgClean, 4% KCl" on 12/8/1999. Numerous perforated and squeezed intervals. No documented production or stimulation prior to recompletion.	No
U 13-13		FU											2	1,130 Pro	duction from Fort Union Formation. Informa tion on completion and possible stimulation missing from well completion report.	No

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (hpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
14-6		WR											0	27	Production from Wind River Formation. Information on completion and possible stimulation missing from	No
32-4		FU													well completion report.  P&A after completion in 1963. Information on well history missing from completion report. No apparent production well casing. No stimulation or production.	No
24-14		FU											2	1,834 Pro	duction f rom base of Wind River Formation. Five perforated intervals between 3443'-3515' without stimulation.	No
44-20		FU													P&A after completion in 1964. No apparent production well casing or production. Drilling report missing from well completion report.	No
23X-24		FU													P&A after completion in 1964. No apparent production well casing or production. Cement plugs at surface, 522'-675', 2035'-2200', and 3765'-3930',	No
44-17		FU													P&A after completion in 1964. No apparent production well casing or production.	No
34-33		FU													Perforated at 2566'-2588' in WR Formation. No information on stimulation or production. Well history missing from well completion report. P&A date unknown	No
33X-10 9	86.3 W	R. 2/22	1965 21.36			16.5		6.89		X 5	,897	0		0	In 1964, acidized in Frontier Formation with "15,000 gals MCA." In 1964, "sptd 500 gals 15% HCl on perfs [in WR Formation] & broke formation down w/1400 psi TP (600 psi CP)total load 532 bbls. "Frac treated Wind River pers15,000 gals 9.6#/gal salt water containing fluid loss additivesTotal load 933 bbls" Completed in 1964. P&A in 1983. Drilled to Madison Formation.	
24X-3 13	59.4 FU	4/28/	966			1.0 8	27			X			2	9,653 "Tr	eatedw/1000 gal P-12 solvent (Dow) contai ning 10 gal free-flo 'C'"	No
14-11		WR											2	1,426 Pro	ducing from Wind River Formation. Perforat ions from 3192'-3864'. Well completion report is not available.	No
13-13 10	18.0 WF	9/7/1	965 16.55			23.0	24.82	19.31		X 2	268				"Breakdown withsalt waterspearhead frac with 500 gal. 15% HCl. Frac with 5000 gal 4% salt	
	1099.7 1099.7		/1965 14.48			28.5	28.96	14.48		X 5 X 5					water." "Breakdown with 750 gal salt waterInj 500 gal. 15% HCl. Frac with12,000 gal 4% salt water." "Diesel frac with 24000 gal diesel."	
32-9	1077.7	FU	0/1703			21.0	28.90	27.38		A 3.	,++3				P&A after completion in 1968. No apparent production well casing or production. Cemented intervals 567-667', 1200-1300', 3200-3300' during P&A.	Yes
WEL 47	9.3 F 6/	14/197	1												Drilled to Mowry Formation. Acidized in Frontier formation with 50,000 gal 7-1/2% HCl and 1000 gal KCl. 1979. P&A in 1981.	. Yes
41X-10 5	51.4 W	R 2/7/1	973			19.3	1	13.79		X					Invert mud contained up to 78% oil while drilling. "Frac treatedas follows9# KCl wtr containing 5# J-133/1000 gal2500 gal 15% HCl containing 5# J-133/1000 gal9120 gal 9# KCl wtr containing 40# J-133, 20# J-110 and 1 gal F-63/1000 gal, 1# J-134 and 400 scf/bbl nitrogen1460 gal 9# KCl wtr containing 560# J-133, 300# J-110, 15 gal F-63, 2 gal J-34 and 139,000 scf nitrogenflushed w/9# KCl wtr containing 5# J-133/1000 galWell flowed back approx. 600 BLW since opened to pitconsiderable amt of wtr." Completion report indicates that 2675 bbls of water flowed to pit between 2/7/1975 – 3/7/1975. On 3/9/1975, "A total of 145 bbls 9.23/gal KCL water was used to keep well under controlflowed control water to pit. Flowed 142 bbls in 10 hrs." Between 3/12/1975-3/26/1975, 745 bbls of water flowed from well In correspondence dated 5/27/1980 [not in well file - obtained from landowner], 41X-10 recommended for plugging and abandonment because of "problems with water production and casing failure." P&A in 1981 with cement plugs (40 sxs each) at 2400°, 2900° and 3456°.	<del> </del> 

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation		Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)		Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	1232.6	U 2/8	k/1979			6.0 44	1.82	22.75		X 4	7,17	1			While perforating FU Formation "Flowed well to pits continuously." "Controlled well w/4% KCl wtr w/clay stabilizer & surfactant. Lost 80 bbls to form while doing soacdz'd gross perf 4044-4450 w/4000 gals 15% HCl acidOpened well to pit & cont'd to flw to pit overnight to cleanup." "Foam frac treated with 90,000 gals to qualify foam, 1,950,000 SCF nitrogen & 645 bbls gelled KCl wtr for sd carrying agent. Total load to rec 645 bls." ISIP for acid stimulation = 4.14 MPa. Updated well schematic in WOGCC (2014).	
41X-2		WR :	1/28/1973												17 perforations from 1554'-4398' with diesel oil to control well. No documented stimulation or gas	No
31X-3 3	95.6 WR	8/30/2	001							X			0	1,215	production  Completed in Dec 1973 with 27 holes from 1665'-4988' and 8 holes 3154'-3161'- no apparent stimulation. Stimulated in Aug 2001, "Frac 1298-1309"	No
42X-11		WR											0	222	30 perforations from 2014' -4741' and 3 perforated intervals from 3773' and 3793' during initial completion in 1974. No documented stimulation fluids. 20 perforated intervals added during recompletion in 2001. No documented stimulation.	No
42X-12	1149.7 FI	J 1/19	/1974							X			0	295	"400 gal 15% HC1"	No
31X-14		WR											2	7,691	Producing from Wind River Formation. Perforations in Wind River and Fort Union Formations during initial completion in 1974 - no apparent stimulation.	l No
CCD		MV													P&A after completion in 1974. No apparent production well casing. No stimulation or production. Water at 2715'. Converted to water well.	No
TR1-22	961.6 WI	2/7/	980							X			0	5,281	In Sundry Notice dated 2/7/1980, "Proposed procedureAcidize well using a 3 stage acid program: a) 500 gal 15% HCl b) 2000 gal RMa c 500 gal 7.5% HCl. Note: all acid should contain 400 cc N2/Bbl acid, 10% mutual solvent and a clay stabilizerFrac well down tubing"	No
1-21		FU													"Lost 80 bbls mud to formation, probably in fractured zone 2738-43 [at 2749'-2790'] lost additional 60 bbls mud." P&A after completion in 1976. No apparent production well casing. No stimulation or production. Cement plugs at 550'-700', 3500'-3650' and 3830' – 3965'.	No
TP 1		WR											0	5,607 7	perforated i ntervals between 3406-3572. No record of stimulation.	No
1-31		WR													Perforations at 2900' and 3580'. Well completion report not available.	No
TU 1		WR											0	220	Perforated from 3460'-3537'. No record of stimulation.	No
4-8	630.9 W 814.1 W 1484.4	R 2/8	2/2005 13.10 /2005 18.27	)	26.05	18.0 38.2	39.38 4	9.45		X 1 X 9 X 6	1 25	1	,110 "	Frac slick	water, 104 bbl s" Updated well schematic in WOGCC (2014).  "Frac: slickwater121-bbls 6% KCl, 28.5 tons of CO2"  "500 gal 15% BDA frac w/102,000 gallons of gel water300 scfpb nitrogen"	Yes
34-13	1404.4	FU	10/17//							1	1,20		0	290	Perforations from 2664-2676. Information on well completion missing.	No
T24-11	<del>                                     </del>										$\Box$				P&A after completion in 1978. No apparent production well casing. No stimulation or production.	No
24-4	<del>                                     </del>	WR			<u> </u>			1			H				P&A after completion in 1978. No apparent production well casing. No stimulation or production.	No
	953 EII	_	76 22 06	l	0.65			182		v	Н		b	1 3/19 "1		N.T.
17-13 12	1367.3	U 4/2	76 22.06 8/1978 24.1	Б З	9.65 15.17	24.1	3	4.83 6.21 10.34	<b></b>	$\frac{X}{X}$	{}		f	1,540 1	500 gal 15% HCldis      pl'd w/28 bbls 2% KCl wtr."  "Acdz'd w/1500 gals 15% HClDispl'd w/32 bls 2% HCl."	.No
	1530.1	FU 4/2	5/1978 15.8	6	13.79			10.34	<u> </u>	X	<u> </u>	. <b></b>	İ	[	"Spt'd 750 gals 15% HC1Displ'd acid w/29 bbls 2% KC1."	11
[	1530.4	'U 4/	4/1978 20.6	8	13.79			6.55		X X					'Pump 1500 gal 15% HCldisplacing acid w/40 bbls KCl.''	
		-	1/1978 33.0	_	10.34	4.0		6.55		_					"Pmp'd 500 gals 7-1/2% HC1Displaced acid w/38 bbls 2% KC1."	
21-11 95	]	R	3/12/1979 13		6.89			4.83		X 5	,897		0	335	Acidize w/850 gals 7 1/2% HCl w/2 als C-17, 2 gals J-501 II, 8 gals J-38 & 25# citric acid. Frac w/15000 gals YE4P5D fluidPump 5000 gal 3% HCl acid, displace w/2% HCl water." 13 perforated intervals from 1681-2750 in April 2001 without apparent stimulation.	No
	J1213.7	FU 2/	3/1979	L	12.41	4.5 12	2.41	5.52		Χ	إ		l	L	"Pump 3150 gals 7 1/2% HCl6 gals M38W, 6 gals A200, 13 gals L-53 & 15 gals U-40."	]]

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation		Break Down Pressure (MPa)				-	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	1471.61	FU 2/2	1/1979		13.79	4.5 2	2.06	6.89		X					"Breakdown w/1100 gals 7 1/2% HCl w/2 gal M38W, 2 gal A200, 4 gal L-53 & 25/L-41. Displace w/9 bbls L-53 water foll'd 9 bbls fresh water."	
	1296.01	WR 2/ FU 3/2 FU 3/2	5/1981 2/1979 24.8 9/1979	2	11.72					X 2 X 9 X		2		18	"CT [coiled tube] frac 256 bbls, 177 mcf N2". Updated well schematic in WOGCC (2014).  "Acidize w/4000 gals 7 1/2 %Frac BWRversa gel"  "Frac [with] 4 bbls L53+15 bbls L53 wtr+6bbls acid." "Lost thousands of bbls KCl to Basal wind river."  "Acidize w/6000 gals wtr." 4252-4580 "WET"	Yes
41-9 560	634.0 W 688.2 W	R 10	1/2004							X 5 X 5 X 5	,443 ,443 ,443	2		15,593 '	74 bbls 6% KCl, 16.3 tons CO2Frac down casing" "78 bbls 6% KCl, 16.3 tons CO2Frac down casing" "82 bbls 6% KCl, 16.3 tons CO2Frac down casing"	No
	788.2 W 826.6 W 876.0 W	R 10. R 10.	1/2004 1/2004			25.0	16.05				,443 ,804 ,804				"87 bbls 6% KCl, 16.3 tons CO2" "100 bbls 6% KCl, 20.4 tons CO2" "103 bbls 6% KCl, 20.4 tons CO2"	
			V1/2004 V1/2004		17.39		16.87 17.51				,165 7,21	 5	+		"128 bbls 6% KCl, 24.4 tons CO2, 18,843 gal 70Q CO2 WF125Frac down casing." In proposed fracturing schedule "Pumping schedule to achieve a propped fracture half-length (Xf) of 82.9 ft with an average conductivity of (Kfw) of 3383 md.ftgel cone 7.5 lb/mgal"  From stimulation report: "281 bbls 6% KCl, 81.4 tons CO2, 33,656 gal 70Q CO2 WF125Frac down	g
															casing". In proposed fracturing schedule "Pumping schedule to achieve a propped fracture half-length (Xf) of 197.6 ft with an average conductivity of (Kfw) of 5366 md.ftGel cone 7.5 lb/mgal." Composition of WF125 from stimulation report: 2.00 gal/mgal F103 surfactant, 3.00 gal/mgal F104 foamer, 15.00 lb/mgal J218 breaker, 1.0 gal/mgal J318 liquid breaker aid, 5.63 gal/mgal B142 guar polymer slurry, 2.00 gal/mgal L55 clay stabilizer.	
	1472.2 ]	U 8/:	/1979 15.17		11.03	4.0		4.14		X					"Lost approx. 50 bbls mud in 24 hrs." [invert mud while drilling] "At'd gross Ft. Union perfs 4830-5097 with 4000 gal 7.5% HCl containing 2 gals A-200, 2 gals M38W, 4 gals L-53 and 35% L-31 per 1000 gal acid. Press csing to 1200 psi with invert oil. Pumped 1000 gal acidspacedball sealers in next 2500 gal acid. Followed with 500 gal acid without ball sealers. Flushed with 20 bbls 2% KCl water containing 6 gal L-53 clay stabilizer." "A total of 65 bbls invert oil has been pmp'd into well" [to control well].	
TU 2 10	69.5 WR							Ī		XX	Ī				"2500 gal 7-1/2% HCl" Cement squeeze after stimulation	No
	•		24/1979		<u> </u>	Ļ.,	<u> </u>	<u> </u>	<u> </u>		L			<u> </u>	"500 gal 15% HC1"	
22-10 60	734.3 W	R 12 R 12	2004 14/2004 14/2004 14/2004	13.00 22.34 29.65 28.96		18.5 22.3 29.6 28.9	8 7 5	8.14 8.45 8.95 9.51 0.69		X 9 X 6	,554 ,085 ,559 0,84			1,363 "8	9 bbls of clean fluid, 2 2 ton CO2"  "129 bbls of clean fluid29 tons of CO2"  "270 bbls of clean fluid17 tons CO2"  "165 bbls of clean fluid27 ton CO2"	Yes
	994.3 W	R 12	14/2004 14/2004 5/1979 7.58	20.70		11.7 4.0	6	0.69 1.17		X 1 X 1 X 0	0,88	<u>.</u>			"Frac: pump 92 bbls of 6% KCldidn't see a breakclean fluid 242 bbl34 tons CO2"  "A.T. perfs 3274-94 w/1000 gals 15% HCl & 48 frac ballsacid containing 2 gals inhibitor, 2 gals surfactant, 4 gals clay stabilizer & 3-5# iron sequestration per 1000 gals acid. Formation brokeFlushed 20 bbls of clay stabilizer water."	
	1396.3	FU 12	/11/2004 /9/2004 31.9  2/1979	31.21 0		46.6 49.2	8 9	32.08 1.94 5.17		X 7 X 2 X	824 4,17	5			"Frac 10 bbls to catch pressureclean fluid 119 bbls19 ton CO2"  "260 bbl clean fluid55 tons CO2"  "Pmp'd 57 bbls 9#/gal KCl w/.5 gal per bbl brine saver, .2 surfactant & .5 clay stablizerpmp'd 5 bbls KCl into formationpmp'd 40 bbls 9#/gal KCl @ 3 BPM 600# into formationacidizedw/3400 gal 15%  HClFlushed w/25 bbls of fresh water containing clay stablizer.	
	1530.1	TU 9/	2/1979							X	<u> </u>		<u> </u>		"Acid treat w/3400 gal 15% HCl"	

21-15 799	1014.7 V 1071.4 V 1071.4 I 1084.8 I	WR 1 WR 1	1/21/1979	11.02				<u> </u> 					io	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
21-15 /99	1014.7 V 1071.4 V 1071.4 I 1084.8 I	WR 1 WR 1	1/21/1979	11.02						77	<u> </u>		lo.	h 4	P&A after completion in 1979. No apparent production well casing. No stimulation or production.	No
	1084.8 I	U 11		11.03	10.34	7.0		2.07		X X 5 X	<b>3</b> ,79	2	0	24	"1000 gallons of 15% HCl". Completion record reviewed by WOGCC in letter to BLM dated 8/14/2012 concerning of 1,000 gallons of a 15% HCl solution in "compromised" casing between 735 to 1,105 feet below ground surface.  "Frac treat B.W.Rw/60,000 gals DOWELLS Y-F4 PSD frac fluid"  "Pmp'd 3450 gals 15% HCl containing 4 gals A-200 inhibitor, 2 gals M-38 W surfactant 4 gals L-53 clay stabilizer 35# L-42 iron sequestration agent/1000 gals of acid"	Yes
	l	<u></u>	/12/1979		13.79	7.0 1	3.79			Х					"A.Tw/2500 gal 15% HCl containing 2 gals A-200, 2 gals M-38 W, 4 gals L-53, 35# L-41 per 1000 gals acidDisplaced acid w/17 bbls fresh wtr containing L-53 clay stabilizer."	
								[	[	X	]		[		"1700 gallons 15% HCl."	
	1187.51	U 11	/2/1979		16.72	6.5		3.45		Х					"Pmp'd 2500 gals 15% HClAcid contained 2 gals inhibitor, 2 gals surfactant, 4 gals clay stabilizer, 35 lbs S-41 iron sequestration agent/1000 galsDispaced acid w/19 bbls fresh wtr containing 4 gals clay stabilizer"	
44-10 82	0.2 WR	10/14	/2004	21.84	8.41 14	1.4		3.68 1	4.70	X 9	072	2		1,751 Fr	rom WOGCC (2014), this interval was fracture treated with 150 barrels of CO2 assisted gelled water.	No
	869.9	0/14/	2004	22.64	8.32 14	1.6			19.91	X 8	115				Updated well schematic in WOGCC (2014)  "Frac: Gel total load 218 bbls" From WOGCC (2014), this interval was fractured treated with 218 barrels of CO2 assisted gelled water.	
			17/1979 /1/2004 31.2	8		11.7	2	10.68		X X 8	165				"Acidize: 3000 gal 15% HCl"  "Break formation with 6% KCltotal fluid pumped 134 bbls" From WOGCC (2014), " In October 2004 additional Fort Union Sands were selectively perforated between 3,592' and 4,925', and fracture treated with a total of 1,303 barrels of CO2 assisted gelled water."	
	1119.81 1147.61	U 10	/1/2004					3.12 8.32 12	2.89	X 9 X 2	7,21	6			"197 bbls clean fluidand 20 tons of CO2 See note above on gelled water. "97 tons CO2 and 276 bbls clean fluid". See note above on gelled water.	
	1400.6 I	FU 9/2	4/2004							X 2	2,45	В			"KCl prepadpump 70 quality CO2 foam frac88 tons CO2 and 11042 gal clean fluid." See note above on gelled water.	1
	1452.1 I	U 9/2	1/2004 7/2004 37.1	1	20.08	46.5	i	10.51 4.01			257 0,41	;			"Frac: 164 bbl 6% KCl, 150 bbl CO2" See note above on gelled water.  "269 bbls clean fluid and 440 bbls CO2" See note above on gelled water.	
			/17/1979			19.9	9.	4.01	·	X					"Acidize: 1500 gal 15% HCl" During cementing on 6/27/1979, "Pmp'd 30 bbls diesel ahead mixed w/5 gals surfactantLost returns last 40 bbls."	
22-12 518	5 WR 4	1/1/19	93								+		0	288	From WOGCC (2014) "In April 1993, additional Wind River Sands were selectively perforated between	Yes
	980.8 W				17.93	25.0	33.78	6.89		X 2	9,48	1	Ĭ 		1,701' and 2,388', and were not stimulated.  On 1/5/1980, "A.T. BWR perfs4100 gals 15% HCl containing 2 gals inhibitor 2 gals surfactant 4 gals clay stabilzer & 35# iron sequestering agent/1000 gals acid 4100 gallons 15% HCL, 2 gallons inhibitor, 2 gallons surfactant, 4 gallons clay stabilzer, 35 pounds iron sequestering agent per 1000 gallons acid." On 1/10/1989 "frac treat basal W.R. w/50,000 gal Titan III-30 gel" and B-11 gel breaker (1# per 1000 gal). "Flushed to top	
	1243.6 I	U 12	/21/1979 /18/1979 /12/1979		13.10 13.10 13.79		15.86	6.21 5.17 5.86		X X					perf w/1000 gals 2% KCl slicked w/3# per 1000 gal FR-16. All frac fluid contained 1 gal per 1000 clay master 1 gal per 1000 aqua flow - 2% KCl 1/2 gal per 1000 ASP 248."  "A.Tw/700 gals 15% HClflushed w/16 bbls."  "Acid treatw/3500 gals 15% HCl containing 2 gals inhibitor 2 gals surfactant, 4 gals clay stabiizer 35# iron sequestering agent per 1000 gals acidflushed w/19 bbls fluid."  "Acidize gross Ft. Unionw/6400 gal 15% HCl 13 gal I-15 13 gal foam X, 26 gal clay master 225# X R-	

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (MPa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation ·	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	1432.6 I	U 12	10/1979		15.17	440000000000	17.24	7.93		X					"Acidized FT. Unionw/4000 gal 15% HCL cont. 8 gal A-200 inhibitor, 8 gal M-38W surfactant, 16 gal L-	-
															53 clay stabilizer, 140 # L-41 iron sequestering agentDisplaced w/31 bbls fresh water containing 10 gal L-53 clay stabilizer."	-
	1500.2 I	U 12	10/1979					h		X	<del> </del>			· <del> </del>	"4000 gal HCl"	·
	1511.8 I	U 12	10/1979							Х	1†				"4000 gal HC1"	
11-14 991	.2 WR 2	/5/19	30							Х			5	12,550	"3600 gal HC1"	No
	1544.1 I							ļ		X	<b>∤</b> ∤				"2500 gal HCI"	
	1564.2 I	U 2/3	/1980							X	$\vdash$				"2500 gal HCl"	N.T
16-28															Perforations from 3714'-3736'. Well completion report not available.	No
1-17 14-2 481.	O W/D Q/	27/10	22			0.69				X			0	44	P&A after completion in 1980. No apparent production well casing. No stimulation or production.  On 11/12/1980, "Hit water flow while drilling at 4105'-4109'Drilling fluid was contaminated with	No Yes
						••••									watercrews attempted to reduce viscosity with the additional of dieselthe diesel and the contaminated drilling fluid did not mix in the wellbore, instead the diesel replaced the weighted mud causing a reduction in hydrostatic headthe well started to flow and was closed in." On 8/24/1982, "Pmpd 800 gals 15% HCl contag 2 gals M38 w/2 gals A-200+4 gals of L-53+#L-41Displaced w/9.5 bbls 2% KCl. On 8/25/1982, "Pumped 2000 gals 15% HClHCl contained 4 gals 38W + 4 gals A200 + 8 gals L-53 + 200 gals alcohol + 70# I-41. Pumped 2 bbls 2% KCl behind acid." Perforated at 20 depths from 1581-2980. "displace acid w/75 bbls 2% KCl"	
	664.5 W 1039.1 I					8.62				X X					"800 gal 15% HCl containing 2 gals M38 W/2 gal A-200 + 4 gals L-53 + # L-41, 9.5 bbls KCl "Spotted 3 bbls 15% HClpmpd 23 bbls 15% HCl.26 bbls 15% HClpmpd 5 bbls 4% KClto flush casing." On 4/16/1981, "bullheaded 100 bbls 4% KCl down csgspotted 3 bbls 15% HClsaw 4 perfs	
								ļ		<b> </b>	<b>∤</b> ∤				open up. Pmpd 23 bbls 15% HCl."	
	1148.2 I		/1981 /1981 17.93			7.93 17.9	2	3.10		X	<b>{</b> ⊦				From WOGCC (2014) "acidized"	·
	1370.1 I				26.20			5.10		X 2	3,587				"Spotted 21 bbls HC1took 2 hrs to pmp 10 bbls into formpmpd 22 bbls flush" "Pmp'd 20 bbls 15% HCl w/additivespumped 30 bbls acidflushed backside w/5 bbls KCl. On 3/30/1981, "frac as follows143 bbls Apollo 30 pad24 bbls gel48 bbls gel72 bbls gel72 bbls gel21 bbls 4% KCl flush."	
	1405.7 I	U 3/2	7/1981		24.13	17.0	26.20	7.58		X .					"Pmp'd 26 bbls acidfollowed w/24 bbls flushflushed backside w/5 bbls KCl wtrFracas follow-100 bbls Apollo 30 pad40 bbls Pad:24 bbls gel48 bbls gel72 bbls gel72 bbls gelflushed w/21 bbls 4% KCl."	
	1481.3 I	U 3/2	0/1981 37.2	3	22.75	17.0	27.58	8.27		X 9	,072				"Pmpd 12 bbls acidpumped 12 bbls acidpmpd 24 bbls acidpmpd 12 bbls acidDisplaced acid w/26 bbls KCl wtrPumped 48 bbls YF4PSD pad. 24 bbls gelled wtr." then 180 bbls YF4PSD. Materials charged for in frac include 700 lbs J-347 gelling agent, 48 lbs J-218 breaker, 16 gal J-318 breaker aid, 32 gal L-53 clay stabilizer, 5 gal D-47, 5 gal MW38 surfactant, A-200 inhibitor, U42"	1
1-8-1B															P&A after completion in 1981. No apparent production well casing. No stimulation or production.	No
21-9 657.													0	11	Information missing from well completion report but reviewed by WOGCC (2014). Well schematic in WOGCC (2014)	Yes
	725.4 W	R 6/8	1981	<u> </u>		6.89		ļ[		X	1,754		ļ		"Acidized" from WOGCC (2014)	
	796.7 W 1022.9 I	K 6/6	1981			6.89 23.4 11.7		ļ		X	<b>{-</b> ,₌,		ļ	.	"Acidized" from WOGCC (2014)	
	1022.9 I 1129.3 I	U 3/2	6/1981 6/1081			23.4	<del>(</del>	<b>├</b>		$\frac{A}{v}$ .	<u></u> †₂/⊇‡		ļ		WOGCC (2014) indicates that this interval was stimulated with "357 barrels of gelled water."  "Acidized" from WOGCC (2014)	
	1129.3 I 1209.1 I	U 5/4	0/1701 1/1981			11.7	2	<b>├</b> -		X X X	┨╌╌┝		ļ	· <b></b>	"Acidized" from WOGCC (2014)	·
	1205.1 I 1295.1 I	U 5/1	0/1981			11.7	7. 2.	<del> </del>		├ <del>``</del>	╂╌╌┼		<del> </del>		"Acidized" from WOGCC (2014)	··

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation	Stimulation Date .	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (MPa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	1340.5 I 1362.8 I 1426.2 I 1468.8 I	U 5/ U 5/ U 4/2	6/1981 7/1981 9/1981			8.27 12.4 7.58 15.1	7			X X X X					"Acidized" from WOGCC (2014)  "Acidized" from WOGCC (2014)  "Acidized" from WOGCC (2014)  "Acidized" from WOGCC (2014)	
12-3	1530.1 I 1481.0 I	WR : FU ?				10.3	4			X			0	1,970 P	"Acidized" from WOGCC (2014)  roduction of gas and w ater production in WR formation in 2005. Stimulation unknown.  Prodution of gas production in FU Formation in 1993. Stimulation unknown.  "6500 gals HCI"	No
RH 1	587.0 W 699.2 W 982.7 W	R 5/2	0/1982							X 2	8,12	3	5,982	10,417	P&A after completion in 1981. No apparent production well casing. No stimulation or production.  3 perforated intervals from 1926'-2136'. No information on stimulation.  "2000 gal 15% HCl, 26,000 gal 75% foam"  "1600 gal 15% HCl, 500 gal NH4Cl, 1500 gal 3% HF, 12% HCl"	No No
14-24 1 A-1	007.7 WR 1041.8 I 679.7 W 727.3 W	8/24/ U 8/2 R 4/2	1982 4/1982 0/1983					11.37		X X X X	9.50	7	155 7,	<b>0</b> 72	"Acidized" P&A in 1982 after completion. No production.  "Acidized"  "1000 gal + 1000 gal acetic acid" squeeze and reperf "1500 gallons HCl." Completion date used.  "4000 gallons HCl, 32,000 gal foam" Completion date used.	No
1-15 45	22.0 C 7/2 4722.9 (	7/198	3							Х Х	φ, 39	<u> </u>	1,116	19	"21000 gallons of acid" in Cody Formation "20 bbls KCl, 275 gal gel water" in Cody Formation	No
B-1	900.7 W 1465.5 I 1556.9 I	U 9/	9/1984							X 4 X X	99				"6000 gallons diesel + additives" "6878 gallons 7½ % HCl SC + HCl-HF" "2100 gal 7½%+15% HCL + additives"	No
33-11 5	601.1 W 627.3 W	R 2/5 R 2/5 R 2/5	/2002 16.20 /2002 12.27 /2002 10.69		15.51 12.41 13.79 12.07	25.0 25.0 25.0		8.91 7.45		X 7 X 8 X 8	,057 ,074 ,185		72 "BE	w/6% I	CdlFrac usin g 75Q CO2, 42 bbls gel, 16 ton CO2flush w/50% CO2."  "Frac-BD w/6% KClFrac using 142 bbls 75Q CO2, 42 bbls gel, 16 tonCO242 bbls 6% flush."  "Frac-BD w/6% KClFrac using 162 bbls 75Q CO2, 47 bbls gel, 18 tons CO248 bbls w/6% KCl."  "Frac-BD w/6% KClFrac using 164 bbls 75Q CO2, 47.5 bbls gel, 18 ton CO2, 48 bbls 6% KCl flush."	No
	855.9 W 1091.2 I 1160.4 I	R 2/5	/2002 11.72 · · · 3/1993	 	13.79 21.86		26.89	7.24		X 7 X X 2	]· 	 3			"Frac-BD w/6% KClFrac using 143 bbls 75Q CO2 foam, 42 bbls gel, 17 tons CO285 bbls 6% KCl flüsh."  "Acidize each zone w/500 gals 7 1/2" NEFE" [3580-3592 and 3815-3939 - total 1000 gals NEFE].  "Acidize each zone w/500 gals of 71/2" NEFE." [3807-3813 and 3830-3851-total 1000 gals NEFE]. "Frac	
12-11 1	1101.5 I	U 11 U 11	/23/2004 /23/2004	9.38 4.	9.14 2	2.4	20.77 14.73 9.38 2	6.07 1	5.83	X 9 X 1 X 1	8,14	<u></u> μ	51 "Fra	c70Q	well down tbg & csg w/33,650 gal CO2 foam frac,70Q."  CO2total load 107.1 bbls"  "Frac70Q CO2total load 175.1 bbls"  "Frac70Q CO2total load 196 bbls"	Yes
	1141.8 I 1164.9 I	U 11 U 11	/23/2004 /5/2004 8.96	16.13	7.52 2		17.57 11.11			X 1 X 2 X 6	8,14 4,14	4 9			"Frac 70Q CO2 216.8 bbl total load" "200 bbls water CO2 assist" "Sand can broke down 300# sand. Go to flush. Over flush 30 bbl Frac 210 bbl clean fluid + 253 from previous 463 total 40 tons CO2."	
	1449.0 I	U 10	/19/2004 /14/2004 /12/1993	11.49 16.44	38.61	40.6 25.0 18.7		8.27 5.23		X 8 X 1 X 3	,381 9,25 2,70	7 4			"128 bbl clean fluid, 29 tons CO2"  "36 bbl clean fluid36 tons CO2"  "Fracwith CO2 foam frac consisting of 11,819 gal of 2% KCl water plus 120 tons CO2total load 2% KC 279 bbls."	ži

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (hpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (MPa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	1624.9	U 10	/12/2004		37.23	25.0		10.25		X 1	4,19	7			"Frac39 tons CO2 and 208 bbl clean fluid"	
11-10 800	).7 WR	0/15	2004	11.18	9.56 2	1.4		6.98				1,238		21,643 In	formation on fluids used for stimulation n ot available.	No
1	818.7 W	R 10	15/2004	5.70 6	.49 15.4 10.92 <b>0</b> .71	1	1	7.02 1	<b>\$</b> .55	X 8	,165				Information on fluids used for stimulation not available.	11
	858.0 W	R 10	14/2004	18.96	10.92	18.6	1	[::::		$X \in$	,804		[	[	Information on fluids used for stimulation not available.	
	897.9 W	R 10	14/2004	5.35 1	<b>0</b> .71	16.6	]	[]]	20.36	Χ 6	804		[		Information on fluids used for stimulation not available.	
			/18/2004 9.38	15.17		35.0		10.38		X 8	,165		I		"frac…129 bbls clean fluid, 29 tons CO2"	
	971.7 W	R 10	8/2004 12.7	<u> </u>	22.75	32.0	1	10.55	20.81	X 5	443		l		"144 bbls clean fluid, 19 tons CO2"	
	1049.4	'U 6/	20/2005 16.2 /8/2004 7.05	29	22.06	30.0	]	11.20		X 1	3,60 9,05	3			"frac232 bbl clean fluid, 39 tons CO2"	
	1358.2	U 10	8/2004 7.05	8.96 3	0.0		]	4.24		X 1	9,05				"frac359 clean fluid, 54 ton CO2"	
	1462.7				20.17			1.78 1			4,49	ļ	l		"CO2 frac 226 bbls total loadrecovered 37 bbls of 226 bbl load."	
	1528.9	TU 9/	<b>2</b> /2004		21.52	18.5	50.81		15.16	X 1	4,96	)			"fraced down12,887 gal CO27OQpad volume 3952.6 gal total load 195 bblsblew rupture disk on	
															#1 CO2 pumprecoverd 41 bbls of 195 bbl load."	
42-10 762					46 12			8.32 2	1.04			595 14,	503 "To	tal load 8	6.1 bbls." Treatm ent report available for 2004 stimulation events.	Yes
	807.1 W	R 12	15/2004	9.74 8	27 13	.31		7.35		$X \epsilon$	871				"Frac 122 bbls slickwater" From stimulation report posted 8/9/2013, 4351 gal 70Q CO2 WF12 consisted of	
			l	. <b>.</b>			ļ	ļ		ļ	J				4351 gal water and 34 lb J216."	
			4/2001 12.82	1	12.07	25.0	12.41	7.70		X 9	,072		l		"fracFlush w/50Q CO2 foam"	
			V2001 9.51 1	D.31	-	30.0	15.51			X 3	,859 072				"frac" No information on stimulation fluids.	
	1068 FU	6/23	/2001 6.16 1	0.69		35.0	11.89	6.48		X	0/2	(			"frac" No information on stimulation fluids.	
	1202 FU	6/22	/2001 10.16 /2001 10.07		13.51 10.82	35.0	13.44	7.36		$X = \frac{1}{3}$	,34 1,34 1,525	, 			"frac70Q CO2 foamtotal clean fluid 267 bbls."	
	1239 F	6/22	72001 10.07 72001 6 52 1	5-44	10.82	30.0	10.00	9.27		X 1	1,34		ļ		"fracclean fluid 197 bbls"	
	1230 F	6/22	/2001 6.52 1 /2001 5.80 1	0.44	-	36.0	10.51	0.83							"fracpumped 84 bbls clean fluid"	
	1448 FU	0/22	72001 3.80 1 3/1004	0.31	-	33.0	10.51	0.14			1,34				"fractotal clean fluid 302 bbls, 89.5 tons CO2" In sundry notice dated 5/27/2005, "Acidize w/2000 gallons 15% NEFE, 2300# rock salt". WOGCC (2014)	
	1446 F	9/10	W 1994							X					states "no treatment" at this depth.	
	1620 FU	6/13	1994		-		<del> </del>	<b></b>		X	<del> </del>		<del> </del>		"Perf 5315-39, 5389-5403', 5476-86acidize w/1250 gal 7 1/2% HCl acid (6/13/94). On 6/12/2001,	·
	10201	0,11	1331							1					"Acidize - Stage 3 (5315-5339') Pump 750 gal 15% HCl750 gal 15% drop 48 balls, 700 gal & flush."	
		FU 6	/12/2001				†	t		X	11				"Stage 2 (5389-5403') Pump 700 gal 15% HCl, 250 gal 6% KCl w/28 frac balls, 700 gal 15% HCl"	
	1643		_	l	l						l .l				Stimulation at this interval not reported by WOGCC (2014).	
	[	FU 6	12/2001				1-3	1		Χ	[		1		"Stage 1 (5476-5486) Pump 900 gal 15% HCl, 10 bbls 6% KCl, w/30 frac balls, 500 gal 15%" Stimulation a	it
	1669														this interval not reported by WOGCC (2014). Modified wellbore schematic available in WOGCC (2014).	
31-10 10	7 FU 1/	16/20	02 11.30		15.17	30.0		6.14		X 8	211	1,412		15,504 "E	reak w 6% kclstart 70Q foam 242 bbl, 80 b bl fluid, 29 ton co277 bbl 40Q flush"	Yes
1	1095 FÜ	$1/1\epsilon$	/2002 10.69	·	14.48	35.0	1			X 1	2,52	,	† <u>-</u>	T	"Break w 6% kclstart 70Q co2 foam, 405 bbl, 151.5 bbl fluid, 39 ton co2"flush w 84.5 bbl 6% kcl"	
1	1377 FU	1/15	/2002 12.07	ļ	15.86	35.0	1	8.27 6.03		X 2	0,55	)	T	T	"Break w 6% kclstart 70Q co2, 695 bbl foam, 232 fluid, 74 ton co2flushed 50% co2 bbl."	
	1411 FU	1/15	/2002 14.13	[	16.89		I	8.80	[	X 1	<b>0</b> ,70		[	[	"Break w 6% kclstart 70Q co2 foam, 254 bbls fluid, 36 ton co2flush was 109.5 bbl 6% kcl."	
	1362 FU	6/22	/1994	Γ	<u> </u>	]	]	[	[	X	ו־־־ן		[	[	In sundry notice dated 5/28/2002, "Acid fraceach & all sets of perfs w/600 gals 7 1/2% HCl acid each	
															4770'-5478'."	
23-10 140	0 FU 7/	8/200	0 9.10 6.03 3	30.0				7.03		X 2	2,38	7			Pump 70Q CO2 foam fr ac3000 gals pad, 480 gals540 gals640 gals812 gals1200 gals3696	Yes
					<u> </u>		<u> </u>	<u> </u>	L				L		gals 50Q flushpumped 226 bbls KCL, 47 ton CO2."	
			/2000 14.92		8.27 28	8.5		4.27	L		2,51		<u> </u>	L	"Pumped 70Q CO2 foam frac3000 gal pad, 1700 gal1840 gals2843 gals 50Q flush."	
	1620 FU	8/8/	1994							X 1	4,74	<b></b>			"500 gal 15% HCl" "Frac w/16500 gal plus 700 N2 foam."	
43-10 138	9 FU 2/	6/200	2 11.86		19.31	35.0		5.28		X 2	1,89	606 28	,467 "I	rac break	w/6% KCLFrac using 547 bbls 70Q CO2 foam, 125 bbls gel, 63 ton CO2flush w/30%	Yes
	]		1	L	L										CO2."	

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Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (hpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (MPa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	1467 FU	2/6/	2002 11.24		17.24	35.0		5.16		X 2	8,93				"Frac-Break w/6% KCLFrac using 837 bbls 70Q CO2, 235 bbls gel, 95 tons CO2112 bbls 6% KCl	
	1574 FU	2/6/	 / <del>2</del> 002		20.34	34.0				X 1	5,94		ļ		flush." "Frac using 457 bbls 70Q foam, 130 bbls gel, 52 ton CO2flush w/120 bbls 6% KCl."	
					24.13			14.89			9,59				"Frac using 545 bbls 70Q CO2156 bbls gel, 61 ton CO2flush w/124 bbl 6% KCl."	
	1623 FU	9/20	/2002 20.48 0/1994		19.31			19.54		Х	1				Sundry notice dated 2/19/2002, "Picke tbg w/600 gal 15% acid. Spot 250 g 15% NEFE acidpress tbg to	11
	1678 FU				16.41	50.0		7.93		X 3	<b>0</b> ,55				5300 psi w/N2Pump 20 mcf N2 @ 2100 scfm @ 2800 psi" WOGCC (2014) indicates no stimulation at this depth. "Frac-total pumped 317 bbls KCl, 598 bbls CO2"	
33-2 432.										X 8	245	0		1,263 "C	il frac104 bbls clean fluid, 41300 scf of N2."	No
	552.3 W	R 10	18/2000				1			X 4	,245 ,954		I		"Coil frac93 bbls clean fluid, 43300 scf of N2."	
	605.6 W	R 10	18/2000							X 1	0,870 3,52: 5,03	)			"Coil frac177 bbls clean fluid, 961000 scf of N2"	
	624.5 W 644 WR	R 10	18/2000		ļ	ļ ·				X 1	3,52	; 	ļ	ļ	"Coil frac139 bbls clean fluid, 77100 scf of N2"	
			)/18/2000 18/2000		<b></b> -					$\frac{X}{V} = \frac{1}{8}$	0,03 0,698				"Coil frac206 bbls clean fluid, 124200 scf of N2" "Coil frac126 bbls clean fluid, 78000 scf of N2"	
	715 1 W	R 10	)/18/2000							X i	2.70				"Coil frac183 bbls clean fluid, 115800 scf of N2"	
	750.1 W	R 10	) 18/2000 ) 18/2000		·					X 1	7,04	)			"Coil frac254 bbls clean fluid, 162300 scf of N2"	11
	776.6 W	R 10	18/2000				1			X 1	2,70 7,04 2,92	7			"Coil frac317 bbls clean fluid, 83800 scf of N2"	
	849.2 W	R 10	21/1994				]			X	]:::[				"Acidizew/300 gals 15% NEFE"	
	862 WR			ļ	ļ					X	J		l	ļ	"Acidizew/300 gals 15% NEFE"	
			21/1994							Χ					"Acidizew/300 gals 15% NEFE"	+
23-1 810.	5 WR 10	0/13/	1994 ) 13/1994		11.40 12.25	5.0 1	2.34	5.38 5.38		X X X X	<b></b> ⊦		0	480	"Spot & pump 400 gal 15% NEFEgained 30.48 bbls in 72 hrs 15,000 ppm chl."	No
			) 13/1994 ) 13/1994		11.07		+.13 6	5.58 7.93		- <u>-</u>	┨╌╌┤				"Spot & pump 400 gal 15% NEFE"  "Spot & pump 400 gals 15% NEFE"	
	1393 FU	8/1.	3/1994		17.33		0	7.93 6.23		<del>     </del> -	<del>  </del>				"Pump 500 gals 15% NEFE"	
	1526 FU	8/1:	3/1994		21.28		9	7.96		X	11		†		"Spot & pump 500 gals 15% NEFE."	11
41-15 165	0 FU 11	/2/19	994		10.34	3.0 3	9.09	40.09		X 1	4,74	2 355 64	,192 "	500 gal 1	5% NEFE-PB", "fr ac w/16,600 gal 65Q N2 foam."	No
	1897 FU	117.	2/1994							X	11				"2000 gal 15% NEFE-PBgained 3.34 bbl in 1 hr(11,000 ppm chl)"	1
43-6 287.			999 10/1999		6.62 6. 8.55 6.	.0		1.57 4.24		X			0	1,062 300	gal "7.5% HL w/mutual solvent, HC2 surfa 'ctant, flush 4% KCl" 400 gal "7.5% HL w/mutual solvent, HC2 surfactant, flush 4% KCl"	No
	379.2 W	R 8/	10/1999		13.79	6.5		4.92		X X X	1				150 gal "7.5% HL w/mutual solvent, HC2 surfactant, flush 4% KCl"	11
	476.1 W	R 8/	10/1999		12.07	6.6	]	5.54		Х	]			[	250 gal 7.5% HL w/mutual solvent, HC2 surfactant, flush 4% KCl"	
	548.6 W				12.07			4.08		X	][				1000 gal "7.5% HL w/mutual solvent, HC2 surfactant, flush 4% KC1"	
	575.5 W	R 8/	10/1999	ļ	12.76	6.0		4.59 7.38		X X 2	1-55	,	ļ		1000 gal 7.5% HL w/mutual solvent, HC2 surfactant, flush 4% KCl"	
	723.6 W				<del> </del> -	<b></b> -				$\frac{A}{X}$	1,381		ļ		"clear frac" "clear frac"	
	751.6 W 1055 W	R 5/2	23/1995		<del> </del> -	<del> </del>	†	8.61		X	\$,07 <u>\$</u>		<b>†</b>	·	"Pmp 100 gals 15% HCl acid & 95, 180 SCE/N2"	
23-11 50						i i				V 4	075	88 208		i	"Coil frac81 bbls clean fluid, 34600 scf N2"	No
	522.1 W	R 10	14/2000		<b> </b>		†			X 2	0,93	5	†	·	"Coil frac282 bbls clean fluid, 141000 scf N2"	
1	554.1 W	R 10	14/2000				1			X _ 7	967		İ	[	"Coil frac119.5 bbls clean fluid, 59400 scf N2"	1
	607.5 W	R 10	14/2000				]		[	X 7	976		[	[	"Coil frac117 bbls clean fluid, 64100 scf N2"	
	739.7 W	R 10	14/2000	ļ	ļ	<b> </b> -	ļ			X 5	0,936 ,967 ,976 ,993 ,617		ļ	ļ	"Coil frac96 bbls clean fluid, 62100 scf N2"	
1	J/92.2 W	JK 10	12/2000	.L	J	J	1	l	L	X 9	J617		l	L	"Coil frac136 bbls clean fluid, 10700 scf N2"	التتبال

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	802.5 V	VR 10	12/2000							X 7	,128				"Coil frac102 bbls clean fluid, 71900 scf N2"	
	843.1 V	WR 10	)/12/2000 )/12/2000							X 1	,128 2,220 ,652	5			"Coil frac198.6 bbls clean fluid, 168,000 scf N2"	
	866.2 V	MR 10	12/2000					0 45		X 4	652				Coil frac 86.2 bbls clean fluid, 69000 scf N2"	
	11034 F	y 3/3/ U 3/2/	2005 7.78 2005 4.94					8.42 3.25 3.72		л. о Х 1	,649 3,160				"Frac: 4172 bbls 70Q" "Frac: 181 bbls 70Q"	
	1159 F	U 2/23	3/2005 11.03					3.72		X 1	3,11				"Frac: 181 bbls 70Q" "Frac: 9348 bbls 60Q"	
	1358 F 1388 F	Ų 3/6/	998					[::::		Χ			[		"Acidize w/300 gals 7.5% HCl"	
	1388 F	U 1/19	W1998	<u> </u>				ļ	ļ	X	ļ		ļ		"Acidize w/1000 gallons 15% HCl"	_
	1403 F	U 12/3	17/1997 4/1007							X	<del></del> -				"Acidize w/500 gal 15% HCl, flush w/brine" "Acidize w/500 gal 15% HClFrac-Delta frac-30% N2 used except flush. Total 742.3 bbls"	
	1558 F	9 12/2 U 11/2	4/1997 25/1997					<del> </del>		X	<del>{</del> }				"Acidize w/500 gal 15% HCl"	
	1581 F	U 12/2	2/1997 21/1997						·	X	11				"Acidize w/500 gal 15% HCl"	
										Χ					"Acidize w/500 gal 15% HCl"	
31-11X 2													1,666	8,797 Hy	draulic fracturing in Lance, Meetesse, Mesa verde, and Cody Formations. Acidize with 18,500 gallons 15% HCl. Frac w/1015 bbls CO2 foam	No
13X-3 4	10.9 WR	. 2/18/	1999		7.58 1. 3.79 1.	.5		5.40		Χ	J		0	0	"Acdw/400 gal 15% HCl"	
	527.3 V 584 WI	MR 2/	18/1999		3.79 1.	.5		3.25 7.65 5.10		X X X X	<del></del> -				"500 gal HCl" "Acd…w/300 gal HCl"	
	635 2 V	MR 2/	18/1999		9.24 1. 6.21 1.	: 5		5 10		ŀ\$	<del> </del>				"Acdw/250 gal HCl"	
	640.4 V	MR 2/	18/1999		0.21 1.	Ĩ·		J. 1 V		X	<del>  </del>				"Acdpmpd 73 gal HCl"	
	676.7 V	VR 2/	18/1999 18/1999					l		X			I		"Acdw/250 gal" "Acidize w/250 gal 15% HCl"	
	689.2 V	MR 2/	18/1999		5.52 1.			4.73		X	ļļ				"Acidize w/250 gal 15% HCl"	
	1179 F	U 2/1:	V1999 (1000			4.0		0.26 0.06		X	<del>-</del>				"Acidizew/1000 gal 15% HC1disp w/2% KC1Fluid pmp 41.5 bbl, fluid recvrd 12.6."	
	1381 F 1489 F	U 2/9/	1999					0.00		X X X X	<del>  </del>				"500 gal HCl" "500 gal HCl"	
	11510 F	(12/9)	1999					6.35		X	11				"500 gal HCI"	
	1558 F	U 2/9/	1999					6.35 2.95		Χ					"500 gal HCI"	
42X-9		FU						•					100 10		pleted · · in Fort Union Formation. Information on perforations and stimulation missing from well completion report.	No
41-11 60	2.3 WR	2/1/19	999							X			0	207	"Acidizew 1100 gallons 15% HC1"	No
	622.1 V 648.6 V	MR 2/	1/1999			6.48	1.61 1.50			X X X	<del>  </del>				"Acidizew/300 gallons 15% HCl each [perforated interval] (600 gals total)" "Acidizew/300 gallons 15% HCl each [perforated interval] (600 gals total)"	
	793.7 V	MR 1/	28/1999 11.89 1/1999	}	8.84 3.	8 13.0	\$6	0.05		X	<b></b>		ļ	ļ	"Acidize w/1500 gallons 15% HCl"	
	1033 F 1054 F				12.41 11.79	4.1 4.1		0.85 4.63			<del>{</del> ∤		<del> </del>	·	"Acidizew/500 gallons 15% HCl" "Acidizew/500 gallons 15% HCl"	
	1183 F	i 1/2	1/1999		7.58 4.		†·	4.63 0.99	·	X X	<del>  </del>		†	<u> </u>	"Acidizew/1000 gallons 15% HCl"	
	1384 F	t 1/19	1999 18.89		15.86	4.5		7.04		X	]		[		"Acidizew/1000 gallons 15% HCl"	
			1/1999 12.62		12.27			7.29		Χ					"Acidizw/500 gallons HLC" [HCl]	
33-10 64	0.4 WR	1/5/20	005 11.29		13.13	24				X 9 X 8 X 1 X 9	525	2	ļ <u>.</u>	2,547 "28	tons CO2"	Yes
			5/2005 6.58 7			22.5		6.96 8.69 3.99		X 8	1165		ļ		"24 tons" "32.6 tons CO2, 148 bbls 6% KCI"	-
1	1/30.3 V	MK 1/	4/2005 13.29 /2005 12.40		10.74 8.05	23.3	<b> </b>	0.09	<b></b>	$A = \frac{1}{2}$	ψ,δδί	)	ļ	L	"32.6 tons CO2, 148 bbls 6% KC1" "170 bbls 6% KC1, 28.6 tons CO2"	

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (MPa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	1192 FU 1562 FU 1637 FU	4/20			12.14 13.55		15.55	6.12 10.84 10.45		X 6,7 X 24,				"71.2 bbls CO2"  "Frac w/35# liner [linear] gel & 70% CO2 foam. Total fluid pmped 10,235 gals & 76.5 tons CO2."  "Acidize w/1500 gal 15% HCl. Frac35# linear gel w/70% CO2total fluid pmped 13,754 gal. Total CO2	
33-3 1372	FU											0	337	68 tons."  Perforated intervals in Wind River and Fort Union Formations. Production from Wind River Formation.  Information on stimulation missing.	No
44-3 213.	1 WR 4/ 505.4 W	/8/199 /R 4/8	9 /1999		7.58 9.65 1	5.0	12.41	2.30 8.84		X X 46,	090	1	1,663	"Adidizew/500 gals 15% HCl" On 4/8/1999, "Acidizew/500 gals 15% HCl" On 5/26/1999, "fracw/273 bbl clear frac" ISIP for acid stimulation was 3.63 MPa.	Yes
	634.3 W 679.7 W	R 4/8	/1999		10.34 6.82 3	.0		6.72 4.92		X X X				On 4/8/1999, "Acidizew/500 gals 15% HCl" On 6/2/1999, "fracw/243 bbl clear frac". ISIP for acid stimulation was 1.03 Mpa.  "Acidizew/200 gals 15% HCl"	
	838.8 W 849.8 W 1070 FU				11.20 11.38			3.06 3.45 5.69		X X X				"Acidizew/500 gals 15% HCl" "Acidize w/300 gals 15% HCl" "Pmp 7 bbl 15% HCl and 5 bbl 2% KCldispl acid w/10 bbl 2% KClreset pkr, pmp 2% KClat 1000	
	1080 FU 1183 FU 1214 FU 1322 FU	3/16	/1999 /1999 6.49 1 999 6.34 10 999 999	3.79 .34		6.0 6.0 3.0 5.0		3.03 3.56 3.85 0.15		X X X X				psiload pmpd 38 bbl"  "Acidizew/5 bbls [HCI]"  "Acidizew/500 gals 15% HCI"  "Acidizew/500 gals 15% HCI"  "Acidizew/500 gals 15% HCI"	
	1451 FU	2/25	/1999			5.0 4.0		0.15 4.83		X X			4= 6 117	"pmp 420 gal 15% HCl" "Breakdown on perf w/1250 gal 15% HCl"	
	1617 FI	2/7/2 2/2/2 12/5/2 1/27/1 1/6/19	01 6.21 4.83 001 10.34 001 10.34 2000 999 999 998		3.45 2 4.14 2			2.41		X		161	,,1/6 "P1	np 20 bbls 6% KClpump 20 bbls 6% KCl"  "Pmp 10 bbls 6% KCl"  "Pump 10 bblsAcidize w/15 bbls 7 1/2% acid, flush w/52 bbls KCl waterno flow back"  "Acidize w/41 bbls prod wtrpump 5.6 bbls more/pump 11.7 bbls 15% HCl & over flush perfs"  "Pmp perfs w/3000 gals diesel & 1000 gal pad acid"  . "Suspected casing collapse @ 15273Breakdown w/4000 gal diesel w/FE 1A Hyflo IV, Musol A"  "Breakdn w/2000 gals diesel w/20 gal Hyflo IV, 100 gal Musol ANo circulation before or during cement job; lost 1100 bbls mud [invert] before job"	No
32-10 161	7 FU 5/ 1661 FU	12/20	000		7.58 2	5.0		4.62 4.94		X X		29 2,	200 "Fra	c w/24,096 gal CO2 foam "  "Acidize w/1000 gal 7.5% HCl, flush 909 gals 4% KCL. Frac w/16054 gals 70Q CO2 foam." ISIP for acid stimulation = 0.94 Mpa.	Yes
13-11 764					16.55	26.0		6.62		X		0	431	"Fracusing 231 bbls wf 135 in 6% KCl water w/10% methanol + adds, 59 tons CO2573 bbls 70Q CO2 foam. Flush w/37 bbls KCl w/10%"	No
	807.1 W				15.86		1	8.58		X ]				"Fracusing 100 bbls wf 135 in 6% kcl w/10% methanol + adds, 24 tons CO2258 bbls 70Q CO2 foam. Flush w/40 bbls 6% kcl w/10% methanol."	
	849.8 W			L	16.55 7.58 2	J		9.24 7.48		X X				"Fracusing 130 bbls wf 135 in 6% KCl water w/10% methanol + adds, 35 ton CO2359 bbls 70Q CO2 foam. Flush w/42 bbls 6% kcl water w/10% methanol."  "Fracusing 276.2 bbls wf 135 in 6% kcl water w/10% methanol + adds, 90 tons CO2849 bbls 70Q CO2 foam. Flush w/55 bbls 6% kcl wtr w/10% methanol."	

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	1390 FU		/2001 /2001 11.72		20.68 9.65 2			7.38		X X					"Fracusing 174.5 bbls wf 135 in 6% KCl wtr w/10% methanol + adds, 40 tons CO2433 bbls 70Q CO2 foam. Flush w/69 bbls 6% kcl wtr w/10% methanol"	
21-13 5			001 11.38		11.72			8.27	_		0,886	5 2		1,422 "I	Freeusing 98 bbls wf 135 in 6% kcl water w/10% methanol + adds, 28 tons CO2275 bbl 70Q CO2	Yes
	651.1 W	/R 2/1	7/2001 18.62	<u>.</u>	17.93	30.0		8.96		X 1	9,504	i			foam. Flush w/33 bbls 6% kcl w/10% methanol."  "Fracusing 170 bbl Wf 135 in 6% kcl water w/10% methanol + adds, 50 tons CO2 488 bbls 70Q CO2	
	804.7 W	/R 2/1	7/2001 15.1′	<del>7</del>	15.17	30.0		11.58		X 1	9,05	i			foam. Flush w/33 bbls 6% kcl w/10% methanol."  "Fracusing 174 bbl wf 135 in 6% KCl water w/10% methanol + adds, 51 tons CO2264 bbls 70Q CO2 foam. Flush w/41 bbls 6% kcl wtr w/10 % methanol."	
43-2 50	2.9 WR 2.				0.97 3			6.83		X			0	97	"Fracusing 298 bbls wf 135 in 6% KCl water w/10% methanol + adds, 106 tons CO21000 bbls 70Q CO2 foam. Flush w/25 bbls 6% kcl w/10% methanol."Fracusing 174 bbl wf 135 in 6% KCl water w/10% methanol + adds, 51 tons CO2264 bbls 70Q CO2 foam. Flush w/41 bbls 6% kcl wtr w/10 % methanol."	No
	603.5 W 748.6 W	<u></u>			12.82 11.03			7.79		X 	ļ				"Frac159 bbls wf 135 in 6% KCl water w/10% methanol + adds, 50 tons CO2496 bbls 70Q CO2 foam. Flush w/30.5 bbls 6% kcl water w/10% methanol."  "Fracusing 156 bbls wf 135 in 6% methanol [typo 6% kcl water w/10% methanol?] + adds, 43 tons	
	902.2 W			L	14.24	<u> </u>		8.14 10.76		х Х					CO2452 bbls 70Q CO2 foam. Flush w/38 bbls 6% KCl w/10% methanol."  "Fracusing 209 bbls wf 135 in 6% kcl wtr w/10% methanol."  "Fracusing 209 bbls wf 135 in 6% kcl wtr w/10% methanol + adds, 67 tons CO2661 bbls 70Q CO2 foam. Flush w/46 bbls 6% kcl w/10% methanol."	
13-2 500	766.6 W 805.9 W 856.8 W	R 1/1 R 1/1 R 1/1 R 1/1 R 1/9	02 13.55 0/2002 23.84 0/2002 23.65 0/2002 24.8 0/2002 24.1 /2002 21.68 /2002 20.48	1 9 2 3	12.55 22.75 22.75 19.99 15.17 17.93 47.57	32.0 29.0 25.0 30.0		6.21 8.36 7.84 7.10 9.38 9.97 9.84		X X X X X			0	1,333 "F	rkctotals pumped 104 bbls KCl, 153 bbls CO2"  "Fractotals pumped 121 bbls KCl, 245 bbls CO2"  "Fractotals pumped 122 bbls, 192 bbls CO2"  "Fractotals pumped 160 bbls KCl, 280 bbls CO2"  "Fractotals pumped 95.6 bbls CO2, 136.6 bbls KCl"  "Frac.using 75Q foamtotals pumped 158 bbls CO2, 131 bbls KCl"  "Frac-breakdown w/6.3 bbls KClPumped 70Q foam pad 50Q san stagesTotals pumped 125 bbls KCl,	No
24 1 42	2.2 WR 3				47.57	20.0		7.04	ĺ				lo.	017	120 bbls CO2"	b.r.
24-1 43.	2.2 WK 3	23/20			L .			<u>-</u> _	<u>                                     </u>		<u>L</u> .	<u>.</u>	<u>.</u> .	817	Producing in Wind River Formation. Six perforated intervals from 1418' to 2964'. No information provided on stimulation.	INO
32-1 37	1.9 WR 3	/23/20	01		9.26 2	2.0		5.45		X			0	102	"Fracusing 165 bbls wf 130 in 6% kcl water w/10% methanol + adds, 39 tons CO2458 bbls 70Q CO2 foam. Flush w/18 bbls 6% kcl water w/10% methanol."	
	535.8 W	R 3/2	3/2001		9.65 2	.4		5.86		X	<del>  </del>		·		"Fracusing 153 bbls wf 130 in 6% Kkcl water w/10% methanol + adds, 35 tons CO2398 bbls 70Q CO2	
	648 WF	3/23	2001		12.89	21.9		8.14		X	<del>  </del>		ļ	<b> </b>	foam. Flush w/27 bbls 6% kcl water w/10% methanol."  "Fracusing 105 bbls wf 130 in 6% kcl w/10% methanol + adds, 21 tons CO2232 bbls 70Q CO2 foam.  Flush w/32 bbl 6% kcl water w/10% methanol "	
	856.5 W	R 3/2	2/2001		8.69 2	.0		7.29		X	<del>  </del>				Flush w/32 bbl 6% kcl water w/10% methanol."  "Fracusing 144.4 bbls wf 130 in 6% KCl water w/10% methanol + adds, 29 tons CO2333 bbls 70Q CO2 foam. Flush w/43.8 bbl kcl water w/10% methanol."	2
	917.4 W	R 3/2	0/2001		15.72	30.0		9.47	<u> </u>	X	<del>  </del>				"Fracusing 177.3 bbls wf 130 in 6% kcl w/10% methanol + adds, 38 tons CO2332 bbls 70Q CO2 foam. Flush w/46 bbls 6% kcl w/10% methanol."	
34-2 38:	5.3 WR 3	20/20	01		8.46 1	8.0		6.00		X			0	414	"Fracusing 92.1 bbls wf 130 in 6% kcl w/10% methanol, 20 ton CO2228 bbls 70Q CO2 foam. Flush w/18.5 bbls 6% kcl w/10% methanol.	No
	469.4 W	R 3/1	7/2001		10.85	19.9		7.58		X					"Fracusing 70.8 bbls wf 130 in 6% kcl w/10% methanol, 14 ton CO2149 bbls 70Q CO2 foam. Flush w/23.5 bbls 6% kcl w/10% methanol."	

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation		MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (hpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	497.4 W	R 3/1	7/2001	7	7.47 1	8.0		5.10		X					"Fracusing 75.9 bbls wf 130 in 6% kcl w/10% methanol + adds, 14 ton CO2160 bbls 70Q CO2 foam.	
	554.7 W	R 3/1	7/2001		10.98	19.0		7.58		X					Flush w/24 bbls 6% kcl water w/10% methanol."  "Fracusing 85.2 bbls wf 130 in 6% kcl water w/10% methanol + adds, 19 ton CO2180 bbls 70Q CO2	
	609.9 W	R 3/1	7/2001		10.81	21.0		8.02		X	<del>  </del>				foam. Flush w/28 bbls 6% kcl water w/10% methanol." "Fracusing 175.3 bbls wf 130 in 6% kcl w/10% methanol + adds, 47.7 ton CO2460 bbls 70Q CO2 foam. Flush w/31 bbls 6% kcl water w/10% methanol."	
	648.6 W	R 3/1	7/2001		7.11 2	2.0		6.57	·	X	<del>  </del>		†		"Frac using 136.3 bbls wf 130 in 6% kel water w/10% methanol + adds, 31 tons CO2335 bbls 70Q CO2	1
	7777	TS 0.71	6/2001		7.00.0		ļ	5.50-	ļ	. <del>.</del>	ļļ		ļ		foam. Flush w/33 bbls 8% kcl water w/10% methanol."	<b>  </b>
	714.5 W	K 3/1	6/2001	ľ	7.08 2	2.0		5.72		X					"Fracusing 190 bbls wf 130 in 6% kcl w/10% methanol + adds, 51.2 ton CO2498 bbls 70Q CO2 foam. Flush w/36 bbls 6% kcl w/10% methanol."	
	793.1 W	R 3/1	5/2001		13.44	20.0		8.89		Χ	11		†		"Fracusing 134 bbls wf 130 in 6% kcl w/10% methanol + adds, 21.5 ton CO2242 bbls 70Q CO2 foam.	1
	843.1 W	D 2/1	5/2001		10.24	22.0	ļ	7.89			<b>∤</b> ∤		ļ		Flush w/40 bbls 6% kcl w/10% methanol."  "Fracusing 86 bbls wf 130 in 6% kcl w/10% methanol + adds, 17 ton CO2157 bbls 70Q CO2 foam.	
	843.1 W	K 3/1	5/2001	ľ	10.24	22.0		7.89		А					Flush w/43 bbls 6% kcl water w/10% methanol."	
	900.4 W	R 3/1	5/2001		12.35	23.7	1	8.20		X	11		ļ		"Fracusing 128.4 bbls wf 130 in 6% kcl w/10% methanol + adds, 31 ton CO2283 bbls 70Q CO2 foam.	11
	986.6 W	R 3/1	5/2001		10.81	30.0		7.54		X					Flush w/46 bbls 6% kcl w/10% methanol."  "Fracusing 105 bbls wf 130 in 6% kcl w/10% methanol + adds, 20 ton CO2192 bbls 70Q CO2 foam.	
12-6				_						<u> </u>			n	1 696 Dr	Flush w/50 bbls 6% kcl water w/10% methanol."  ducing from Wind River Formation. Information on perforation and stimulation missing from well	No
12-0													O	1,000 11	completion report	140
44-1		WR											0	1,375 Pr	oducing fro m Wind River Formations (8 perforated intervals). Information on stimulation missing from	No
14.10.63	0.5.1170	4 (1.1.10	1001		14.00	21.0		0.07		37 1	A 5 C	2.670		2 225 115	well completion report.	N.T.
14-10 63	9.5 WK	4/11/2	(001		14.09	21.9		8.27		X 1	Ψ,36 <u>1</u>	3,678		3,225 "F	racusing 102.8 bbls wf 130 in 6% KCl w/10% methanol + adds, 24 tons CO2219 bbls 70Q CO2 foam. Flush w/31 bbls 6% kcl water w/10% methanol."	No
	662 WR	4/11/	2001		10.81	20.4		6.89		X 1	1,11	;			"Fracusing 112.6 bbbls wf 130 in 6% KCl w/10% methanol + adds, 25 tons CO2219 bbl 70Q CO2 foam. Flush w/42.2 bbls 6% kcl water w/10% methanol."	
	872.3 W	R 4/1	1/2001		9.83 20	0.5	1	7.31		X 2	<b>0</b> ,34				"Fracusing 171.6 bbls wf 130 in 6% KCl water w/10% methanol + adds, 42 tons CO2397 bbls 70Q CO2	2
	931.5 W	D 4/1	1/2001		17.03	20.0	ļ	8.62		v	0,454		ļ <u>.</u>		foam. Flush w/44.5 bbls 6% kcl water w/10% methanol."  "Fracusing 121.6 bbls wf 130 in 6% kcl water w/10% methanol + adds, 24 tons CO2224 bbls 70Q CO2	
	931.5 W	10.4/1	1/2001	ľ	17.03	20.0		8.02		A 1	V,43	•			foam. Flush w/47 bbls 6% kcl water w/10% methanol."	
13-15 65	.1 WR 5	/17/2	001 15.86	٥	9.91 2:	5.8		8.76		X 1	3,21	0		0	"Fracusing 120.2 bbls Wf125 in 8% KCl with 10% methanol, 38 tons CO2277 bbls 80Q, 75Q, 70Q, and	l No
	754.7 W	R 5/1	7/2001 5.60 7.	74 23	.8			4.48		X 1	6,44			<b></b>	60Q CO2 foam. Flush w/49 bbls 6% KCL w/10% methanol"  "Fracusing 140.3 bbls Wf 125 in 8% KCl with 10% methanol, 45 tons CO2325 bbls 80Q, 75Q, 70Q,	
	002 1 77	D 675	7/2001 0.06	<u> </u>			ļ	7.07	ļ	37 - 7	1-00		ļ	ļ	and 60Q CO2 foam. Flush w/56.5 bbls 8% KCl w/10% methanol"  "Frac using 138.9 bbls Wf 125 in 6% KCl with 10% methanol, 36 tons CO2270 bbls 80Q, 75Q, 70Q, &	
	893.1 W	K 3/1	7/2001 8.96 8.	31 Z6	.8			7.97		X 1	3,09	,			"Fracusing 138.9 bbls Wt 125 in 6% KCl with 10% methanol, 36 tons CO2270 bbls 80Q, 75Q, 70Q, & 60Q CO2 foam. Flush w/67 bbls 6% KCl w/10% methanol"	
	1048 W.	R 5/10	5/2001 7.76 6.4	17 27	0		1	4.83		X 1	3,29	,			"Fracusing 153.6 bbls Wf 125 in 6% KCl.w/10% methanol, 38 tons CO2277 bbls 80Q, 75Q, 70Q, and 60Q CO2 foam. Flush w/79 bbls 8% KCl w/10% methanol"	
12-11W	70.8 WI	R 5/3/	2001 11.86	٥	9.07 2	1.7		6.87		X			0	460	"Fracusing 144.2 bbls wf 125 in 6% KCl water + adds, 37 tons CO2290 bbls 70Q CO2 foam. Flush w/5	Yes
	843.4 W	R 5/3	/2001 2.76 7.5	1 21.5	5			6.62		X			l	l	bbls 6% KCl w/10% methanol" "Fracusing 120.4 bbls wf 130 in 6% kcl water w/10% methanol + adds, 25 tons CO2180 bbl 70Q CO2 foam. Flush w/63 bbls 6% KCl water w/10% methanol."	

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	864.1 W	R 5/2	/2001 15.17		10.14	22.4		7.69		X					"Fracusing 116.7 bbls wf 130 in 6% KCl water w/10% methanol + adds, 22 tons CO2 170 bbls 70Q CO2 foam. Flush w/65 bbls 6% KCl w/10% methanol."	
	883.3 W	R 5/2	/2001 9.79 1	4.11		23.0		7.98		X	<del>  </del>				"Fracusing 131.2 bbls wf 130 in 6% KCl w/10% methanol + adds, 24 tons CO2223 bbls 70Q CO2 foam. Flush w/66 bbls 6% KCl water w/10% methanol."	
			/2001 7.24 1	0.99		20.0		7.72		X					"Fracusing 146.4 bbls wf 130 in 6% KCl water w/10% methanol + adds, 27 tons CO2251 bbls 70Q CO2 foam. Flush w/69 bbls KCl water w/10% methanol."	
34-3R 72	6.3 WR 773.6 W				10.72 11.13		<u> </u>	8.96 7.93		X X			2	1,153 "5	Start frac & pump 86 bbl 80 Q CO2 foamLeak on wellhead. Flush w/37 bbl kcl waterStart to frac againLeak on wellhead againFrac using 67.7 bbl wf 125 in 6% kcl water w/10% methanol + adds, 16 tons CO2119 bbl 80Q CO2 foam. Flush w/37 bbl 6% kcl water w/10% methanol."  "Fracusing 101.6 bbls wf 130 in 6% kcl w/10% methanol + adds, 24 tons CO2207 bbls 70Q CO2 foam.	Yes
	809.2 W	R 5/4	/2001 16.84		13.48	27.2		8.55		X	╂├				Flush w/39.4 bbls 6% KCl water w/10% methanol."  "Fracusing 127.4 bbl wf 130 in 6% KCl water w/10% methanol + adds, 33 tons CO2288 bbl 70Q CO2 foam. Flush w/41.3 bbls 6% KCl water w/10% methanol"	
	842.5 W	R 5/4	/2001 13.93		13.33			8.69		Χ	† <u> </u>				"Fracusing 108.8 bbl wf 130 in 6% KCl water w/10% methanol + adds, 29 tons CO226 bbls 70Q CO2 foam. Flush w/43 bbls 6% KCl water w/10% methanol."	
	942.7 W	R 5/4	/2001		11.84	21.5		9.65		Χ					"Fracusing 103.6 bbls WF 130 in 6% KCl water w/10% methanol + adds, 22 tons CO2170 bbl 70Q CO2 foam. Flush w/48 bbls 6% KCl water w/10% methanol"	
11-11 102	4 FU 5/				19.85		1	9.45			0,818	0		9,051 "I	Fracusing 161.2 bbls Wf 125 in 6% KCl water w/10% methanol, 45 tons CO2441 bbls 70Q & 60Q CO2 foam. Flush w/50 bbls 50% CO2 & 50% - 6% KCl water w/10% methanol."	Yes
	1169 FU				20.68	28.7		5.17		X 2	1,881				"Fracusing 200.3 bbls Wf 125 in 6% KCl water w/10% methanol, 50 tons CO2466 bbls 70Q & 60Q CO2 foam. Flush w/58.5 bbls 6% KCl water w/10% methanol."	
			/2001 24.82		18.73	J		13.44			\$,708				"Fracusing 178.5 bbls Wf 125 in 6% KCl water w/10% methanol, 41 tons CO2372 bbls 70Q & 60Q CO2 foam. Flush w/62.5 bbls 6% KCl water w/10% methanol."	
			/2001 9.31 1			22.3		10.82		X 1	2,146	•			"Fracusing 153.1 bbls Wf 125 in 6% KCl water w/10% methanol, 28 tons CO2262 bbls 70Q & 60Q CO2 foam. Flush w/68 bbls 6% KCl water w/10% methanol."	
	1380 FU	5/11	/2001 24.34		21.35	24.0				X 1	6,594				"Fracusing 85.2 bbls Wf 125 in 6% KCl water w/10% methanol + adds, 45 tons CO2334.8 [bbls] 80Q, 75Q, 70Q & 60Q CO2 foam. Screened out."	
	1394 FU	5/11	/2001 24.61		15.49	25.4		9.85		X 1	2,207				Fracusing 136.2 bbls Wf 125 in 6% KCl water w/10% methanol + adds, 38 tons CO2258 bbls 80Q, 75Q, 70Q & 60Q CO2 foam. Flush w/70 bbls 6% KCl water w/10% methanol."	
	1467 FU	5/9/2	2001 20.51		15.55	28.5		8.41		X 1	8,033				"Fracusing 178 bbls Wf 125 in 6% KCl water w/10% methanol + adds, 58 tons CO2417 bbls 80Q, 75Q, 70Q & 60Q CO2 foam. Flush w/70 bbls 6% KCl water w/10% methanol."	,
12-5 571.	2 WR 5/	22/20	01		12.41			6.50		Χ			0	3,402 "I	racusing 45.5 bbls 6% KCl w/10% methanol + 40 bbls CO2"	No
	609.6 W	/R 5/2	2/2001		13.48	31.0		7.63		X 1	3,291				"Fracusing 134.4 bbls WF125 in 6% KCl w/10% methanol, 40 tons CO2332 bbls 70Q & 60 CO2 foam. Flush w/30.8 bbls 6% KCl water w/10% methanol."	
	665.4 W	R 5/2	2/2001		15.55	29.4		7.72		X 1	2,788				"Fracusing 119 bbls WF125 in 6% KCl w/10% methanol, 32 tons CO2267 bbls 70Q & 60Q CO2 foam. Flush w/33 7 bbls 6% KCl w/10% methanol "	
	748.9 W				15.50	]		7.93	L		<b>0</b> ,389	,	ļ		"Fracusing 104.4 bbls 125 in 6% KCl w/10% methanol, 21 tons CO2209 bbls 70Q & 60Q CO2 foam. Flush w/38 bbls 6% KCl water w/10 % methanol"	
	829.1 W				9.65 3			6.34		X 0					"Breakdown perfs w/6% KCL, 35 bblsstart ball sealers. Pump48 bbls 6% KCLFlush w/17 bbls 6% KClNo gas."	
13-12 66	1.4 WR (	\$/1/20	01		11.64	21.7	12.27	8.41		X 8	504	)		221	"Fracusing 87.9 bbls wf 125 in 6% KCl water w/10% methanol, 21 tons CO2170 bbls 70Q & 60 Q CO2 foam. Flush w/33 bbls 6% KCl water w/10% methanol"	Yes

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	706.2 W 755 WE 841.6 W 878.7 W	R 6/1/2 R 6/1/2 R 6/1	/2001 001 /2001 /2001		16.89 14.15	17.9 26.3 20.8	18.96 19.22 17.58 18.13 17.58	9.50 7.87		X 5 X 1 X 8	4,989 377 2,31 335 4,71	3			"Fracusing 135.2 bbls wf 125 in 6% KCl water w/10% methanol, 35 tons CO2323 bbls 70Q & 60Q CO2 foam. Flush w/36 bbls 6% KCl water w/10% methanol"  "Fracusing 76.1 bbls wf 125 in 6% KCl water w/10% methanol, 14 tons CO2118 bbls 70Q & 60Q CO2 foam. Flush w/38.5 bbls 6% KCl water w/10% methanol"  "Fracusing 125.4 bbls wf 125 in 6% KCl water w/10% methanol, 24 tons CO2258 bbls 70Q & 60Q CO2 foam. Flush w/43 bbls 6% KCl water w/10% methanol"  "Fracusing 102.6 bbls wf 125 in 6% KCl water w/10% methanol"  "Fracusing 102.6 bbls wf 125 in 6% KCl water w/10% methanol"  "Fracusing 145.4 bbls wf 125 in 6% KCl water w/10% methanol"  "Fracusing 145.4 bbls wf 125 in 6% KCl water w/10% methanol"	
34-11		WR WR											2	1,227 P	Producing fr om Wind River Formation with 9 perforated intervals. Information on stimulation missing from well completion report.  Produced in Wind River Formation (7 perforated intervals). Information on stimulation missing from well completion report.	No No
	71.8 WR 8 655.9 W 689.5 W 785.2 W 922.9 W	R 8/3 R 8/2 R 8/2 R 8/1	/2001 /2001 /2001 /2001		12.07 12.07 10.72 16.24 17.24 24.13 25.86	25.0 25.0 30.0		7.45 7.13 8.87 9.13		X 1 X 1 X 1 X 8	0,17 1,83 5,51 233 4,89 3,97	5 7 5 3 6		9,066 "	"Frac70Q CO2 foam68 bbls KCl, 113 bbls CO2"  "Frac70Q CO2 foam87 bbls KCl, 117 bbls CO2"  "Frac-pump 70Q CO2 foam88 bbls KCl, 152 bbls CO2"  "Frac-pump 70Q CO2 foam121 bbls KCl, 183 bbls CO2"  "Frac-pump 70Q foam92 bbls KCl, 183 bbls CO2"  "Frac-pump 70Q foam92 bbls KCl, 99 bbls CO2"  "Frac-Breakdown w/8 bbl s KClPumped 70Q CO2 foam frac using145 bbls KCl, 228 bbls CO2"  "Frac-Breakdown w/4 bbls KClPumped 70Q CO2 foam frac using226 bbls KCl, 316 bbls CO2"	No No
	1447 FU 1471 FU 1539 FU 1570 FU	8/8// 8/8// 6/1// 7/31	23.44 2001 7.54 17.9 2001 20.45 2001 19.04 2001 18.37	93	26.20	30.0		6.88 2.59 3.48		X 1 X 1 X 6 X 9	0,97 3,75 3,75 ,832 0,16	7			"Frac-Breakdown w/4 bbls KClPumped 70Q CO2 foam frac using124 bbls KCl, 139 bbls CO2"  "Frac-Breakdown w/6 bbls KClPumped 70Q CO2 foam frac using144 bbls KCl, 139 bbls CO2"  "Frac-Breakdown w/60 bbls KClPumped 70Q CO2 foam frac using162 bbls KCl, 172 bls CO2"  "Frac-Breakdown w/12 bbls 6% KClPumped 70Q CO2 frac using141 bbls KCl, 146 bbls CO2"  "Frac-Breakdown w/12 bbls 6% KClPumped 70Q CO2 foam frac using 74 bbls 6% KCl126 bbls CO2screened out w/6 bbls of the 4 PPA & 32 bbls of 6 PPA left in csg. Pumped 70.4 bbls 6% KCl & screened out again".  "Frac-Breakdown w/16 bbls 6% KCl Pumped 70Q CO2 foam using 204 bbls 6% KCl242 bbls CO2"	
43-1 622		7/26 1/200	/2001 8.96 1 11.72		13.84 12.87	<u></u>		3.45 7.58 7.33		X 0 X 6		12 8,500	) "Frac	using	"Pump 10 bbls 8% KCl into formation"  6 9.2 bbls W F 125 in 6% KCl water, 15 tons CO2147 bbls 70Q and 60Q CO2 foam. Flush w/31 bbls 6% KCL water"  "Frac using 79.4 bbls WF 125 in 6% KCl water, 20 tons CO2174 bbls 70Q and 60Q CO2 foam. Flush	No
		/R 8/3	1/2001 1/2001 8.96 1 9/2001 13.65	7.21	14.21 15.32	27.7		7.28 8.69 11.45		X 1	508 6,48 4,42	0			w/33.5 bbls 6% KCL water"  "Fracusing 89.1 bbls WF 125 in 6% KCl water, 23 tons CO2222 bbls 70Q and 60Q CO2 foam. Flush w/35 bbls 6% KCL water"  "Fracusing 124.8 bbls WF 125 in 6% KCl water, 41 tons CO2357 bbls 70Q and 60Q CO2 foam. Flush w/39 bbls 6% KCL water"  "Fracusing 112.1 bbls WF 125 in 6% KCl water, 32 tons CO2289 bbls 70Q and 60Q CO2 foam. Flush w/45 bbls 6% KCL water"	
33-1													0	3,176 P	Producing in W ind River Formation (10 perforated intervals). Information on stimulaton missing from well completion report.	No

Well Abbreviation	of Stimulation rval (m bgs)	Completion or Stimulated Formation	Stimulation Date	ık Down Pressure a)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Stimulation	Proppant (kg or sxs sand)	Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
Well	Top	Con	Stin	Break (MPa)	Ave	Ave	Max	Insta	Frac	Hyd	Acid	Prof	10	Proc	Posson Notice Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control of Control	WO
12-7													0	118	Producing in Wind River Formation (6 perforated intervals). Information on stimulation missing from well completion report.	No
21-10W	585.5 W	R 9/1:	/2001		18.02	19.1		8.80		X 1	6,24	5 0		21,102 '	Fracusing 108.6 bbls YF 125 LG in 6% kcl wtr, 30 tons CO2287 bbls 70Q & 60Q CO2 foam. Flush	No
	645.9 W	R 9/1	5/2001		15.44	28.0		8.62		X 1	1 12,67	ļ	·		w/28 bbls 50/50 6% kcl wtr & CO2".  "Fracusing 101.4 bbls YF 125 LG in 6% kcl wtr, 22 tons CO2241 bbls 70Q & 60Q CO2 foam. Flush	
	760.8 W	R 9/1	5/2001		16.24	26.9		7.67		X 1	   <b>8</b> ,49	] 3			w/32 bbls 6% kcl wtr." "Fracusing 139.5 bbls YF 125 LG in 6% kcl wtr, 38 tons CO2342 bbls 70Q & 60Q CO2 foam. Flush	
	850.1 W	R 9/1	5/2001		10.64	21.2		7.29		X 7	, 439				w/38 bbls 6% kcl wtr".  "Fracusing 91.9 bbls wf 125 in 6% KCl wtr, 22 tons CO2176 bbls 70Q & 60Q foam. Flush w/42.3 bbls	
	914.4 W	R 9/1	4/2001		20.39	12.4		ļ		X 8	3,9ōō				6% kcl wtr"  "Fracusing 88.5 bbls wf 125 in 6% KCl wtr, 20 tons CO2166 bbls 70Q & 60 Q foam. Flush w/43 bbls 6% KCl water"	
	1062 FU	9/14	/2001		16.80	25.8		9.45		X 1	4,36	9			"Frac132.4 bbls wf 125 in 6% kcl wtr, 36 tons CO2289 bbls 70Q & 60Q foam. Flush w/53 bbls 6% kcl wtr"	
	1134 FU	9/14	/2001		14.53	30.9		5.45		X 2	28,03	8			"Fracusing 214.9 bblswf 125 in 6% kcl wtr, 72 tons CO2615 bbls 70Q & 60Q foam. Flush w/57 bbls	
	1291 FU	9/14	/2001		17.11	27.6		7.98		X 2	21,81	i i			6% kcl wtr"  "Fracuisng 184.3 bbls wf 125 in 6% kcl wtr, 59 tons CO2536 bbls 70Q & 60Q CO2 foam. Flush w/65 bbls 6% kcl wtr."	
23-12 52			001 11.48		17.93			7.45 8.83 8.07 8.68			7,03			139	"totals pumped 112 bbls KCl, 218 bbls CO2"	Yes
	712.6 W	R 9/1	9/2001 17.17 9/2001 16.89	·	15.51 15.17	25.0		8.07		X 7	3,07 , <mark>459</mark>	<b>*</b>	·		"totals pumped 118 bbls KCl, 180 bbls CO2" "totals pumped 78 bbls KCl, 83 bbls CO2"	
			9/2001 13.51		20.68	26.0		8.68		X 1	],05	þ.			"totals pumped 106 bbls KCl, 134 bbls CO2"	
			9/2001 20.12		17.24	_		0.00			1,01			1	"totals pumped 111 bbls KCl, 134.6 bbls CO2"	
44-2 609			18.85 2001 15.51		13.04 10.63			8.20 6.76 6.89 8.00 8.62		X 7	,042 4,22	<u> </u>		198	"Totals pumped 58 KCl, 88 CO2"  "Totals pumped 107 KCl, 162 CO2"	.No
	753 5 W	R 9/2	1/2001 24 87		11.91			6.89	·	X	7,22 3,16	ž	·		"Totals pumped 107 KCi, 162 CO2"	·
	783 WF	9/21	2001 21.57		17.20	28.3		8.00		X 2	3,16 3,33	6	·		"Totals pumped 119 bbls KCl, 180 CO2" "Totals pumped 164 bbls KCl, 272 CO2"	11
	921.7 W	R 9/2	1/2001 22.7	· .	13.93	22.0		8.62		X 8	3,091				"Frac-pumped WF 125 70QLoar XO2 pumpwent to flush early to prevent screen out. Totals pumped	]]
	1122 E	1 0/20	V2001 21.68		19.31	24.0		6.55		V 1	] [3,18	<u>.</u>			105 bbls KCl, 116 bbls CO2"  "Frac-pumped WF 125 70QTotals pumped 131 bbls KCl, 152 bbls CO2"	
31-9 705				26.10		_					,382			1.346 "6		Yes
31-9 703	802.2 W	R 10	18/2001					9 33		X 1	1502	<u>-</u>		1,340 0	"92 bbls clean fluid, 150.7 bbl CO2"	1 68
	829.7 W	R 10		28.19	15.31 14.51	22.7		9.86		Χ e	1,66 5,924	ř	·		"82 bbls clean fluid, 81.6 bbl CO2"	
			18/2001	24.71		23.0		10.55 9.33 9.86 12.09 26.09		Χ 7	022		[		"Total clean fluid 95 bbls, 108.1 bbls CO2"	
			18/2001	17.11	15.81	20.0		26.09		X 7	154				"Total clean fluid 87 bbls and 89.4 bbl CO2"	
34-10 1			01 19.51				28.91		ļ	$X = \frac{1}{2}$	7,55	В 5 	ļ	4,816 "7	dtal pumped 143 bbls KC 1, 219 bbls CO2"	Yes
	1538 F	10/3	/2001 20.20 /2001 25.51		10.13 19 <i>44</i>	18.9 28.4	26.89 26.45	19.10 9.16		X 1	3,437 3,73 6,32	ļ	<b>}</b>		"Total pumped 120 bbls KCl, 167 bbls CO2" "Total pumped 136 bbls KCl, 206 bbls CO2"	
	1590 FU	10/3	/2001 25.51		19.65	27.4	19.71	9.65	<b> </b>	X 1	6.32	<u> </u>	<b>†</b>		"Total pumped 156 bbls KCl, 242 bbls CO2"	1
	1639 FU	10/2	/2001 14.48		21.02	33.0	21.02	6.39	<u> </u>	ΧÌ	6,03	5	t		"Total pumped 145 bbls KCl, 230 bbls CO2"	1
	1682 FU	9/26	2001 10.64		16.97	2.0 1	6.97			X 8	3,440		<u> </u>		"Screened out with 8458# in 12/20 sand in csgTotal pump 83.6 KCl,108 bbls CO2"	
34-1 564	.8 WR 1	<b>0</b> /11/2	001	12.37	10.51	21.0	13.13	7.45	L	X 8	,145	0	l	930	"Total pumped 82 bbls KCl, 95 bbls CO2"	No

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
				10.26 11.89						10 10					"Total pumped 93 bbls KCl, 127 bbls CO2" "Totals pumped 98 bbls KCl, 124 bbls CO2"	
				15.58						7					"Frac-WF 125 70QTotals pumped 92 bbls KCl, 87 bbls CO2"	
21-12 5	06 WR 1			7.58 1			24.82		2	18	,001	0		14	"Totals pumped 112 bbls KCl, 223 bbls CO2"	No
				22.93				7.70	[	15	,142				"Totals pumped 107 bbls KCl, 180 bbls CO2".	
				12.74 19.99				6.89 11.20		7. 1					"Totals pumped 67 bbls KCl, 104 bbls CO2"  "Totals pumped 105 bbls KCl, 134 bbls CO2"	
12-10 7	26.6 WR			7.58 1			18.62			13		2		1,465 "]	Gtals pumped 102 bbls K CL, 196 bbls CO2"	No
	790 W			14.48					2	7,	244				"Frac-WF 125 70Q CO2 foam fracscreened out w/6032#Totals pumbed 53 bbls 6% KCl, 86 bbls CO2"	
12-1 60	5.6 WR 1		001	18.24	13.79	25.0		9.10 6.34 9.40 13.51		9,0	)66	)		653	"Totals pumped 70 bbls KCl, 111 bbls CO2"	No
			/10/2001 /9/2001 21.0:	ţ	12.76 21.72	30.0 28.0		6.34 9.40		10 10	,46) 928				"Totals pumped 99 bbls KCl, 131 bbls CO2"  "Totals pumped 88 bbls KCl, 153 bbls CO2"	
			9/2001 19.82		19.99	25.0		13.51	<u> </u>	7	148				"Totals pumped 93 bbls KCl, 83 bbls CO2"	
42-3 43			05 12.69					7.43 2			978 (	)		1,675 "I	rnc w/64 bbls slickwater"	No
	507.8 V	MR 1/2	9/2005 11.3	6 				6.92 2 7.51 2	3.75	6.8	312				"Frac w/100 bbls slickwater"	
	727.6 V	MR 11	2005 14.34 14/2001					7.31 Z 9.14	1.04	8	718				"Frac w/93 bbls slickwater" "Frac w/68 bbls KCl, 103 bbls CO2"	
	774.8 V	MR 11	13/2001					9.14 12.20 9.51	[	6, 8, 7, 12	944				"Frac w/67 bbls KCl, 110 bbls CO2"	-
	850.4 V 1109 F	MR 11	8/2001					9.51 17.53	[	12 7	,77 <b>5</b>				Frac w/95 bbls KCl, 163 bbls CO2	
22 1 62	1109 F 5.7 WR 1			1				17.53	2	6,8				892	"Frac w/72 bbls KCl, 110 bbls CO2"  "Frac w/168 bbl 75Q CO2 foam"	No
22-1 02	687.6 V							ļ		10				092	"Frac w/197 bbl 75Q CO2 foam"	
33-10W	1064 FU	J 12/1/	2001 24.13					12.34	2	( 9)	929 2	2		8,228 "I	rac-BD w/6% KClPmp 230 bbl 70Q WF-125 CO2 foamTotal fluid 104, CO2 tons. Stimulation report indicates that 70Q CO2 WF-125 foam and fluids used contained Biocide B69, Surfactant EZEFLO F103, Foaming Agent F104, Breaker J218, Breaker Aid Liquid J318, Slurry PSG Polymer J877, Clay Stabilizer L55.  "Start 70Q CO2, 310 bbl"	Yes
	1170 F	U 12/1	30/2001 10/2004					[		0					"Breakdown w Linear gel"	
	1191 F 1368 F			7.93 2	02	30.0		10.96	<u></u>	0	227				"Breakdown w Linear gel"	
				22.30					} <u> </u>		,337 ,560				"Total pumped 113 bbls KCl, 163 bbls CO2"  "Total pumped 172 bbls KCl, 229 bbls CO2"	
				21.55	21.93			9.65 9.65	2	1					"Total pumped 154 bbls KCl, 154 bbls CO2"	
41-3 40	2.9 WR 2							4.27 2	Φ.36 Z	6,	285	)		29	"Frac w/77 bbl slickwater"	No
	534.9 \	MR 12	/6/2001 19.39 1/2005 25.07	9 	14.48	25.0		8.48 7.52 2	3 30 - 5	5, 6,9	126				"Frac-BD w/6% KClStart 70Q CO2 143 bbls75 bbls water, 14 ton CO2" "Frac w/86 bbl slickwater"	
	595 W	MR 2/ R 1/28	2005 26.10	<b></b>				7.32 2. 8.79 2	7.30   2 5.11   5	6,	557				"Frac w/86 bbl slickwater"  "Frac w/93 bbl slickwater"	
	613.9 \	MR 1/2	6/2005 17.2	ş				8 55 2	1 98	71	799			<u> </u>	"Frac w/108 bbl slickwater"	
	731.8 V	MR 1/2	2/2005 28.2		17.00	105.0		10.74	24.88 Z	8	196				"Frac w/104 bbl slickwater" "Frac-BD w/6% KCl Start 70Q CO2 170 bbl22 ton CO2."	
	851 W	MK 12 R 12/5	/5/2001 27.8: /2001 18.53	<b>}</b>	17.93 20.68	25.0 30.0		10.55 8.72	}  ₂	8,0	571 571				"Frac-BD w/6% KClStart 70Q CO2 170 bbl22 ton CO2."  "Frac-BD w/6% KClStart 70Q CO2 211 bbls109 bbl fluid & 20 ton CO2"	
	1065 F	t 12/4	1/2001 25.86		20.68			10.82	[	9, 8,0	008		 	<u> </u>	"Frac-BD w/6% KClPump 233 70Q CO2 foam24 ton CO2, 129 bbl fluid."	·]

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	1120 FU				19.65 18.27			10.55		X 5,	139 1,14	I			"Frac-Breakdown 29 bbl 6% KClStart 70Q CO2 foam 162 bbls57 bbls fluid & 19 ton CO221 bbls flush screened out w/4410# 6# sand in formation."  "Frac w/6% KClStart 70Q CO2 foam, 235 bbls slurryflush 57 bbl 50Q foam32 ton CO2, 140 bbl 6% KCl."	
22-11 56	730.9 W 845.5 W 905.6 W	R 12 R 12 R 12 R 12	15/2001 14/2001 14/2001 14/2001	12.83 20.20 26.54 16.20 24.15	13.79 13.79 22.06	35.0 30.0 30.1 33.0	5 23.44	7.38 6.83 8.08 0.00	2	X 10 X 10 X 0	303	i		306	"Frac-Start 75Q foampump 197 bbls foam25 tons CO2, 67 bbls fluid"  "Frac-Breakdown w/6% KCIStart 75Q CO2 foam 281 bbls, 31 tons CO2, 137 gel"  "Frac-BreakdownTotals pumped 93 bbls KCl, 134 bbls CO2"  "Fracpsi increasded to 4373-bled well down, psi continued to climb to 4007 shut down job. Pumped 87 bbls KCl & 96 bls CO2"  "FracTotals pumped 146 bbls KCl, 149 bbls CO2"	No
43-11 50	7.2 WR 1 589.5 W 734.9 W	/4/20 R 1/4 R 1/4 R 1/4 1/3//		1.37	I	37.0 30.0 35.0 35.0 32.0 32.5		8.23 9.17 6.89 8.80 8.91 4.90 5.91		X 6, X 7,	059 684 2,221	. <b></b> .	0	140	"Frac-Pump 41 bbls KCl, 85.7 bbls CO2Screened out w/3227# in formation, 9219# in csg"  "Frac-Breakdown w/6%KClStart 75Q CO2, 411 bbls foam, 123 bbls fluid, 44 tons CO2"  "Frac-Breakdown w/6% KClStart 75Q CO2, 202.5 bbls fluid, 20 ton CO2"  "Frac-Breakdown w/6% KClStart 75Q CO2, 243 bbls, 97 bbls fluid, 23 tons CO2"  "Frac-Breakdwon w/6% KClStart 75Q CO2 foam, 143 bbls fluid, 26 tons CO2"  "Frac-Break down w/6% KClStart 70Q CO2 frac, 299 bbls, 136 fluid, 28 tons CO2"  "Frac-Break down w/6% KClStart 70Q foam 306 bbls, 157 bbls gel, 25 tons CO2"  "Frac-Break w/6% KClStart 70Q foam 881 bbls, 275 bbls gel, 97 tons CO2"	No
	.9 WR 12 804.7 W 899.8 W 1167 FU	/12/2 R 12/ R 12/ 12/6	001 12/2001 12/2001 /2001 29.30	26.89 18.68 19.08	15.86 15.17 18.62 24.13	25.0 25.0 25.0 27.0		7.45 8.66 8.63	2	X 5, X 7, X 7, X 7,	648 983 888 121	1		1,895 "]	Fric-Break w/6% KCKSta rt w/168 bbls 75Q CO2 foam, 17 ton CO2, 60 bbls of fluid"  "Frac-Break w/6% KCIStart w/180 bbls 75Q CO2, 19 ton CO2, 96 bbls wtr"  "Frac-Break w/6% KCIStart w/169 bbls 75Q CO2 foam, 51 bbl gel, 19 ton CO2"  "Frac-Break down w/6% KCIStart 70Q CO2 185 bbls20 tons CO2, 55 bbl gelScreened out 4161 in formation, 11540 in pipe Re-frac break w/6% KCl 50 bbls. Start 337 bbl 75Q foam, 36 ton CO2, 147 bbl fluidscreened out w/12331 in formation, 5867# in pipe"	No
41-10 49	661.7 W 766.9 W	R 1/2 R 1/1	002 15.72 0/2002 19.2 9/2002 17.6 9/2002 11.8	7 5	14.48 13.79 14.48  15.86	35.0 30.0		6.89 7.86 8.48  7.14		X 1 X 9,	1,832 1,104 525 1,118	1		157	"Frac-Break w/6% KCL Start 75Q CO2, 70 bbls fluid, 28 ton CO2 flush 24 bbls 50/50"  "Frac-Break down w/6% KCL Start 75Q foam, 96 bbls gel, 27 ton CO2 32 bbls 6% KCl flush"  "Frac-Break down w/6% KCL Start 75Q 208 bbls, foam 63.5 bbls, 26 ton CO2 flush 37 bbls 50/50 flush"  "Frac-Break down w/6% KCL Start 75Q foam 228 bbl, 64.5 fluid, 26 ton CO2 Flush w/40.5 bbls 6% KCl"	Yes
	863.8 W 959.5 W	R 1/1 R 1/1	9/2002 11.0 9/2002 18.6 9/2002 16.1	2 3	15.86 13.79 14.48	25.0 25.0		6.41 8.96		X 6, X 7,	0,559 562 228				"Frac-Break down w/6% KCLStart 75Q foam 222 bbls, 62.5 bbls fluid, 26 ton CO2 43.5 bbls flush 6% KCl"  "Frac-Break w/6% KCLStart 75Q foam 144 bbls, 44 bbls fluid, 16 ton CO2flush 44.5 bbls 6%"  "Frac-Break down w/6% KClStart 75Q CO2 150 bbl fluid, 18 ton CO2flush 48 bbls 6% KCl"	
13-12W	823.6 W 982.4 W 1052 FU	R 1/2 R 1/2	/2002 18.09 3/2002 15.4 2/2002 19.0 /2002 20.82 /2001 16.55	9 5 	14.48 14.48 18.62 18.62 19.99	30.0 25.0 30.0	29.33	9.10 8.56 6.00		X 6, X 6, X 6,				322	"Frac-Break down w/6% KClStart 75Q foam, 72 bbls fluid, 30 tons CO2 37 bbl 50/50"  "Frac-Break down w/6% KClStart 75Q CO2 foam, 175 bbls, 78 bbl fluid, 16 ton CO2"  "Break w/6% KClStart 75Q foam, 146 bbls, 43 bbl fluid, 17 tons CO2screened out w/7900# in formation, 6340# in pipe"  "Frac-Break w/6% KClStart 70Q foam 258 bbls, 81 bbl fluid, 24 ton CO252 bbl 6% flush"  "Frac-Break w/6% KClStart 70Q CO2 foam, 482 bbls, 142 bbls fluid, 55 ton CO255 bbl flush 6% KCL"	No

ition	ation (s)	Stimulated	ate	ressure	ure During IPa)	during	re During (MPa)	Shut-In	lient	Fracturing		or sxs sand)	ı (ppls)	er (bbls)	n of Stimulation Completion d Sundry	Well File
Well Abbreviation	Top of Stimulati Interval (m bgs)	Completion or Formation	Stimulation Date	Break Down F (MPa)	Average Press Stimulation (A	Average Flow du	Max Pressure Stimulation (A	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradien (MPa/km)	Hydraulic	Acid Stim	Proppant (kg	Oil Production (bbls)	Produced Water	Description from Well C Reports and Notices	WOGCC Review ³¹
24-3B 13	1401 FU 1464 FU 1470 FU	2/6/2 1/30 1/30	2 14.55 2002 25.51 /2002 11.72 /2002 12.09 /2002 12.41		21.37	27.: 35.0 35.0	58 23.24	3.74		X 1	8,835 2 7,156 5,161 5,663 3,287			13,316 "	Frac-Breakdownstart 70Q CO2 foam- 564 bbls, 169 bbls gel, 62 tons CO265 bbl flush 50/50did not screen outmonitored well 24X-3 off set, psi did not increase"  ["Frac-Breakdowntotals pumped 184 bbls KCl, 337 bbls CO2CO2 hose leaking"  ["FracBreakdownTotals pumped 161 bbls KCl, 297 bbls CO2"  ["Frac-BreakdownTotal pumped 207 bbls KCl, 282 bbls CO2"  ["FracBreakdowntotal pumped 190 bbls KCl, 254 bbls CO2"	No
11-11B 4	62.1 524 566.3 659 688.8	WR WR WR WR	2/18/2005 1 2/18/2005 1 2/18/2005 1 2/18/2005 2 2/18/2005 9 2/17/2005 1	2.31 2.79 0.02 6.23 96		33.9 33.9 35.0 35.6 36.3	19.37 20.29 17.01 21.13 17.84 1.31 1	6.48 10.32 7.09 7.04 7.56		X I X X X X X X	7,221 6,550 9,254 8,315 11,269	9	4	13,056	"Frac18 ton of CO2, 63 bbl of clean fluid" "Frac15 tons CO2 and 78 bbls clean fluid" "Frac23 ton CO2 and 95 bbls clean fluid" "Frac19 tons of CO2 and 91 bbls clean fluid" "Frac27 tons of CO2 and 124 bbls clean fluid" "Frac32 ton of CO2, 232 bbls clean fluid"	Yes
	1045 1078	FU FU	2/14/2002 2 2/15/20005 2/14/2002 9 2/13/2002 1	18.73 17 18.0	16.55 52 19.31	35.0		10.02		X X X	4,923 16,08- 10,775 10,600	4 8			"FracBreak w/6% KClFrac using 197 bbls 70Q CO2 foam, 64 bbls gel, 22 ton CO2 Flush w/6% KCl & 50/50 CO2"  "Frac211 bbl clean fluid and 42 ton CO2"  "Frac-Break w/6% KClFrac using 386 bbl 70Q CO2 foam, 140.5 bbls gel, 37 tons CO253.5 bbls 6% flush"  "Frac-Break w/6% KClFrac using 346 bbls 70Q CO2, 138 bbls gel, 33 tons CO2. Flush w/56 bbls 50/50	
31-11 59	1375 1404 1442	FU FU FU	2/12/2002 1 2/9/2002 19 2/12/2005 2 2/9/2002 22 002 10.67	.62 4.13 .85	21.72 19.31 21.37	35.0 35.0		7.61 7.03 7.10		X X X X	11,54 15,569 20,111 9,515 2,955 0	9 8		207	CO2"  "Frac: Break w/6% KClFrac using 70Q CO2 foam, 157 bbls gel, 37 tons CO2 64 bbl flush 50/50."  "Frac: Break w/6% KClFrac w/438 bbls 70Q foam, 145 bbls gel, 50 tons CO2 flush 60% CO2."  "Fracpumped 356 bbl clean fluidand 33 tons CO2"  "Frac: Break w/6% KClFrac w/280 bbls 70Q CO2 foam, 83 bbls gel, 28 tons CO2"  "Frac-BD w/6% KClFrac using 75Q foam, 63 bbls gel, 25 tons CO2 27 bbls 30Q foam flush"	No
	678.2 W 730 WR 774.5 W 808.9 W 1034 FU	R 2/2 2/19/ R 2/1 R 2/1 2/16	0/2002 7.79 2002 21.92 9/2002 13.6 6/2002 7.01 /2002 16.75 /2002 20.93	12.07 5 19.31	13.79 17.93 25.51 18.62	25.0 25.0 30.0 30.0 35.0		6.14 7.58 8.20 8.52 4.96		X 6 X 6 X 9 X 1 X 1	781 715 167 0,883 2,244 1,494				"Frac-BD w/6% KCl Frac using 140 bbls 75Q foam, 41.5 bbls gel, 17 ton CO2flush 32 bbls 6% KCl" "Frac-BD w/6% KCl Frac using 142 bbls 75Q CO2 foam, 41 bbls gel, 16 tons CO236 bbls 6% KCl" "Frac-BD w/6% KCl Frac using 75Q CO2 foam, 92 bbls gel, 23 ton CO2 flush w/38.5 bbls 6% KCl" "Frac-BD w/6% KCl Frac using 75Q foam, 63 bbls gel, 24 ton CO2 flush w/40 bbls 6%" "Frac-BD w/6% KCl Frac using 75Q CO2, 123 bbls gel, 41 tons CO2 "Frac-BD w/6% KCl Frac using 380 bbls 70Q CO2 foam, 112 bbls gel, 45 ton CO254 bbls 6% KCl flush"	
23-3 510	1153 FU 1180 FU	2/15 2/14	/2002 15.03 /2002 15.86 /2002 27.30 02 16.55		9.65 2 15.17 16.20 12.07	30.0 35.0		4.34			2,280 ,741 2			1,202 "F	"Frac-BD w/6% KClFrac using 85 bbls CO2, 25 bbls in formation"  "Frac-BD w/6% KClFrac using 85 bbls 75Q CO2, flush 25 in formationrecover 17 bbls of 85 bbls"  "Frac-BD w/6% KClFrac using 346 bbls 70Q CO2 foam, 104 bbls gel, 39 ton CO2flush w/46 bbls 50/50 + 10 bbls 6% KCl111 of 190 recovered"  rac-BD w/6% KClFrac using 176 bbls 75Q CO2, 44 bbls gel, 20 ton CO223 bbls 6% KCl + CO2	No
	641.9 W 775.4 W 823 WR	R 2/2 R 2/2 2/20/		5	15.17 19.31 15.17	25.0 32.0 27.0		8.89 7.58 9.89		X 8 X 1 X 9	,482 1,113 ,843 0,985				flush" "Frac-BD w/6% KClFrac using 176 bbls 75Q CO2, 52 bbls gel, 20 ton CO230 bbls 6% flush" "Frac-BD w/6% KClFrac using 75Q CO2, 109 bbls gel, 26 ton CO236.5 bbls 6% KCl flush" "Frac-BD w/6% KClFrac using 75Q CO2, 64 bbls gel, 19 ton CO239 bbls 50/50 flushmade recover 122 bbls of 629" "Frac-BD w/6% KClFrac using 75Q CO2, 65.5 bbls gel, 27 ton CO242.5 bbls 6% KCl flush"	

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	1155 FU	2/20	/2002 20.77 /2002 8.27 1 /2002 15.38	8.96	18.27 16.89	35.0		9.17 4.07 5.38		X 6 X 1 X 1	668 1,87 1,94				"Frac-BD w/6% KClFrac using 206 bbls 70Q CO2, 65 bbls gel, 24 ton CO252 bbls 6% KCl flush" "Frac-BD w/6% KClFrac using 492 bbls 70Q CO2, 184 bbls gel, 50 ton CO256 bbls 6% KCl flush" "BD w/6% KClFrac using 70Q CO2, 144 bbls gel, 53 ton CO2flush w/67 bbls 50% CO2"	
32-11 53	603.2 V 721.2 V	R 2/2	002 12.55 6/2002 17.4 6/2002 19.3 6/2002 13.1	Ī	13.79 15.86 13.79 20.68	30.0 30		7.83 5.52 6.79 6.21		X 9 X 9 X 1 X 1	764			1,027 "F1	ac-BD w/6% KClFrac u sing 161 bbls 75Q CO2 foam, 45 bbls gel, 18 ton CO [CO2]24 bbls KCl flush" "Frac-BD w/6% KClFrac using 201 bbls 75Q CO2, 56 bbls gel, 23 ton CO228.5 bbls 6% flush" "Frac-BD w/6% KClFrac using 206 bbls 75Q CO2, 60 bbls gel, 23 tons CO234 bbls 8% flush" "Frac-BD w/6% KClFrac using 273 bbls 70Q CO2, 110 bbls gel, 28 ton CO237.5 bbls 6% flush"	No
	1035 F	R J 2/22	6/2002 13.1 2/23/2002 1 /2002 30.67 /2002 20.34		20.68 12.07 26.20	28		3.35		X 6	218				"Frac-BD w/6% KClFrac using 296 bbls 75Q CO2, 87 gel, 35 ton CO246 bbls 50% CO2 flush"  "Frac-BD w/6% KClFrac using 207 bbls 70Q CO2, 72 bbls gel, 22 tons CO2screened out w/6570# in formation, 7136 in piperecover 122 of 609"  "Frac-BD w/8% KClFrac using 382 bbls 70Q CO2, 121 bbls gel, 43 ton CO254 bbls 6% flush"	
44 11 52	1133 FU 1161 FU	2/22 2/21	/2002 20.34 /2002 26.20 /2002 24.82 /002 19.55		18.96 17.24 17.93	40.0		5.52 4.69 2.34		X 1 X 1 X X 7				1 642 95	"Frac-BD w/8% KClFrac using 352 bbls 76Q CO2, 121 bbls gel, 45 ton CO254 bbls 6% flush"  "Frac-BD w/6% KClFrac using 70Q foam, 164 bbls gel, 59 ton CO257 bbls 6% flush"  "Frac-BD w/6% KClFrac using 50 bbls 75Q foam, flush w/50Q foamTotal fluid 53 bbls, 12 ton CO2, flush 60 bls 50Q foam"  ac-BD w/6% KClFrac using 150 bbls 75Q CO2 foam, 47 bbls gel, 16 tons CO2Flush w/24.5 bbls	NTo
44-11 33	642.8 V	R 2/2 R 2/2	8/2002 14.6 8/2002 20.1 2/28/2002 1	<u> </u>	14.48 15.86 19.17	25.0 35.0		6.62 11.17 1.52		X 6	940 917			1,043 F1	150% CO2"  "Frac-BD w/6% KClFrac using 147 bbls 75Q CO2 foam, 44 bbls gel, 17 ton CO230 bbls 6% flush"  "Frac-BD w/6% KClFrac using 147 bbls 75Q CO2 foam, 44 bbls gel, 17 ton CO230 bbls 6% flush"  "Frac-BD w/6% KClFrac using 152 bbls 75Q CO2 foam [foam], 47 bbls gel, 17 ton CO2"  "Frac-BD w/6% KClFrac using 303 bbls 75Q CO2 foam, 83 bbls gel, 35 ton CO2"	No
	]	J	/2002 29.65 /2002 13.13		13.10 20.68			5.17 6.96	L	X 8	JL	,			"Frac-BD w/6% KClFrac using 245 bbls 70Q CO2 foam, 87.5 bbls gel, 28 ton CO2flush w/54 bbls 6% KCl" "Frac-Breakdown w/6% KClFrac using 620 bbls 70Q CO2 foam, 182 bbls gel, 69 tons CO2flush w/57	
42-9W													5.051	25 202 D	bbls 50% CO2"	No.
32-9W 7	832.1 V 894.9 V 1001 W	R 3/ R 3/ R 3/1	2002 17.42 9/2002 17.2 9/2002 22.2 9/2002 23.92	₹ 3	18.27. 13.10 18.62 26.89	25.0 30.0		6.83 8.76 10.34 10.55		X 1 X 7 X 9 X 9	3,420 487 784 502				oduction in Wind River Formation. 8 perfor ated intervals from 1776-3138.' No information on stimulation ac-BreakPump pad • 28+2 tons GO2, 132.6 load" "Frac-Break formationPump pad17+1 CO2, 105 bbls load" "Frac-Break formationPump pad128 bbls load, 22+1 tons CO2" "Frac-Break formationPump pad103.6 bbls clean fluid, 22+2 tons CO2"	Yes
32-10B 1	1442 FU 1476 FU 1569 FU 1614 FU	3/33 3/21 3/21 3/20	002 10.62 /2002 12.41 /2002 18.13 /2002 13.79 /2002 17.25 /2002 18.96		19.31 19.31 26.54 26.89 22.06 25.51	35.0 34.0 28.0 35.0		3.45 3.79 10.14 6.69		X 1 X 1 X 1	9,39 8,27 8,28	; ; ;	7 "Fra	c-Break	CO2 hose rupt ured during pad/replace. Extend pad 53 bbls97 tons CO2296.4 bbls"  "Frac-fill hole 57 bbls, breakFrac using 62 tons CO2275 bbls"  "Frac-Break formationFrac using67 tons CO2, 198 bbls load"  "Frac-BreakFrac using63 tons CO2, 314 bbls load"  "Frac-BreakFrac using50+2 ton CO2, 318 bbls kel"	Yes
13-11B 1	1716 FU 102 FU	3/20 4/6/20	/2002 17.93		25.51 24.13 19.65 24.13	30.0 35.0		3.52 14.65 5.07 6.83		X 1 X 1 X 7 X 1 X 3 X 1	4,787	0		7,087 "F1	"Frac-BreakFrac-pump pad56+2 ton CO2, 234 kcl" "Frac-Break formationFrac using204 bbls 6% kcl, 23+2 tons CO2"  ac-Breakdown w/6% KClF rac using 70Q CO2 foam, 125 bbls gel, 39 tons CO253 bbls 50% CO2 flush" "Frac-Break w/6% kclFrac using 70Q CO2, 896 bls, 283 bbls gel, 97 ton CO257 bbls 30% CO2 flush" "Frac-Break67 tons CO2+209 bbls load"67 tons CO2, 209 bbls "load"	No

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Avgerage Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	1452 FU	3/23/2002 3/23/2002		20.68 16.55	35.0		8.27 10.48		X 1 X 9	0,851				"Frac-Break formation167 bbls, 34 tons CO2"167 bbls of ?, 34 tons CO2 "Frac-Break formation35 ton CO2 & 175 bbls fluid"35 tons CO2, 175 bbls "fluid"	
		/9/20 <mark>02 8.19 22.7</mark>	_	16.55	37.0		10.48			3,224	3		5 605 "E	ac-Break down w/6% KClFr ac using 70Q CO2. 650 bbls, 183 bbls gel, 70 tons CO286 bbls 50%	Yes
	1408 FU 1538 FU 1578 FU	[9/2002 8.19 22.7] [4/9/2002 7.83 22 [4/9/2002 14.20] [4/6/2002 15.86] [4/5/2002 17.13]	.75	22.75 26.20 27.58	36.0 33.0 27.0		4.48 7.58		X 2	2,290 1,857 ,145			5,695 "F1	"Break down w/6% KC1Frac using 70Q CO2 foam 630 bbls, 174 bbls gel, 70 tons CO286 bbls 50% CO2 flush"  "Breakdown w/6% KClFrac using 70Q CO2 foam 630 bbls, 174 bbls gel, 71 ton CO272 bbls 6% flush"  "Break down w/6% KClFrac using 70Q CO2 faom [foam], 338 bbls, 39 ton CO276 bbls 6% flush"  "Break down w/6% KClFrac using 70Q CO2 209 bbls, 22 ton CO2screened out w/12411# in formation, 3342# in pipe"  "Break down w/6% KClFrac using 206 bbls gel, 20 ton CO2"	
		/29/2001	15.51	27.36	27.0		9.79			4	)		0	"BD w/6% KCl171 bbls 70Q CO254 bbls 6% KCL, 22 ton CO2, 32 bbls 50Q foam"	No
	851 WR	11/29/2001 R 11/29/2001	21.51 28.96	15.17 14.82	25.0		9.24 9.97		X 7 X 8	,763 ( ,385 ,432			Y	"Frac BD w/6% KClstart 70Q CO2 foam 177 bbls41.5 bbls KCl flush" "Frac-BD w/6% KClStart 70Q CO2 foam. 174 bbls81 bbls 6% KCl, 22 ton CO2. Flush w/45 bbls 50Q CO2"	
		11/27/2001	27.58						X 7	1 1				"Break w/6% KC1Start 70Q CO2 foam, 164 bbls slurry pumped17370# 12/20 sand screened out w/11278# in pipe, 6083# in formation. Total 51 bbls no flush pumped"	
23-10W 6	51.1 WI	R 12/14/2002	21.50	24.13	32.0		10.98		X 1	5,987 7,25 i	2		5,892 "F1	ac-Pumped 114 bbls KCl, 219 bbls CO2"	No
			26.24 23.12	17.93	35.0 25.0		10.62			7,251				"Frac-Pumped 136 bbls KCl, 220 bbls CO2" "Frac-Pumped 111 bbls KCl, 138 bbls CO2"	
	1138 FU	R 12/14/2002	12.94	16.89	23.0 30.0		7 27		л 0 Х 7	644				"Frac-Pumped 111 bbls KCl, 138 bbls CO2"	
	1161 FU	12/13/2002 12/13/2002	7.64 20	0.68 22.41	35.0		7.27 4.14		X 2	,644 3,873				"Frac-Pumped 258 bbls KCL, 442 bls CO2"	
			16.33	22.41	35.0		9.65			4,436				"Frac-Pumped 192 bbls KCl, 260 bbls CO2"	
		10/13/2004								741	5		4,554 "Fl	ush w/22 bbls. Scr een out w/2 bbls let on flush"	Yes
	557.2 W	R 10/13/2004 10/13/2004	7.36 13.10				7.62 7.79			,705 <b>0</b> ,550				"Flush w/28 bbls water" "Flush w/34 bbls water"	
		D 10/13/2004	0.57				7.79 7.43		X 1	ψ,33ψ .928				"Flush w/34 bbls water" "Flush w/36 bbls"	
	812 WR	10/13/2004	14.94 11.38 18.34 9.17				7.73			3895 1895			<u> </u>	"Flush w/36 bbls" "Start flush 20 bbls"	·
	864.1 W	R 10/13/2004	11.38	<u> </u>		1	7.45			342		İ	[	"Flush w/43.5 bbls water"	
	927.5 W	R 10/13/2004	18.34				7.45 7.98 7.58			581				"Flush to top perf w/46 bbls water" "Flush to top perf w/48 bbls water"	
	949.8 W	R 10/13/2004 10/4/2004 10.74	9.17				7.58		X 7 X 0	032				"Flush to top perf w/48 bbls water" "Start frac when 26 bbls flush away"	
	1077 FU	10/4/2004 10.74	5 51		35.0		6.21		<u> </u>	295		<del> </del>		"Start frac when 26 bbls flush away"  "131 bbl clean fluid and 30 ton CO2"	·
	1411 FU	10/4/2004	T	15.17	35.0		6.21 6.48 7.14		X 9	388		<del> </del>	<b> </b>	"28 ton CO2"	
	1544 FU	10/4/2004 10.30	<u> </u>	22.06	35.0	1	7.14		X 7	711		<u> </u>	[	"166 bbl "clean fluid", 24 ton CO2"	
		10/4/2004 8.73 1			35.0	] ,	5.81 6.71			<b>0</b> ,216				"182 bbl clean fluid and 28 ton CO2"	
	1646 FU	10/4/2004 8.73 2 10/4/2004 11.88	2.06	24.13	35.0 35.0		6.71 6.71			3,017 2,987		ļ		"225 bbl "clean fluid" and 39 tons CO2" "268 bbl "clean fluid" and 39 tons CO2" .	
		1/19/2004 11.88 1/19/2005 15.86		₩-1.1 <i>J</i>	19.2	4	7.24			511	)		9 501 "F	ac 139 bbls slickwater"	No
7.35,73	1039 FU	11/9/2004	·						X 1	3.608			F.221-13	"Frac w/70Q CO2 foam."	
	1070 FU	11/9/2004 11/9/2004	[			1			X 1	3,608		[	[	"Frac w/70Q CO2 foam"	
	1134 FU	11/9/2004	[			[			X 9	3,608 ,525 3,608				"Frac w/0Q CO2 foam"	
l	1401 FU	11/9/2004	L	<u>L</u>	l <u></u> .	1	l l	L	X 1	3,608		l	L	"Frac w70Q CO2 foam"	. Jl

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	1490 FU	11/9/2004			34.4	7			X 1	0,886	•			"Frac w/70Q CO2 foamscreened out w/7 bbls flush remainingpressure up to 5000# could not pump int	o
11	1555 FU 1579 FU	11/2/2004 16.13 11/2/2004 13.49 11/2/2004 14.34 11/2/2004 10.34					9.17 8.05 16.82		X 1	705 0,47 7,27 10,026				perfs"  "Frac 185 bbl clean fluid, 29 tons CO2. Screened out 46 bbl into flush"  "Frac 185 bbl clean fluid, 33 ton CO2"  "Frac 267 bbl clean fluid, 49 tons CO2"  "Frac 32 bbl clear fluid, 49 ton CO2"	
24-2 468.	8 WR 10	/27/2004	7.07 1	4.48	35.0	İ	6.06	İ		018	0	İ	174	"Frac86 bbl clean fluid, 26 tons CO2, flush w/50 quality."	No
	497.1 W	R 10/27/2004 R 10/27/2004	4.83 1		35.0 35.0		4.65 6.07 6.55 7.24		X 9	,602 ,696				"frac118 bbl clean fluid, 29 tons CO2" "Frac29 tons CO2, 128 bbl clean fluid"	
			11.48 8.48 1		35.0 35.0		6.55		X 6	275		<del> </del>		"Frac108 bbl clean fluid, 18 tons CO2"	
	1116 FU	10/27/2004	14.80	19.31	35.0		7.24		X 1	<b>0</b> ,85		İ		"Frac170 bbls clean fluid, 31 tons CO2"	-
			2.07 1° 10.34		35.0 35.0		4.14 3.65		X 1	1,528 6,140		ļ		"Frac246 bbl clean fluid, 34 tons CO2"	.
			10.34		35.0		6.93		_	485			4 625 "91	Frac227 bbl clean fluid, 49 tons CO2" bbl clean fluid, 22 ton CO2"	Yes
23-10B 0.	819.6 W	R 10/21/2004	8.96 1	7.93	35.0		8.00 19	9.91	X 6	473		<del> </del>	4,023 72	"150 bbl clean fluid, 20 tons CO2	-   105
	872.6 W	R 10/20/2004	8.30 1	9.65	35.0		7.35 1	8.55	X 6	559		ļ		"96.5 bbls clean fluid, 22 tons CO2. Flush w/50Q"	
	893.7 W	R 10/20/2004 R 10/20/2004	12.45 11.71		35.0 35.0		9.86 2 8.83 1			628 181				"117 bbls clean fluid, 19 tons CO2" "141 bbls clean fluid, 28 tons CO2"	
			14.78		35.0 35.0		10.29			174		<del> </del>		"149 bbls clean fluid, 28 tons CO2"	
1	1134 FU	10/20/2004	8.94 1	8.62	35.0		7.58 1		X 1	0,310		l		"224 bbls clean fluid, 34 tons CO2"	-
			10.34		35.0		3.00 3.19			8,086				"235 bbls clean fluid, 54 tons CO2"	.
	1458 FU 1631 FI	10/16/2004 10/16/2004	11.20	17.24 20.68	35.0 35.0		3.19 4.92		$\begin{bmatrix} X & 1 \\ Y & 1 \end{bmatrix}$	5,481 5,804				"248 bbls clean fluid, 43 tons CO2" "267 bbls clean fluid, 43 tons CO2"	
				21.37			1.21		X i	5,985		<del> </del>		"224 bbl clean fluid, 43 ton CO2"	
		12/6/2004 7.78					9.09		<del>                                     </del>	,0	72 2		2,219 "SI	ckwater, CO2 assist-96 bbl"	Yes
		R 12/6/2004 30.5					8.30			,165		[		"Slickwater, CO2 assist-83 bbl"	
		R 12/6/2004 11.0					9.14			0,433 .804				"Slickwater, CO2 assist-89 bbl"	
		R 12/6/2004 27.0 R 12/6/2004 16.1					7:50 14.63	ļ::		,804 ,897		}		"Slickwater, CO2 assist-87 bbl" "Slickwater, CO2 assist-85 bbls"	-
		R 12/6/2004 12.7					8 46			4,51				"Slickwater, CO2 assist-140 bbl"	
1		12/5/2004 18.37					9.47			,123				"Slickwater, CO2 assist-89 bbl"	
1		R 12/5/2004 17.9	6			ļ	12.04			804		ļ		"slickwater, CO2 assist-180 bbl"	
		12/5/2004 17.37 12/5/2004 4.32					8.96 8.25	·	Λ. 1 Χ 1	5,966 5,876		<del> </del>		"Slickwater, CO2 assit-177 bbl" "Slickwater, CO2 assit-187 bbl"	
	1406 FU	12/5/2004 10.96				l	6.78 3.01	<u> </u>				İ	L	"Slickwater, CO2 assist-260 bbl"	-
	1453 FU	11/23/2004	15.71					[	X 6	6,329 ,877		ļ	[	"Slickwater, CO2 assit-102 bbl"	
			26.32		12.2		12.69			0,04			721	"Slickwater, CO2 assit-126 bbl"	\$7
112-11B 4	28.3 WR	12/31/2004	10.73	10.14	13.2	1	6.54		X 1	3,387	U		731	No description of stimulation fluids in well completion report. From WOGCC (2014), "Wind River Sands were selectively perforated between 1,406' and 2,674' and fracture treated with an estimated total of 610 barrels of CO2 assisted gelled waterThe shallowest perforations are 1,406'-1,473' and this interval was fracture treated with 110 barrels of CO2 assisted gelled water"	Yes
	467.6 W	R 12/31/2004	13.47	9.68	4.23	]	5.98 2	2.85	X 7	251		[		see above	-

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	523 WR 811.7 W	R 12/31/2004 12/31/2004 R 12/31/2004	10.71 17.20 8.61 1	12.82 1.24	14.0 17.2 16.7	0 7	5.80 2 5.81 2 5.37 10	1.26 5.74	X 7 X 8	910 909 ,147				see above see above see above	
		12/31/2004	9.54 12		19.5	4	6.40 10	5.29	X 1	1,320				From WOGCC (2014) "fracture treated with an estimated 100 barrels of CO2 assisted gelled water"	
	577.6 W 638.3 W 732.7 W	11/18/2004 R 11/18/2004 R 11/18/2004 R 11/18/2004	11.09 22.13 10.69 11.55	18.16 12.60	21.0 21.4	24.12 17.97	8.69 2: 9.45 20 8.83 2: 10.34	5.47 3.98	X 6 X 6 X 7	666 817 543 068	2		2,606 Fro	m stimulation rpt: 3529 gal wa <u>ter, 3529 gal 70Q CO2 WF12, 43 lb J218, 25 lb/1000 gal polymer loading</u> From stimulation rpt: 4206 gal water, 2989 gal 70Q CO2 WF12, 44 lb J218, 25 lb/1000 gal polymer loading From stimulation rpt: 4329 gal water, 2969 gal 70Q CO2 WF12, 46 lb J218, 25 lb/1000 gal polymer loading From stimulation rpt: 4596 gal water, 3027 gal 70Q CO2 WF12, 46 lb J218, 25 lb/1000 gal polymer loading	
	830.6 W 1103 FU 1163 FU	R 11/18/2004 R 11/13/2004 11/13/2004 11/13/2004	17.65 14.75				5.27 5.27		X 7 X 8 X 6 X 9	,031 ,092 ,841 ,274				"slickwater/CO2 assist" "Frac: slickwater/CO2 assist-158 bbls" "Frac: slickwater/CO2 assit-162 bbls" "Frac: slickwater/CO2 assist-114 bbls"	
	1505 FU 1579 FU 1598 FU	11/13/2004 11/13/2004 11/13/2004 11/13/2004	17.65 14.75 8.62 8.76 12.41 11.38				6.21 9.48 12.82 11.03		X 1 X 1 X 8 X 1	6,036 0,866 6,919				"Frac: slickwater/CO2 assit-210 bbls" "Frac: slickwater/CO2 assist-171 bbls" "Frac: slickwater/CO2 assist-169 bbls" "Frac: slickwater/CO2 assist-247 bbls"	
		11/13/2004	14.13				9.79		X 9	=			1 476 1101	"Frac: slickwater/CO2 assist-263 bbls"	NT.
		2/16/2005 R 12/16/2005					8.09 28 8.76 24			131 916			1,4/6 91	bbls linear gel" "102 bbls linear gel"	No
	659.3 W	R 12/16/2005					10.79		X 9	949				"122 bbls linear gel"	
		R 12/16/2005					8.54 19			481		[		"122 bbls linear gel" "111 bbls linear gel"	
	931.5 W	R 12/16/2005 12/16/2005					10.84		X 6	,570 0,177		ļ		"114 bbls linear gel"	
	1033 FU 1067 FU	12/16/2005					10.79	20.58		,177 ,514				"224 bbls linear gel" "135 bbls linear gel"	
	1094 FU	12/16/2005	14.48				3.03 12	.89		4,887				"233 bbls linear gel"	
	1136 FU	12/16/2005							X 9	,757				"137 bbls linear gel"	
	783.6 W	12/30/2004 R 12/30/2004 R 12/30/2004	8.03 8. 13.73 16.90	10:78	.39 17.4 18.4	2	5.98 6.84 8.89		X 9	1525	2,570		14,008 "F	rac: slickwater36.6 tons CO2, 125 bbls KCl (est)" "Frac: slickwater:28.5 tons CO2118 bbls KCl (est)" "Frac: slickwater20.4 tons CO2, 102 bbls KCl (est)"	Yes
		12/30/2004	16.90		18.4	9	8.89		X = 0	,804 0,886		<b> </b>	<b> </b>	"Frac: slickwater32.6 ton CO2, 143 bbls KCl (est)"	1
	1396 FU	12/30/2004 12/30/2004	10.09	9.45	4.78	I	9.45	<u> </u>	X 1	3,608		[	[	"Frac: slickwater 40.7 tons CO2, 185 bbls KCl (est)"	
			9.48 1.	3.82	21.5		9.85		X 1	3,608				"Frac: slickwater40.7 tons CO2, 190 bbls KCl (est)"	
		/14/2005 8.52	<u>,</u>		19.5 22.4			24.20			)	ļ	185	"91 bbls slickwater" .	No
		R 1/14/2005 6.27 1/14/2005 7.17	· <del> </del>		22.5	0	7.24 18	20.13 3.78				<del> </del>		"94 bbls slickwater" "148 bbls slickwater"	·
	847 WR	1/13/2005 2.55			14.6	2	6.96 18	3.10	X 8 X 6	804		· · · · · ·		"377 bbls slickwater" ·	
	1044 FU	1/13/2005 14.75 1/13/2005 10.27	Ţ		18.6	5	9.24 1	8.55	X 9	525		ļ	[	"124 bbls slickwater" "155 bbls slickwater"	
				15.24	19.4	4	6.07 1:	5.38		0,886			400-77		1
44-11B 4	55.1 WR	1/11/2005 R 1/11/2005	· <b></b>						X 6	,690 ⁴	<del>-</del>	ļ	4,985 "18	2 bbls WF125/75Q CO2" "185.6 bbls WF125 75/65Q CO2"	No
	540.1 W	R 1/11/2005 R 1/11/2005	+				<del> </del>		X 7	,199 ,430 ,212		<del> </del>	<u> </u>	"184 bbls WF125 75/65Q CO2"	
	879.3 W	R 1/11/2005	·						X 7	212		t	l	"191 bbls WF125/75Q CO2"	1

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation Stimulation Date .	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	974.1 W 1041 FU 1074 FU	R 1/11/2005 1/11/2005 1/11/2005							X 7 X 1 X 8	,044 1,412 ,831				"288 bbls WF125/70Q CO2" "325 bbls WF125/70Q CO2" "298.5 bbls WF125/70Q CO2"	
	684 WR 728.5 W 768.1 W 1077 FU 1401 FU 1419 FU 1447 FU 1473 FU 1558 FU	12/17/2004 R 12/17/2004 R 12/17/2004 12/16/2004 12/16/2004 12/16/2004 12/16/2004 12/16/2004 12/16/2004	16.82 16.83 12.69 12.13 10.68 8.94 11.00 11.86 11.17 9.51				8.61 7.41 8.27 4.85 4.43 7.63 7.03 7.33 8.62		X 7 X 6 X 7 X 6 X 1 X 8 X 8	,532 [ ,121 ,827 ,072 ,808 0,845 0,587 ,246 ,119 0,791 1,939			1,886 "S1	ckwater, 92 bb 1CO2 assist"  "Slickwater, screen-out, 65 bblCO2 assist"  "Slickwater, 93 bblCO2 assist"  "Slickwater, 115 bblCO2 assist"  "Slickwater, screen-out, 72 bblCO2 assist"  "Slickwater, 161 bblCO2 assist"  "Slickwater, 163 bblsCO2 assist"  "Slickwater, 144 bblCO2 assist"  "Slickwater, 145 bblCO2 assist"  "Slickwater, 155 bblCO2 assist"  "Slickwater, 175 bblCO2 assist"  "Slickwater, 175 bbl CO2 assist"	No
13-10 670	0 WR 12 761.1 W 956.5 W 982.1 W 1003 W 1100 FU 1211 FU 1377 FU 1407 FU 1475 FU 1505 FU 1571 FU	7//2004 10.56 R 12/7/2004 12.0 R 12/7/2004 15.6 R 12/7/2004 15.6 R 12/7/2004 7.33 12/7/2004 7.31 12/7/2004 7.71 12/7/2004 7.14 12/7/2004 10.56 12/7/2004 10.19 12/7/2004 11.03 12/7/2004 11.80 12/7/2004 10.97	\$ 1	11	28.0 29.0 31.0 32.0 30.0 28.0 29.0		9.80		X 6 X 6 X 6 X 8 X 6 X 8 X 1 X 6 X 8 X 8	,804 ,804 ,804 ,804 ,165 ,804 ,165 0,886 ,804 0,886			7,329 "S1	ckwater/CO2 assi st20 tons CO2"  "Slickwater/CO2 assit-106 bbl20 tons CO2"  "Slickwater/CO2 assit-108 bbls20 tons CO2"  "Slickwater/CO2 assit-120 bbls20 tons CO2"  "Slickwater/CO2 assit-120 bbls243 tons CO2"  "slickwater/CO2 assit-114 bbls20 tons"  "Slickwater/CO2 assit-114 bbls20 tons"  "Slickwater/CO2 assit-131 bbls24 tons"  "Slickwater/CO2 assit-131 bbls24 tons"  "Slickwater/CO2 assit-164 bbls20 tons"  "Slickwater/CO2 assit-168 bbls32 tons"  "Slickwater/CO2 assit-148 bbls34 tons"  "Slickwater/CO2 assit-151 bbls24 tons"  "Slickwater/CO2 assit-177 bbls32.2 tons CO2"	No
21-10B 1	1079 FU	/24/2005 12.27 1/24/2005 13.97 1/12/2005 14.48					7.58 8.62 8.96		X 6 X 9 X 9	,957 8 ,458 ,056	3		14,747 "1	00 bbls clean flu id" "147 bbls clean fluid" "168 bbl clean fluid"	No
43-11B 4	33.1 WR 498.7 W 517.2 W 563.6 W 862 WR 933 WR 961 WR 1098 FU	1/27/2005 R 1/7/2005 R 1/7/2005 R 1/27/2005 I1/27/2005 1/27/2005 1/27/2005 1/27/2005							X 7 X 6 X 5 X 6 X 7 X 8 X 8	,532 (c ,923 ,418 ,319 ,702 ,581 ,383 1,638			190	"199 bbls WF125 75Q CO2" "195.4 bbls WF125 75Q CO2" "180 bbls WF125 75Q CO2" "191 bbls WF125 75Q CO2" "231 bbls WF125 75Q CO2" "278 bbls WF125 75Q CO2" "306 bbls WF125 75Q CO2" "338 bbls WF125 75Q CO2"	No
42-10B 5	76.1 WR 660.2 W 752.2 W	2/3/2005 R 2/3/2005 R 2/3/2005							X 5 X 6 X 9	,118 ( ,998 ,656	)		2,882 "17	Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes   Yes	

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation Stimulation Date .	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa) .	Instantaneous Shut-Ih Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	817.8 W	R 2/3/2005 R 2/3/2005 R 2/3/2005 R 2/2/2005 2/2/2005 2/2/2005 2/2/2005							X 6,751 X 6,854 X 6,855 X 8,165 X 9,329 X 9,935 X 14,07		İ		"206 bbls WF 125 75Q"	1
	909.5 W	R 2/3/2005							X 6,854				"208 bbls WF 125 75Q"	
	1939.4 W	R 2/3/2005 R 2/2/2005		-			<b> </b> -		X 6,804		ļ		"WF 125 75Q" "240 bbls WF 125 75Q"	
	1062 FU	2/2/2005		<del>-</del>					X 8 165				"WF 125 70O"	
	1081 FU	2/2/2005							X 9,329		İ		"329 bbls WF 125 70Q" "339 bbls WF 125 70Q"	
	1377 FU	2/2/2005							X 9,935				"339 bbls WF 125 70Q"	
	1467 FU	2/2/2005							X 14,07	7			"422 bbls WF 125 70Q"	<u> </u>
22-11B 6	80.9 WR	2/7/2005			ļ		<b>∤</b> -		X 6,804 X 8,165	0	ļ	817	"WF 125 70Q CO2" "WF 125 70Q CO2"	No
	1050 FU	R 2/7/2005 2/7/2005					·		X 8 165				WF 125 70Q CO2   "WF 125 70Q CO2"	
	1099 FU	2/7/2005					h		X 8,165 X 7,813 X 6,595		+		"272 bbls WF 125 70Q CO2"	
	1127 FU	2/7/2005 2/7/2005							X 6,595		<u> </u>		"272 bbls WF 125 70Q CO2" "285 bbls WF 125 70Q CO2"	
		2/4/2005							X 11,39				"340 bbls WF 125 70Q"	
32-10C 5	85.2 WR	2/10/2005 R 2/9/2005 R 2/9/2005		ļ			ļ		X 13,94 X 6,459	4 8 -		7,099 "3		Yes
	649.2 W	R 2/9/2005 B 2/d/2005		-	ļ		ļ		X 6,459 X 3,239				"190.5 bbls WF 125 75Q CO2"  '163 bbls WF 125 75Q"	
	790 WR	2/9/2005					<del> </del>		X 8.190		<del> </del>		"237 bbls WF 125 75Q CO2"	·
	867.5 W	2/9/2005 R 2/9/2005 R 2/9/2005		- <del> </del>					X 8,190 X 6,329 X 9,371		†		"237 bbls WF 125 75Q CO2" "204.5 bbls WF 125 75Q CO2"	
	1031 W.	R 2/9/2005							X 9,371		[		"342 bbls WF 125 70Q CO2"	
		R 2/9/2005							X 6,768				"270.5 bbls WF 125 70Q CO2"	<del></del>
22-11C 4	149.3 WR	2/16/2005 2/16/2005					ļ		X 5,979 X 6,566	6		8,725 "1	79 bbls WF 125, 75Q CO2"  "194 bbls WF 125, 75Q CO2"	No
	759 6 W	R 2/16/2005					·		x 8,375				"229 bbls WF 125, 75Q CO2"	
	857.7 W	R 2/16/2005 R 2/16/2005		-			h		X 6,838				"204 bbls WF 125, 75Q CO2"	
	880 WR	2/16/2005 R 2/16/2005							X 6,878 X 6,688		İ		"207.5 bbls WF 125, 75Q CO2"	
	926.3 W	R 2/16/2005		ļ					X 6,688				"202.5 bbls WF 125, 75Q CO2"	
		2/16/2005 · ·	+ •	<u> </u>					X · 6,709			• • •	"230 bbls WF 125, 70Q CO2"	<u> </u>
44-4 115	3 FU 3/8	[2005] [3/8/2005			ļ		6.09 13 6.69 14		X 16,45 X 20,42	1 1,265		26,707 "	l60 bbls slickwater" "178 bbls slickwater"	Yes
	1411 FU	3/8/2005 3/8/2005		-			8.80 16		Λ 2 <b>Ψ,</b> 42 Χ 15,94				"175 bbls slickwater"	
		3/8/2005						37.53.7			†		"107 bbls slickwater"	
12-12 59	8.6 WR 3	/3/2005 10.73					7.55 22	2.62	X 13,90	0.0		187	"96 bbls slickwater" .	No
	1111 FU	3/3/2005 7.26 3/3/2005 11.42					6.12 11	.61	X 11,42	β	[		"96 bbls slickwater" "109 bbls slickwater" "183 bbls slickwater"	
				<u> </u>			6.23 15	.38	X 10,32 X 13,90 X 11,42 X 20,73	2				Щ.
33-2C 56	68.5 WR	2/24/2005 15.76	4	<b></b> -	ļ		9.17 8.98		X 6,844 X 6,133 X 7,304 X 6,542 X 10,82	0	ļ	0		No
	1693.9 W	R 2/24/2005 15. 2/24/2005 12.51	44				8.98		X 6,133 X 7,204	ļ			"4790 bbls 75Q slickwater" "2111 bls 75Q slickwater"	
	789.1 W	R 2/24/2005 12.31	: 11				8.69		X 61542	<del> </del>			3846 bbls 750 slickwater	
	812 WR	R 2/24/2005 13. 2/24/2005 14.62	2	†·			8.69 7.72 7.58		X 10,82	‡ 5	†		"3846 bbls 75Q slickwater" "5054 bbls 75Q slickwater"	
	835.2 W	R 2/24/2005 17.	07	1			7.58		X 6,758	· · · · · · · · · · · · · · · · · · ·			"4002 bbls 75Q slickwater"	1

		T.	in the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the		<b>5</b> 0							<b>-</b>			<b>.</b>	
=	uo.	Stimulated		Pressure	e During	during tom	iring a)	Instantaneous Shut-In Pressure (Mpa)	=	ıring		sxs sand)	(siqu	Water (bbls)	.  Description of Stimulation from Well Completion Reports and Sundry Notices	lle
Well Abbreviation	Stimulatio I (m bgs)	or	Stimulation Date	ı Pre	Average Pressure Stimulation (MPa	w dr.	Q S	us St [pa]	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Stimulation	(kg or	Oil Production (bbls)	/ater	Of St.	WOGCC Well File Review ³¹
bbre	Stim II (m	etion tion	ation	Dow	e Pr	e Fle	ressu	ane re (V	5 (E)	alic I	liii.	ınt (4	duct		Vell C	S
ell A	Top of Stim Interval (m	Completion Formation	imi	Break Down   (MPa)	verag	Average Flow o	Max Pressu Stimulation	Instantaneous S Pressure (Mpa)	Fracture ( (MPa/km)	ydrai	Acid St	Proppant	il Pro	Produced	escri otices	OGC eview
= =				B ()	A 22	A 22	Z 22		E 6				0	Ъ	and the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of th	<b>\$</b> \$\div 2
			/2005 14.75					7.93			2,39				"7158 bbls 75Q slickwater"	
13-2B 4	29.5 WR 480.4 W	B/19/2	005			<b>∤</b> ∤		6.00 2			720	0		3,944 "3	9 bbls slickwater"	.No
	536.8 W	K 3/1 D 2/1	9/2005					6.55 2 7.07 2		X 9	,807 720				"70 bbls slickwater" "67 bbls slickwater"	
	586.4 W	R 3/1	9/2005					7.07.2 7.89.2	3.53	X 9	730				"67 bbls slickwater"	
	586.4 W 670 WR	3/19/	2005					7.89 2 5.58 1	\$.55	X 9	625				"70 bbls slickwater"	
	800.1 W	R 3/1	9/2005					8.27 2	0.36	X 1	,720 ,730 ,625 3,700	5			"128 bbls slickwater"	11
	1063 FU 1107 FU	3/18	/2005					9.10 1	<b>\$</b> .78	X 7 X 6 X 6	253			[	"68 bbls slickwater" "66 bbls slickwater"	
	1107 FU	3/18	/2005						ļ	X 6	536				"66 bbls slickwater"	
	1128 FU							7.17 1							"92 bbls slickwater"	<u> </u>
43-4 524	1.B WR 3/	16/20	05 8.55 6/2005 14.60	·				7.83 1	0.18	X 1 X 7		0 44 19,6	81 "35	73 bbls	70Q x-linked gel…re servoir pressure 963 psi" "2555 bbls 70Q x-linked gel…reservoir pressure 1167 psi"	Yes
	043.3 W	R 3/1 R 3/1	6/2005 14.60 6/2005 12.78	; ?				7.21 1 5.99 1	ψ.18 Δ.18	$\frac{X}{Y} = \frac{1}{2}$	306				"2858 bbls 70Q x-linked gelreservoir pressure 1167 psi"  "2858 bbls 70Q x-linked gelreservoir pressure 1466 psi"	
			6/2005 12.70						10.18	$\frac{\alpha}{x}$ $\frac{\beta}{9}$	525				"3074 bbls 700 x-linked gel reservoir pressure 1736 nsi"	
	1053 FU	3/16	/2005 16.64			11				X 7	525 719				"3074 bbls 70Q x-linked gel…reservoir pressure 1736 psi" "3424 bbls 70Q x-linked gel…reservoir pressure 1904 psi"	11
			/2005 15.49			11		5.56 1		X 2	0,51	3			"8293 bbls 70Q x-linked gelreservoir pressure 2107"	11
	1402 FU	3/16	/2005 13.70			1			10.18	X 6	823				"3077 bbls 70Q x-linked gelreservoir pressure 2531 psi"	
33-2B 4	30.4 WR :	3/23/2	005								,121			,617 "5	6 bbls slickwater" "62 bbls slickwater"	No
			3/2005 10.63	5				5.80 2			258				"62 bbls slickwater"	
	565.7 W	R 3/2	3/2005 12.43 3/2005 13.80	<u></u>				7.34 2		X 2	0,31	B			"144 bbl slickwater" "60 bbls slickwater"	
	6/6.7 W	K 3/2	3/2005 13.80 3/2005 14.13	<u>,</u>				6.30 1	9.45 20.13	X 6	985				"60 bbls slickwater"   162 bbls slickwater"	
	863.5 W	R 3/2	2/2005 14.11 2/2005 10.97	, ,				9.80 2			439	·			"1442 bbls slickwater"	
14-3B 8	87.3 WR							8.97 1	+		748	5		1,901 "5		Yes
17-35-0			/2005 14.94						21.04					1,501	"111 bbls slickwater"	103
	1146 FU									X 1					"1215 bbls slickwater"	11
41-11B	498.3 WR	4/6/2	005 3.00					4.54 1		X 3	835	12 640			"53 bbls slickwaterFlush with 23 bbl 6% KCL w/50% CO2""	No
			/2005 4.37					6.10 1	9.23	X 7	380 213 0,85				"60 bbls slickwaterFlush with 33.5 bbl 6% KCl"	
	713.5 W	R 4/5	/2005 0.00							X 7	213				"55 bbls slickwaterFlush with 34 bbl 6% KCL and 60% CO2"	]
			005 12.47					7.02 1	<b>8</b> .55	X 1	0,85	1			"80 bbls slickwaterFlush with 40 bbls 6% KCL"	
	1077 EI	K 4/5	/2005 11.09 2005 15.36			<del> </del>		9.22 2			536				"61 bbls slickwaterFlush with 45 bbl 6% KCL" "105 bbls slickwaterFlush with 54 bbl 6% KCl"	
	1158 FU							7.35 1 4.01 1	1.19	A 8 X 1	275	5			"170 bbls slickwaterFlush with 58 bbls 6% KCl"	
42_4B_5	26.4 WR							8.16 2			3,60			Q Q57 "I	Flush with 17 bbl 6% KCL and 7 bbl CO2"	No
72-40 )	730 WR	3/29	2005 16.11											0,007 1	"Flush with 36 bbl 6% KCL"	
	802.5 W	R 3/2	2005 16.11 9/2005 9.14			11		10.18	3.53 22.85	X 9	525			·	"Flushed with 40 bbl 6% KCL"	1
			9/2005 10.07	7						X 4					"Screen out 22.4 bbl into flush, 19.9 bbl shy of full flushPumped 81 bbl of clean fluid and 16 tons of CO2 + sand"	
	864.7 W	R 3/2	9/2005 15.48	3		19.8			1.72					T	"126 bbl clean fluid and 27 ton CO2"	
	1136 FU	3/29	/2005 12.15 /2005 16.33			1			19.45 19.45						"180 bbl clean fluid and 39 ton CO2"	
						22.3									"165 bbl clean fluid and 30 ton CO2"	
21-11B	440.1 WR	4/12	2005 7.18			J		5.16 1	<b>ф</b> .18	X 6	,811	18 1,560	) "5 <del>4</del> b	ols slick	water"	Yes

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	626.4 W	R 4/12/2005 7.17					6.49 10			0,906				"77 bbls slickwater"	
		R 4/12/2005 7.57					6.83 10			803		[		"55 bbls slickwater"	
	741.6 W	R 4/12/2005 10.2 R 4/12/2005 17.5	Ţ				7.27 10 8.43 10			,511 ,826				"58 bbls slickwater" "63 bbls slickwater"	
		4/12/2005 9.19	f				6.32 10		л о Х 9	740				"89 bbls slickwater"	!
		4/12/2005 14.16					6.59 10		X 6	891				"74 bbls slickwater"	
	1102 FU	4/12/2005 11.09					6.14 13			018				"87 bbls slickwater"	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
13-3W 45		16/2005 17.07					7.58 26			483	3		1,340 "60	bbls slickwater"	Yes
		R 4/16/2005 17.0 R 4/16/2005 17.0					7.58 20		X 6	582 104		ļ		"74 bbls slickwater" "66 bbls slickwater"	
		R 4/16/2005 17.0					7.58 20 7.58 19		X 6 X 1	1.132				"93 bbls slickwater"	!
	860.1 W	R 4/16/2005 17.0	Ŧ				7.58 19			417				"68 bbls slickwater"	
		R 4/16/2005 17.0	Z				7.58 17	7.87		071		[		"100 bbls slickwater"	
		4/16/2005 17.07					7.58 13		X 6	_				"134 bbls slickwater"	<u> </u>
41-10B 5	46.2 WR	4/30/2005 11.58 R 4/30/2005 12.0	ļ				7.14 23 8.09 21	3.30	X 5	,285 1,864	9		293	"'48 bbls slickwater" "'82 bbls slickwater"	Yes
		R 4/30/2005 12.0 R 4/30/2005 23.3					8.09 21 9.34 20			393				"53 bbls slickwater"	!
		4/30/2005	F				0.00 1			3,494				Information on stimulation missing from completion report. From WOGCC (2014) "CO2 assist"	
34-28 605		0/2005 13.61		13.56	18.6	1	8.62 8.09			,165	)		0	"97 bbls 6% kcl 24.4 tons co2"	No
		R 5/20/2005 7.89			22.8					165				"109-bbls 6% kcl 24.4 tons co2"	
	927.2 W	R 5/16/2005 15.5 R 5/10/2005 19.4	<u>*</u>		17.9		13.93 11.76		X 8	165 811				"115 bbls 6% kcl 24.4 tons co2" "172.2 bbls total co2-27 tons"	
		4/29/2005 19.03	f	19.03	23.1		5.85		л о Х 0			<del> </del>		"Acidize w/750 gal KCl, 7.5% acid"	
	1367 FU	4/14/2005 14.26			-====		7.89 13	.83		1,197	,			"Total fluid pumped was 145.6 bbl, total slurry was 172 bbl, total CO2 was 33 tonsLeft +/-10,000 pounds	,
			ļ							l			L	lbs sand in casing"	
	1392 FU	4/8/2005 15.17 3/26/2005 17.93					4.14 10.03	16 51	X 0	 				"Acidize w/23 bbls kcl, 7.5% acidFlush w/18 bbls kcl" "WF 125 SlickwaterFlush with 78 bbl 6% KCL and 50% CO2"	
32-3 575		25/2005 17.06		18.62	20.6		8.40	10.51				m "25_	bb1d 6% 1	cl 20.4 for sco2" s co2"	No
32-3313.		R 5/25/2005 17.3		20.68	22.0	6	8.74			4 L	, 1 30,2	10 05-	5014 0701	"125-bbls 6% kcl 32.6 tons co2"	
	910.7 W	R 5/25/2005 12.2	\$	20.68 20.68	23.4	4	8.74 9.47 8.48 7.07 6.62		X 7	1,037 ,021		<u> </u>	[	"104-bbls 6% kcl 20.4 tons co2" "127-bbls 6% kcl 28.5 tons co2"	
		R 5/25/2005 16.5	1	22.75	26.5	4	8.48			370		ļ	ļ	"127-bbls 6% kcl 28.5 tons co2"	_
	1427 FU	5/25/2005 20.04 5/25/2005 22.51	<b></b>	20.68 22.75	27.5 25.5	8	7.07 6.62			,931 0,412		ļ		"133-bbls 6% kcl 20.4 tons co2" "245 bbls 6% kcl 61.1 tons co2"	
43_9 1544		7/2005 9.63 24.13		22.13	23.3		5.41		л 2 У 0	066 414	, 2	<u> </u>	20 928 "1	245 bbls 6% kcl 28.5   tons co2"	No
15-7 1540	1618 FU	5/27/2005 14.80	<b></b>	26.20		<u> </u>	V.71		$\frac{\Lambda}{X}$	,066 ,157 3,641 7,557		<b> </b>	20,720	"143 bbls 6% kcl 20.4 tons co2"	
	1649 FU	5/27/2005 14.80 5/27/2005 14.39		26.20 24.13	27.7	2	6.32		X 1	3,64		<u> </u>	[	"200-bls 6% kcl 40.7 tns co2"	
	1697 FU	5/27/2005 20.26		24.13	29.9		8.55		X 1	7,557	, <b></b>			"180-bbls 6% kcl 32.6 tons co2"	
		9/2005 16.20	ļ				7.65 9.48		X 1	0,210 ,354	0	ļ	19,153 "1	loo bbls fluid"	No
	842.3 W  912 W/D	R 7/9/2005 13.54 7/9/2005 13.38	<b></b> -				9.48 8.93		А / Х 7	334 208		<del> </del>		"108 bbls fluid" "185 bbls fluid"	
	970.8 W	R 7/9/2005 15.69	<b></b> -			<u> </u>	10.34		X 1	,208 1,387 3,950	,	<b> </b>	<b></b>	"132 bbls fluid"	
	1166 FU	R 7/9/2005 15.69 7/9/2005 27.03	<b></b>			1	6.41		X 1	3,950		†	l	"206 bbls fluid"	

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated Formation Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during Stimulation (bpm)	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbis)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
	1490 FU 1550 FU	6/17/2005 20.97 6/17/2005 27.72 6/17/2005 21.34 6/17/2005 22.05			28.4	8	8.89 8.17 9.93 15.72	16.51	X 1 X 1	6,595 6,551 6,664 378				"183 bbls 70Q x-linked fluid" "225 bbls of 70Q x-linked fluid" "226 bbls of 70Q x-linked fluid" "193 bbls of 70Q x-linked fluid"	
44-3C 56	9.1 WR 662.3 W 706.2 W 819.9 W 884.2 W	6/3/2005 12.62 R 6/3/2005 12.50 R 6/3/2005 16.97 R 6/3/2005 17.23 R 6/3/2005 8.81	T				7.77 7.47 8.16 2 9.19 2 9.15 2	1.49 1.26 0.58	X 8 X 1	_		87 "88	bbls fluid	"C ement squeeze on 7/7/2005 apparently due to well making water. "116 bbls fluid" "101 bbls fluid" "95 bbls fluid" "121 bbls fluid"	No
32-2 794.	3 WR 3/ 919.6 W 1088 FU 1498 FU	6/3/2005 16.55 28/2006 11.02 R 3/28/2006 11.8 3/24/2006 13.87 3/22/2006 10.54 3/15/2006 17.93	i		40.5 18.1 20.1 19.5	2	7.52 10 7.01 19 9.43 20 12.19 10.03 7.25 1	0.00 0.36 21.26 16.74	X 1 X 1 X 1	6,019 3,830 2,448 3,100 2,938	) 2		4,450 "18	"213 bbls fluid"  1 bbls 6% KCl, 65Q CO2"  "204 bbls 6% KCl, 65Q CO2"  "Breakdown with 71 bbls 6% KClFrac w/226 bbls 6% KCl, 65Q CO2"  "Breakdown w/90 bbls 6% KCL, 2 gal/1000 surfactantFrac w/221 bbls 6% KCl, 65Q"  "Breakdown w/24 bbls 6% KCl"	No
33-12 557	.8 WR : 897.9 W 1106 FU 1443 FU 1543 FU 1576 FU 1604 FU	/29/2006 9.00 R 3/29/2006 10.1 3/29/2006 8.67 3/2/2006 17.04 3/2/2006 17.46 3/2/2006 15.26 3/2/2006 19.47	2		13.9 17.7 16.8	1 8	8.00 24 8.04 19 7.64 10 9.44 10 9.95 10 9.63 10 20.48	4.88 9.23 5.97 5.74 5.74 5.51 23.07	X 1 X 1 X 1 X 1 X 1 X 1	<b>0</b> ,50			5,520 "16	3 bbl 6% KCL and 28 ton CO2" "190 bbl 6# KCL and 29 ton CO2" "226 bbl 6% KCL, and 30 ton CO2" "Total clean fluid 189 bbl, total slurry 227 bbl, total CO2 42 ton" "Total clean fluid 186 bbl, total slurry 212 bbl, total CO2 27 ton" "Total clean fluid 186 bbl, total slurry 212 bbl, total CO2 27 ton" "Total clean fluid 176 bbl, total slurry 201 bbl, total CO2 24 ton" "Total clean fluid 188.7 bbl, total slurry 213.6 bbl, total CO2 28 ton"	
	1626 FU	3/2/2006 20.01					12.84	18.10	X 1	0,45	i			"Total clean fluid 189.6 bbl, total slurry 214 bbl, total CO2 27 ton. Total injected 352 bbl"	h =
14-21 22-4 610.	2 WR 4/ 671 8 W	3/2007 R 4/3/2007							X 2 X 2	,349 .	2		4,390 "86	bbls WF 118nitrogen assist" "85 bbls WF 118nitrogen assist"	No No
	786.4 W 928.1 W 1014 W 1130 FU 1476 FU 1512 FU	R 4/3/2007 R 4/3/2007 R 4/3/2007 4/3/2007 1/5/2007 18.20 1/4/2007 12.07 1/4/2007 16.82		21.72 19.31	40.0	24.06	11.25	18.55 16.74 18.78	X 2 X 2 X 2 X 1 X 2	,096 ,274 ,235 ,505 2,65 5,129				"101 bbls WF 118nitrogen assist"  "122 bbls WF 118nitrogen assist"  "108 bbbls WF 118nitrogen assist"  "110 bbls WF 118nitrogen assist"  "492 bbls Delta 140 15# xlink gel"  "643 bbls 15# Delta x-link gelFlush w/76 bbl sleik wtr"	
42-15 666	.6 WR : 702.9 W	/20/2007 R 3/20/2007		19.31	30 19	1.77	14.84		v o	421	2		6,668 "14	"440 bbls Delta 140 15# x-link gelFlush w/83 bbl slick wtr"  3 bbls WF118 70Q N2" "146 bbls WF118 70QN2" "150 bbls WF118 70QN2"	No
	861.7 W 906.8 W 1007 W 1059 FU 1081 FU	R 3/20/2007 R 3/20/2007 R 3/20/2007 3/20/2007 3/20/2007 3/20/2007 3/20/2007							X 2 X 2 X 2 X 2 X 2	,183 ,298 ,291 ,230 ,359 ,327 ,277 ,267				"160 bbls WF118 70QN2 "206 bbls WF118 70QN2" "167 bbls WF118 70Q N2" "121 bbls WF118 70QN2" "128 bbls WF 118 70N2" "165 bbls WF118 70QN2"	

Well Abbreviation	Top of Stimulation Interval (m bgs)	Completion or Stimulated	Stimulation Date	Break Down Pressure (MPa)	Average Pressure During Stimulation (MPa)	Average Flow during	Max Pressure During Stimulation (MPa)	Instantaneous Shut-In Pressure (Mpa)	Fracture Gradient (MPa/km)	Hydraulic Fracturing	Acid Stimulation	Proppant (kg or sxs sand)	Oil Production (bbls)	Produced Water (bbls)	Description of Stimulation from Well Completion Reports and Sundry Notices	WOGCC Well File Review ³¹
			2007 30.34					10.16	16.74	X 1	0,43	1			"485 bbls YF 116ST"	
	1554 FU	3/20	) 2007 12.07			1	1	5.31 1	3.35	X 2	0,85	3			"563 bbls YF 116ST"	11
	1608 FU	3/20	V2007 17.79		11.03	30.0	1	5.97 1	<b>3</b> .57	Χ	]				"632 bbls YF 116ST"	
41-26			-												P&A after completion in 2007. No apparent production well casing. No stimulation or production.	

BWR – Basal Wind River Formation

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WR – Wind River Formation

FU – Fort Union Formation

 $L-Lance\ Formation$ 

MT – Meeteetse Formation

F- Frontier Formation

C – Cody Formation

MV - Mesaverde Formation

bbm = barrels per minute bbls - barrels

sxs = sacks

Table SI C3. Summary of compounds used for well stimulation. Information from Material Safety and Data Sheets provided to EPA from Encana³⁵

Compound	Cas No.	Product	Manufacturer	Percent	ets provided to EPA from Encana ³⁵ Specified Product Use
Compound	Ca3110.	Trounct	Manufacturer	Composition	Specifica Froduct & Sc
acetic acid	64-19-7	FE-1A Acidizing Composition H	al liburton	30-60	additive
4		BA-20 Buffering Agent	Halliburton	10-30	buffer
acetic anhydride	108-24-7	FE-1A Acidizing Composition H		60-100%	additive
acetone	67-64-1	MC-B-8630	Multi-Chem Group	15-40	biocide
alcohol (proprietary)	not provided W		Weatherford	1-5	flow enhancer
alcohol (oxylated)	1	usol A Solvent	Halliburton	10-30	solvent
alcohols, C6—10, ethoxylated,	68037-05-8 M		Multi-Chem Group	<8	foaming agent/scale & corrosion inhibitor combination
sulfate, ammonium salts			•		
alkylated quaternary chloride	not provided C		Halliburton	not provided cl	v
alkylamine salts		C6106A Biocide	Nalco/Exxon Energy Chemicals 40		biocide
alkyl hexanol	not provided H		Halliburton	5-10	surfactant
ammonium acetate	631-61-8	BA-20 Buffering Agent	Halliburton	60-100	buffer
ammonium bisulfite	10192-30-0 EC		Nalco/Exxon Energy Chemicals 10	-30	corrosion inhibitor
ammonium chloride	12125-02-9 CI	-12	Halliburton	1-27	crosslinker
anionic surfactants	not provided M	C FA-4013	Multi-Chem Group	<20	foaming agent/scale & corrosion inhibitor combination
aromatic solvent	64741-68-0 M	CDF-7120	Multi-Chem Group	<75	defoamer/emulsion breaker
2-bromo-2-nitro-1,3-propanediol	52-51-7	BE-6 Microbiocide	Halliburton	60-100	biocide
2-butoxyethanol	111-76-2	F104	Schlumberger	10-30	foaming agent
44	"	AQF-2 Foaming Agent	Halliburton	10-30	foaming agent foaming agent
44		MC FA-4500	Multi-Chem Group	1-10	foaming agent
٠,		MC FA-4500 MC FA-4295	Multi-Chem Group	1-10 <10 <11 <12	foaming agent
ι.		MC FA-4001	Multi-Chem Group	<11	foaming agent/scale & corrosion inhibitor combination
ες		MC FA-4013	Multi-Chem Group	<12	foaming agent/scale & corrosion inhibitor combination
ι		F103	Schlumberger :	10-30	'surfactant
ες		Musol Solvent	Halliburton	60-100	solvent
44		Musol A Solvent	Halliburton	60-100	solvent
44		WSP 9999	Weatherford	not provided so	
44		WSP 92011	Weatherford	15-40	not provided
44		Transfoam C	Weatherford	5-10	drilling foam
cationic polymer	not provided L		Schlumberger	10-30	clay stabilizer
copper iodide	7681-65-4	HAI-85M Acid Inhibitor	Halliburton	1-5	corrosion inhibitor
diammonium peroxidisulphate	7727-54-0	J218	Schlumberger	60-100	breaker
2,2-dibromo-3-		-3S Bactericide	Halliburton	60-100	biocide
nitrilopropionamide	10222-01-2 BE	-38 Bactericide	riamourton	00-100	biocide
""		B069	Baker Hughes	60-100	biocide
diethylene glycol	111-46-6	2	Halliburton	2-10	
" diemylene grycor	111-40-0	AQF-2 Foaming Agent Triethylene glycol	Shell Chemicals	0.01-5.0	foaming agent not provided
£ 1 C 1 #2	(047( 24 ( 1 (			30-60	
diesel fuel #2	68476-34-6 LC		Halliburton		liquid gel concentrate
44		LGC-8 J877	Halliburton	30-60	liquid gel concentrate
1' 1 1 0 ' 1			Schlumberger	30-60	guar polymer slurry
dimethyl formamide	68-12-3	HAI-85M Acid Inhibitor	Halliburton	10-30	corrosion inhibitor
d-limonene	5989-27-5	WFT 9527	Weatherford	3-7	flow enhancer
EDTA/copper chelate		AT-3 Activator	Halliburton	10-30	activator
ester salt	not provided F		Schlumberger	30-60	foaming agent
ethanol	64-17-5	LOSURF-300M	Halliburton	30-60	surfactant
44	"	F104	Schlumberger	10-30	foaming agent

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Compound	Cas No.	Product	Manufacturer	Percent	Specified Product Use
				Composition	
ethoxylated alcohol	9016-45-9	WFT 9785	Weatherford	1-3	foaming agent
ethoxylated alcohol linear (1)	not provided F		Schlumberger	5-10	surfactant
ethoxylated alcohol linear (2)	not provided F		Schlumberger	5-10	surfactant
ethoxylated alcohol linear (3)	not provided F		Schlumberger	5-10	surfactant
ethylene glycol	107-21-1	WSP 9030	Weatherford	40-70	hydrate inhibitor
44	44	MC FA-4001	Mult-Chem Group	54-58	foaming agent/scale & corrosion inhibitor combination
"	"	MC FA-4500	Mult-Chem Group	<33	foaming agent
44	46	MC FA-4295	Mult-Chem Group	1-5	foaming agent
"	46	MC WC-7549	Mult-Chem Group	<70	water clarifier
"	44	Artietherm E-50	Quadra	47-53	heat transfer fluid
2-ethyl hexanol	104-76-7	Klean-Break	Weatherford	10-30	not provided
ethyl octynol	5877-429 HA	I-85M Acid Inhibitor	Halliburton	1-5	corrosion inhibitor
glutaraldehyde	111-30-8	MC B-8630	Multi-Chem Group	10-30	biocide
heavy aromatic petroleum naptha	64742-94-5 HY	FLO IV	Halliburton	30-60	surfactant
	44	Pad acid with aromatic naphtha	Halliburton	10-50	pad acid
	44	LOSURF-300M	Halliburton	10-30	surfactant
٠,٠	٠	LOSURF-259	Halliburton	5-10	surfactant
hydrochloric acid	7647-01-0.		alliburton	1,0-30	pad acid
<u>-</u>		Hydrochloric acid	Halliburton	30-60	solvent
hydrotreated light petroleum distillates	64742-47-8 B2	21B	Schlumberger	40-60	polymer slurry
inner salt of alkyl amines		HC-2	Halliburton	10-30	additive
isooctanol	26952-21-6 HY	FLO IV	Halliburton	5-10	surfactant
isopropanol	67-63-0 · ·	LOSURF-259	Halliburton · · · · · ·	30-60 · · ·	• surfactant
٠		F103	Schlumberger	10-30	surfactant
44	44	MC DF-7120	Multi-Chem Group	not provided de	foam er/emulsion breaker
44	٠	MC FA-4295	Multi-Chem Group	1-5	foaming agent
44	44	MC FA-4001	Multi-Chem Group	<8	foaming agent/scale & corrosion inhibitor combination
44		MC FA-4013	Multi-Chem Group	<3	foaming agent/scale & corrosion inhibitor combination
44	44	MC EB-1790	Mult-Chem Group	<1	emulsion breaker
44		Klean-Break	Weatherford	10-30	not provided
	44	HAI-85M Acid Inhibitor	Halliburton	10-30	corrosion inhibitor
		EC1385A	Nalco/Exxon Energy Chemicals 10	<b>j</b> -30	corrosion inhibitor
44	44	Transfoam C	Weatherford	10-30	drilling foam
		WFT 97112W	Weatherford	1-3	mixture
44		EC6106A Biocide	Nalco/Exxon Energy Chemicals 26	-40 · · ·	- Biocide
methanol	67-56-1	Klean-Break	Weatherford	7-13%	not provided
44	44	L55	Schlumberger	not provided cl	ay stabilizer
44	44	WSP 9030	Weatherford	40-70	hydrate inhibitor
		WSP 92011	Weatherford	15-40	not provided
		WFT 97112W	Weatherford	15-40	mixture
٠٠٠		WFT 9785	Weatherford	10-30	foaming agent
		MC FA-4295	Multi-Chem Group	1-25	foaming agent
ζζ		MC FA-2013	Multi-Chem Group	<25	foaming agent/scale & corrosion combination
	44	EC9037a Surfactant	Nalco/Exxon Energy Chemicals 20	-40	surfactant
44		Methanol	Murex N.A.	99.8	methanol
	1			1	

Compound	Cas No.	Product	Manufacturer	Percent	Specified Product Use
methyl isobutyl ketone	108-10-1	WFT 9527	Weatherford	Composition 1-5	flow enhancer
2- monobromo-3- nitrilopropionamide	1113-55-9	BE-3S Bactericide	Halliburton	1-5	biocide
naphthalene	91-20-3	HYFLO IV	Halliburton	5-10	surfactant
	44	LOSURF-300M	Halliburton	0-1	surfactant
2,2`,2`-nitrilotriethanol	102-71-6	J318	Schlumberger	60-100	breaker
organic salt	not provided F	E-3A	Halliburton	60-100%	iron control agent
petroleum raffinates	not provided K	ean-Break	Weatherford	30-60	not provided
polyepichlorohydrin, trimethylamine quaternized	51838-31-4 Cl	a-Sta XP Additive	Halliburton	30-60%	clay stabilizer
polyether	not provided E	C9037A	Nalco/Exxon Energy Chemicals	20-40	surfactant
potassium hydroxide	1310-58-3	CL-31	Halliburton	<5	crosslinker
potassium metaborate	13709-94-9 CI	-31	Halliburton	30-60	crosslinker
44	44	CL-31/Water Blend	Halliburton	5-10	crosslinker
propargyl alcohol	107-19-7	HAI-85M Acid Inhibitor	Halliburton	5-10	corrosion inhibitor
proprietary blend	not provided N	C FA-4001	Multi-Chem Group	<8	foaming agent/scale & corrosion inhibitor combination
proprietary blend	not provided N	C FA-4013	Multi-Chem Group	<12	foaming agent/scale & corrosion inhibitor combination
quaternary ammonium salts	not provided H	AI-85M Acid Inhibitor	Halliburton	10-30	corrosion inhibitor
sodium chloride	7647-14-5	HC-2	Halliburton	5-10	additive
sodium persulfate	7775-27-1	SP Breaker	Halliburton	60-100	breaker
toluene	108-88-3	WFT 9527	Weatherford	3-7	flow enhancer
triethylamine hydrochloride	593-81-7	EC1385A	Nalco/Exxon Energy Chemicals	1-5	corrosion inhibitor
triethylene glycol	112-27-6	Triethylene glycol	Shell Chemicals	95.0-99.9	not provided
1,2,4-trimethylbenzene	95-63-6	LOSURF-300M	Halliburton	0-1	surfactant
xylene -	1330-20-7	WFT 9527 ·	Weatherford	40-70	flow enhancer
22	- C C	MC DF-7120	Multi-Chem Group	not provided de	foam er/emulsion breaker
zirconium complex	not provided C	L-12	Halliburton	30-60	crosslinker

**Table SI C4.** Specified volumes of "gel" used with  $CO_2$  foam during hydraulic fracturing between 2001 and 2002 (1 barrel or bbl = 42 gallons or 159 L)

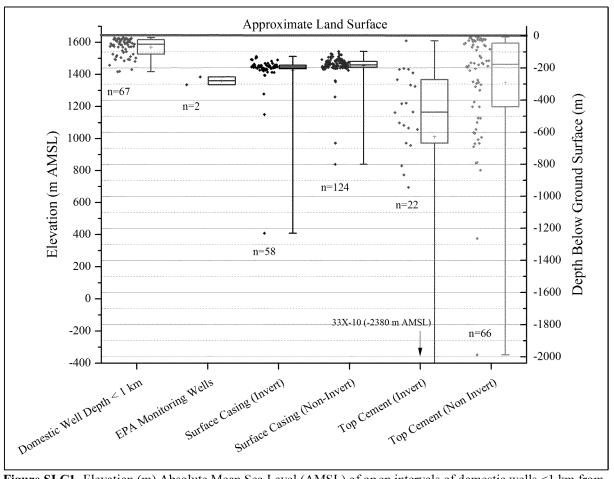
Year	Production Well	Volume
2001 Pa	villion Fee 11-3	51 bbls
44	Pavillion Fee 43-11	157 bbls
2002 Pa	villion Fee 41-10	96 bbls
44	Pavillion Fee 33-11	221 bbls
44	Tribal Pavillion 43-10 646	bbls
44	Pavillion Fee 24-3B	169 bbls
44	Pavillion Fee 11-11B	728 bbls
44	Pavillion Fee 31-11	528 bbls
44	Pavillion Fee 23-3	92 bbls
44	Pavillion Fee 23-3	584 bbls
44	Pavillion Fee 32-11	715 bbls
44	Pavillion Fee 44-11	491 bbls
44	Pavillion Fee 14-3W	206 bbls
44	Pavillion Fee 13-11B	363 bbls
44	Pavillion Fee 14-3W	357 bbls

**Table SI C5.** Specified volumes of "WF-125, WF-130, WF-135, and WF-12" polymer slurries with  $CO_2$  and  $N_2$  foam during hydraulic fracturing from 2001 to 2007 (1 barrel or bbl = 42 gallons or 159 L)

Year	Production Well	Polymer Slurry	Use of 6% KCl solution	Use of 10% Methanol Solution	Foam	Volume of Polymer Slurry (per well)				
2001	Tribal Pavillion 43-1	villion 43-1 WF-125 Yes		No	CO ₂ 658	bbls				
44	Tribal Pavillion 43-1	WF-125	Yes	No	CO ₂ 658	bbls				
44	Pavillion Fee 21-10W	WF-125	Yes	No	CO ₂ 142	0 bbls				
44	Tribal Pavillion 12-5	WF-125	Yes	Yes	CO ₂ 506	bbls				
44	Pavillion Fee 11-11	WF-125	Yes	Yes	CO ₂ 1,4	71 bbls				
44	Pavillion Fee 13-12	WF-125	Yes	Yes	CO ₂ 915	bbls				
44	Pavillion Fee 13-15	WF-125	Yes	Yes	CO ₂ 805	bbls				
44	Tribal Pavillion 34-2	WF-130	Yes	Yes	CO ₂ 1,6	52 bbls				
44	Tribal Pavillion 32-1	WF-130	Yes	Yes	CO ₂ 912	bbs				
46	Tribal Pavillion 14-10	WF-130	Yes	Yes	CO ₂ 673	bbls				
44	Pavillion Fee 34-3R	WF-130	Yes	Yes	CO ₂ 718	bbls				
44	Pavillion Fee 12-11W	WF-125, WF-130	Yes	Yes	CO ₂ 92′	bbls				
44	Pavillion Fee 21-13	WF-135	Yes	Yes	CO ₂ 549	bbls				
46	Pavillion Fee 13-11	WF-135	Yes	Yes	CO ₂ 1,1	55 bbls				
44	Tribal Pavillion 43-2	WF-135	Yes	Yes	CO ₂ 1,1	77 bbls				
2004	Tribal Pavillion 43-10B	WF-12		No	CO ₂ ~2	6 bbls				
2005	Pavillion Fee 43-11B	WF-125	?	No	CO ₂ 362	bbls				
44	Pavillion Fee 44-11B	WF-125	?	No	CO ₂ 1,4	72 bbls				
44	Pavillion Fee 43-11B	WF-125	?	No	CO ₂ 1,5	43 bbls				
44	Tribal Pavillion 42-10B	WF-125	?	No	CO ₂ 2,1	41 bbls				
44	Pavillion Fee 22-11B	WF-125	?	No	CO ₂ 89	bbls				
44	Tribal Pavillion 32-10C	WF-125	?	No	CO ₂ 1,5	64 bbls				
44	Pavillion Fee 22-11C	WF-125	?	No	CO ₂ 1,4	46 bbls				
2007	Pavillion Fee 22-4	WF-118	?	No	$N_2$	612 bbls				
44	Tribal Pavillion 42-15	WF-118, YF116ST	?	No	N ₂	1,386 bbls of WF-118 and 1,680 bbls of YF116ST				

**Table SI C6.** Volumes of slickwater used for hydraulic fracturing (1 barrel or bbl = 42 gallons or 159 L)

Year	Production Well	Foam	Volume (per well)
2004 Tr	bal Pavillion 43-10B CO	2	1,494 bbls
	Tribal Pavillion 33-10B C	D 2	3,432 bbls
	Tribal Pavillion 42-10	$CO_2$	122 bbls
	Pavillion Fee 13-10	$CO_2$	1,731 bbls
	Tribal Pavillion 21-14	$CO_2$	1,353 bbls
	Pavillion Fee 31-10B	$CO_2$	863 bbls
2005 Pa	villion Fee 33-11B	None	949 bbls
	Tribal Pavillion 41-3	None	524 bbls
	Tribal Pavillion 33-2C?		29,873 bbls
	Tribal Pavillion 42-3	None	201 bbls
	Blankebship Fee 4-8	None	121 bbls
	Tribal Pavillion 12-12	None	388 bbls
	Pavillion Fee 44-4	None	620 bbls
	Tribal Pavillion 33-2B No	ne	1,442 bbls
	Tribal Pavillion 13-2B No	ne	1,249 bbls
	Pavillion Fee 14-3B	None	1,380 bbls
	Pavillion Fee 41-11B	None	584 bbls
	Tribal Pavillion 21-11B N	one	557 bbls
	Pavillion Fee 13-3W	None	595 bbls
	Pavillion Fee 34-3B	None	139 bbls
	Pavillion Fee 41-10B	None	183 bbls



**Figure SI C1.** Elevation (m) Absolute Mean Sea Level (AMSL) of open intervals of domestic wells <1 km from production wells, EPA monitoring wells, surface casing with invert mud, surface casing without invert mud, top of primary cement with invert mud, and top of cement without invert mud. Median land surface elevation = 1636 m AMSL.

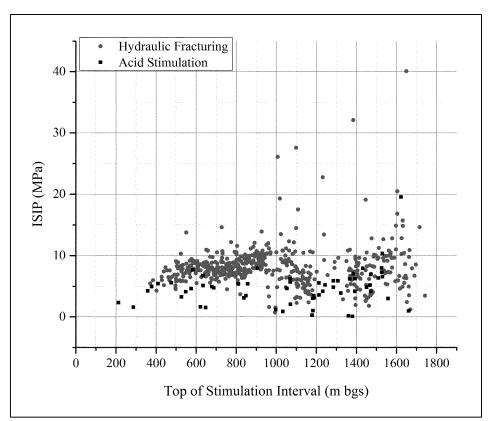


Figure SI C2. Instantaneous Shut-In Pressure (ISIP) values for well stimulation with depth

#### D - Extended Discussion on Impact to USDWs and Usable Water from Well Stimulation

D.1 Examples of Potential Loss of Zonal Isolation (Data Source: Well Completion Reports and Sundry Notices, Seach by API Number in Table SI C1)

## Parted Casing and Cement Squeezes

Casing failure occurred at five production wells following well stimulation resulting in potential loss of zonal isolation.

# Blankenship 4-8

Blankenship 4-8 was completed in March 1977. The base of surface casing is at 134.4 m bgs. On 3/26/1977, hydraulic fracturing was conducted at a depth of 1484 m bgs using "500 gal 15% BDA frac w/102,000 gallons of gel water...300 scfpb nitrogen." A cement bond log/variable density log (CBL/VDL) conducted at 2.76 MPa (400 psig) on 1/05/2005 indicated top of primary cement at 564 m bgs with high amplitude to 625 m bgs. During recompletion activities in January 2005, "a hole" in casing was noted between 312 to 322 m (1025 – 1062 ft) bgs. The time in which the hole in casing formed over a 28-year period between 1977 and 2005 is unknown. Since the base of surface casing is at 134.4 m bgs, there was 429 m of uncemented production casing below surface casing and no cement behind casing at depth of the hole. The potential for migration of stimulation fluid during hydraulic fracturing in 1977 was not assessed. The 1977 well completion report indicates tubing pressure at 4.41 MPa (640 psig) and casing pressure at 9.48 MPa (1375 psig) – well beyond hydrostatic pressure at 312 m bgs indicating likely gas migration at this depth and to presumably through the uncemented borehole to the depth of surface casing. Two cement squeezes were performed on 1/25/2005 and 1/27/2005 to remediate casing.

On 2/8/2005, 121 barrels of slickwater and CO₂ foam in a 6% KCl solution was used for hydraulic fracturing at 814 m bgs using, "slickwater...121-bbls 6% KCl, 28.5 tons of CO2" at a maximum stimulation pressure of 38.2 MPa (5546 psig). On 2/12/2005, hydraulic fracturing was conducted at a depth of 631 m bgs using "Frac slickwater, 104 bbls." at a maximum stimulation pressure of 39.4 MPa (5711 psig). In a well schematic dated 10/5/2011, "parted casing" was noted at 790.9 m (2595 ft) bgs with an assigned date of 12/21/2006. Parted casing, apparently induced during hydraulic fracturing, indicates loss of zonal isolation at 790.9 m bgs during hydraulic fracturing. There is no record of casing repair at this depth. In a sundry notice dated 11/7/2011, tubing, casing, and Bradenhead pressure were recorded as 0 psig. In a sundry notice dated 3/6/2012, a mechanical integrity test (MIT) conducted with a cast iron bridge plug (CIBP) at 616.9 m bgs (above parted casing) at 2.07 MPa (300 psig) indicated no bleed off.

### USA Tribal 258 21-15 (Tribal 21-15)

USA Tribal 258 21-15 (Tribal 21-15) was completed in December 1979. The base of surface casing is at 188.7 m bgs. According to the well completion report, a CBL/VDL was conducted. However, the CBL/VDL is not in the well file. Hence, depth to primary cement and length of uncemented production casing below surface casing is unknown. In September 1982 during recompletion, a packer was set at 1004 m bgs and 1,000 gallons of a 15% HCl solution was used for acid stimulation at 799 m bgs. In October 1982, a cement squeeze was performed above the depth of acid stimulation at 472 m (1550 ft) bgs. The reason for a cement squeeze following stimulation was not provided.

On 3/7/2012, a sundry notice indicated that a MIT was conducted at Tribal 21-15 with "failed casing ...from 735? -1,105?" [ft]. Failed casing was at a depth (224 m bgs) lacking primary cement. It is unclear when casing failed. On 8/14/2012, the WDEQ requested information from the Bureau of Land Management (BLM) on stimulation practices at Tribal 21-15 to evaluate the potential release of stimulation fluid at 224 m bgs (within depths of domestic ground water use). In a response dated 8/23/2012, BLM reiterated previously publicly available information on well completion at this production well thereby providing no additional insight on the potential for release of stimulation fluid through parted casing. The status of casing remediation at this production well is unknown. Bradenhead testing at this production well was either not conducted or documented.

# Unit 41X-10

Unit 41X-10 was completed in January 1973. The base of surface casing is at 188.7 m bgs. A CBL/VDL conducted on 11/22/1972 indicated top of primary cement at approximately 427 m bgs. On 2/7/1973, hydraulic fracturing was conducted at a depth of 551.4 m bgs. From the well completion report, "Frac treated...as follows...9# KCl wtr containing 5# J-133/1000 gal...2500 gal 15% HCl containing 5# J-133/1000 gal...9120 gal 9# KCl wtr containing 40# J-133, 20# J-110 and 1 gal F-63/1000 gal, 1# J-134 and 400 scf/bbl nitrogen...1460 gal 9# KCl wtr containing 560# J-133, 300# J-110, 15 gal F-63, 2 gal J-34 and 139,000 scf nitrogen...flushed w/9# KCl wtr containing 5# J-133/1000 gal...Well flowed back approx. 600 BLW since opened to pit...considerable amt of wtr."

On 2/8/1979, hydraulic fracturing was conducted at a depth of 1232.6 m bgs. While perforating in the Fort Union Formation, "Flowed well to pits continuously...Controlled well w/4% KCl wtr w/clay stabilizer & surfactant. Lost 80 bbls to form while doing so...acdz'd gross perf 4044-4450 w/4000 gals 15% HCl acid...Opened well to pit & cont'd to flw to pit overnight to cleanup." "Foam frac treated with 90,000 gals to qualify foam, 1,950,000 SCF nitrogen & 645 bbls gelled KCl wtr for sd carrying agent. Total load to rec 645 bls."

In correspondence dated 5/27/1980, 41X-10 was recommended for plugging and abandonment (P&A) because of "problems with water production and casing failure." P&A occurred in 1981 with cement plugs. An updated well schematic for Unit 41X-10 appeared in the WOGCC Well Integrity Report³¹. This well schematic did not indicate casing failure. If well casing failure occurred during well stimulation above primary cement, release up through up the uncemented borehole could have occurred at or below the depth of surface casing.

#### Tribal Pavillion 42-10

Tribal Pavillion 42-10 was competed in June 1994 with acid stimulation at depths of 1448, 1620, 1643, and 1669 m bgs. Tribal Pavillion was recompleted in June 2001 with hydraulic fracturing in 7 stages between 1005 and 1380 m bgs. A CBL/VDL conducted on 12/15/2004 indicated top of primary cement at approximately 792 m bgs. The base of surface casing is at 190.8 m bgs. Hence, top of primary cement was 601 m below surface casing.

On 12/15/2004, hydraulic fracturing, ("frac down casing") was conducted at a depth of 807.1 m only 15 m below top of primary cement. The well completion report indicated use of "122 bbls slickwater." A stimulation report, one of only three for the entire field, posted on 8/9/2013, indicated use of "4351 gal 70Q CO2 WF12" consisting of "4351 gal water and 34 lb J216." A Material Safety Data Sheet for "J216" was not provided to EPA. Thus, the chemical composition of this product is unknown.

A cement squeeze was performed on 12/17/2004 (two days after hydraulic fracturing) for "casing remediation" at 774.2 m bgs (18 m above top of primary cement). If well casing integrity failure occurred during well stimulation, upward migration of stimulation fluid could have occurred above the top of primary cement to some undetermined depth below surface casing.

On 12/20/2004, another CBL/VDL was conducted at 3.45 MPa (500 psig). The CBL/VDL indicated high amplitude readings above 741 m bgs with chevrons (pipe connections) visible at 655 m bgs indicating poor casing to cement bonding. On 12/20/2004, 86 barrels of "fluid" was used for hydraulic fracturing at 763 m bgs (22 m below poor cement).

#### Tribal Pavillion 43-10B

Tribal Pavillion 43-10B was completed in January 2005. The base of surface casing is at 193.9 m bgs. A CBL/VDL conducted on 11/8/2004 indicated top of primary cement at 357 m bgs (163 m below surface casing). In November 2005, hydraulic fracturing was conducted over 13 intervals from 552 m to 1667 m bgs using ~80,000 gallons of slickwater with CO₂ assist and CO₂ foam using "WF-12" having a polymer loading of 25 lb/1000 gallons. A cement squeeze was performed subsequent to hydraulic

fracturing on 1/14/2005 at 326.1 m bgs (31 m above the top of primary cement) to repair a "casing leak." If the "casing leak" occurred during well stimulation, upward migration of stimulation fluid could have occurred above the top of primary cement to some undetermined depth below surface casing. The last stimulation stage was on 11/11/2004. Hence, gas was free to migrate through casing to 357 m bgs prior to the cement squeeze more than two months later. Casing and tubing pressure are not provided at the time of well completion.

## Cement Squeezes

Cement squeezes were performed above primary cement after, often days after, hydraulic fracturing without explanation at six production wells. In the absence of an explanation, potential migration of stimulation fluid above primary cement cannot be discounted.

## Pavillion Fee 12-11B

Pavillion Fee 12-11B was completed in January 2005 with the base of surface casing at 167.9 m bgs. A CBL/VDL conducted on 12/29/2004, indicated top of primary cement at  $\sim$  313 m bgs. On 12/29/2004, 110 barrels of " $CO_2$  assisted gelled water" was used for hydraulic fracturing at 429 m bgs. On 1/7/2005, a cement squeeze was performed above primary cement at 283 m bgs.

#### Pavillion Fee 21-10B

Pavillion Fee 21-10B was completed in February 2005 with the base of surface casing at 193.2 m bgs. On 1/6/2005 a CBL/VDL indicated top of primary cement at ~1265 m bgs (1072 m below surface casing). Good bonding ("GOBO") was indicated starting at 1277 m bgs. On 1/12/2005, 168 barrels of "clean fluid" was used for hydraulic fracturing at 1292 m bgs – only 15 m below good bonding. On 1/17/2005 and 1/19/2005, days after hydraulic fracturing, cement squeezes were performed above top of primary cement at 1216 m and 1125 m bgs, respectively. On 1/24/2005, 247 barrels of "clean fluid" was used for hydraulic fracturing at 1049 m and 1079 m bgs. Again, days after hydraulic fracturing, cement squeezes were performed on 1/25/2005 and 1/27/2005 at 928 m and 244 m bgs, respectively.

## Pavillon Fee 34-3B

Pavillion Fee 34-3B was completed in October 2004 with the base of surface casing at 196.6 m bgs. In October 2004, a CBL/VDL indicated top of primary cement at 838 m bgs (641 m below surface casing). In November 2004, "clean fluid" and CO₂ foam was used for hydraulic fracturing between 1039 m and 1637 m bgs. On 4/3/2005, a cement squeeze was performed at 823 m bgs. In this instance, a cement squeeze was apparently performed to enable hydraulic fracturing above primary cement. On

4/19/2005, 139 barrels of slickwater was used for hydraulic fracturing at 951 m bgs. On 4/21/2005, two days after hydraulic fracturing, another cement squeeze was performed at 256 m bgs.

#### Pavillion Fee 31-10B

Pavillion Fee 31-10B was completed in January 2005 with the base of surface casing at 192.0 m bgs. On 12/29/2004 a CBL/VDL indicated top of primary cement at 411 m bgs (219 m below surface casing) with high amplitude readings and a "railroad-like" pattern on the VDL extending to 488 m bgs. On 12/30/2004,  $\sim 36,000$  gallons of slickwater with CO₂ assist was used for hydraulic fracturing between 519 m and 1508 m bgs. Shortly after hydraulic fracturing, cement squeezes were performed on 1/8/2005, 1/13/2005, and 1/18/2005 above primary cement at 381m, 305m, 213 m bgs, respectively.

### Tribal Pavillion 12-12

Tribal Pavillion 12-12 was completed in March 2005 with the base of surface casing at 193.5 m bgs. A CBL/VDL conducted on 2/28/2005 indicated top of primary cement at 290 m bgs (97 m below surface casing). On 3/3/2005, 387 barrels of slickwater was used for hydraulic fracturing from 599 m to 1177 m bgs. On 3/9/2005, cement squeeze performed above primary cement at 259 m bgs.

#### Pavillion Fee 11-11B

Pavillion Fee 11-11B was completed in February 2002 with production casing cemented to the surface. However, a CBL/VDL conducted on 2/8/2002 indicated poor or spotty cement from 320 to 457 m bgs and production casing without cement between 777 m – 960 m bgs. This extensive interval uncemented production casing without cement was noted in the well completion report. On 2/18/2005, 232 barrels of "clean fluid" was used for hydraulic fracturing at 964 m bgs – only 4 m below this interval. A maximum stimulation pressure of only 13 MPa (190 psig) was noted indicating little resistance to flow and likely upward flow of stimulation fluid into the uncemented region.

### D.2 Omissions to Bradenhead Testing

Bradenhead testing was not conducted at John K. Coolidge 1-4, Fike Tribal A-1, Tribal NP 31-11X, Tribal Pavillion 44-3, Tribal Pavillion 15-21X, and Tribal 21-14.

Pressure build-up following detection of brandenhead pressure was not measured at Ora Wells 14-12, Tribal Pavillion 24X-3, Tribal Pavillion 11-10, Tribal Pavillion 23-11, Pavillion Fee 42X-9, Tribal Pavillion 43-2, Pavillion Fee 34-11, Pavillion Fee 34-11, Pavillion Fee 21-10W, Pavillion Fee 11-3, Pavillion Fee 34-3B, and Tribal Pavillion 24-2.

Gas samples at well exhibing bradenhead pressure were not collected at Tribal Pavillion 31-15, IND 14-20-258-41X-2, Tribal Pavillion 33-2, Tribal Pavillion 44-1, Pavillion Fee 44-3C, Tribal Pavillion 32-10, Tribal Pavillion 44-1, and Pavillion Fee 21-10.

## D.3 Summary of Bradenhead Testing with Water Flow

Water flow to the surface during Bradenhead testing occurred at 4 production wells. A summary of events, including information from well completion reports, cement bond/variable density logs (CBL/VDLs), and Sundry Notices is provided below.

### Pavillion Fee 12-11W

Pavillion Fee 12-11W was completed in May 2001 with the base of surface casing at 131.1 m bgs. A CBL/VDL conducted on 4/21/2001 at Pavillion Fee 12-11W indicated top of primary cement at ~594 m bgs (463 m below surface casing). During Bradenhead testing in July 2012, 4,303 barrels (~180,700 gallons) of water flowed to the surface over a 15-day period at Pavillion 12-11W. Bradenhead pressures after 24-hour and 7-day shut-in periods were 85 and 979 kPa (142 psig), respectively. On 10/3/2012, a mechanical integrity test (MIT) was conducted above 764 m bgs (top perforation at 771 m bgs) at 3.4 MPa (500 psig) for 30 minutes – holding pressure without loss, verifying integrity of production well casing. Hence, the source of water was aqueous flow outside production casing at one or more depths. On 5/17/2013, cement squeezes were performed at 146 m and 442 m bgs.

### Tribal Pavillion 13-2

Tribal Pavillion 13-2 was completed in March 2001 with the base of surface at 123.1 m bgs. A CBL/VDL conducted on 2/23/2001 at Tribal Pavillion 13-2, completed in March 2001, indicated top of primary cement at 198 m bgs (75 m below surface casing). During Bradenhead testing in January 2012, pressure after a 7-day shut-in period was 1.45 MPa (210 psig). During testing in July 2012, 3,785 barrels (~159,000 gallons) of water flowed to the surface over a 15-day period. Bradenhead pressures during a 7-day shut-in period was 0.965 MPa (140 psig).

## Tribal Unit 44-10

Tribal Unit 44-10 was completed in December 1979 with the base of surface casing at 184.4 m bgs. A CBL/VDL conducted on 7/23/1979 at Tribal Unit 44-10, completed in December 1979, indicated top of primary cement at ~585 m bgs (401 m below surface casing). During Bradenhead testing in May 2012, 410 barrels (17,200 gallons) of water flowed to the surface during the first 8 hours of a 15-day test period. Bradenhead pressure during subsequent a subsequent 7-day shut-in period was 0.724 MPa (105 psig).

# Tribal Pavillion 13-1

Tribal Pavillion 13-1 was completed in June 2001 with the base of surface casing at 163.1 m bgs. A CBL/VDL was not conducted. Thus of primary cement is unknown. During Bradenhead testing in July 2012, 6 barrels (~250 gallons) of water flowed to surface during the first hour of the 15-day testing period. Subsequent Bradenhead pressure after a 7-day shut-in period was 0.689 MPa (100 psig).

Table SI D1. Major Ions in Produced Water. Data obtained from sundry notices. NA for 33X-10 denotes not analyzed. Bradenhead samples denoted with (B) suffix

Well	Stimulation Dates	n Produced Water. Data obtained from su Stimulation Fluids	Prod	Sample	pН	SC	Na	K	Ca	Mg	Ĉi	SO4	Fe	CO3	HCO3	TDS
Abbrev			Water	Date		(µS/cm)	(mg/l)	(mg/l)	(mg/l)	(mg/l)	(mg/l)	(mg/l)	(mg/l)	(mg/l)	(mg/l)	(mg/l)
	37 2001	Train 1 is 1900	(bbls)	0/0/2007		5.010	1000	9.70		2.0			10.15		0.00	1000
12-1	Nov 2001	KCl solution and CO2	653	8/8/2007	6.86	5,019	1323	270	71	30	1,753	34	48.45	0	903	4,260
14-1	Oct 1964, Apr 1993, Dec 1999	Undiluted diesel fuel, CO2 with methanol, 15% HCl solution	2,735	8/14/2007 7	.15	3,996	785	160	205	29	956	49	190.60 0		902	3,325
22-1	Nov 2001	CO2 foam	892	8/8/2007	7.71	3,389	945	34	44	11	882	9	12.07	0	1,001	2,771
24-1	Mar 2001	No information on stimulation	817	8/8/2007	8.71	3,389	970	112	12	7	985	7	4.81	68	978	2,771
33-1	Sep 2001	No information on stimulation	3,176	8/8/2007	7.70	3,684	916	78	46	13	821	12	8.67	0	907	3,040
43-1	Aug 2001	WF125 in 6% KCl solution and CO2 foam	8,500	8/8/2007	7.73	2,322	667	21	15	4	503	5	1.97	10	919	1,796
44-1	Mar 2001	No information on stimulation	1375	8/8/2007	7.73	3,934	1051	94	39	13	1,263	8	13.87	0	737	3,269
24-2	Oct 2004	"clean fluid" and CO2	174	8/13/2007 8	.28	4,940	1,479	202	29	14	1,774	7	0.25	7	1,235	4,188
32-2	Mar 2006	6% KCl solution, CO2, surfactant	4450	8/13/2007 6		3,823	768	268	67	14	817	11	57.90	0	807	3,167
33-2	Oct 1994, Oct 2000	15% HCl solution, "clean fluid", N2	1,263	8/13/2007 8		2,703	769	57	18	8	853	6	31.58	20	614	2,144
11-3	Dec 2001	6% KCl solution, CO2 foam, gel	1,895	8/13/2007 8		2,107	596	45	10	3	366	8	2.63	14	963	1,600
13-3W	Apr 2005	slickwater	1340	8/20/2007 6		5,702	1060	233	25	21	1,315	485	165.05 0		899	4,884
14-3W	Apr 2002	6% KCl solution, CO2, gel	5,695	8/14/2007 8		4,813	1538	88	7	7	1,089	8	4.11	12	2,243	4,072
24X-3	Nov 1965, Jun 1966	"P-12 solvent"	9653	8/14/2007 8		5,159	1572	47	2	3	1,094	17	5.95	11	1,094	4,388
31X-3	Aug 2001	unknown	1,215	8/13/2007 8		2,512	647	153	13	6	595	34	0.00	0	802	1,970
32-3	May 2005	6% KCl solution, CO2	50,290	8/13/2007 8		3,706	1264	17	13	3	1,194	4	4.82	35	1,072	3,060
33-3	May 1999	No information on stimulation	337	8/13/2007 8		3,270	1072	53	7	4	574	43	5.00	159	1,496	2,662
44-3	Apr 1999	15% HCl solution, 2% KCl solution	1,663	8/13/2007 8		2,364	697	20	19	4	387	5	4.48	11	1,113	1,834
1-4	May 1982	15% HCl soln, 3% HF soln, NH4Cl solution, foam.	10,417	8/20/2007 8		2,438	608	81	22	6	585	135	2.00	0	788	1,902
	1114, 1702	Possible recompletion in 2005	10,117	0.20.2007 0	ľ	2,130	000	"			505	***	2.00		1,00	1,,,,,
42-4B	Apr 2005	6% KCl solution, CO2, "clean fluid"	8,857	8/20/2007 8	.13	2,252	615	34	25	7	603	17	1.75	0	763	1,732
43-4	Mar 2005	70Q cross-linked gel	19,681	8/20/2007 8		3,343	1044	59	12	4	915	16	6.57	0	1,402	2,729
12-5	May 2001	WF125 in 6% KCl and 10% methanol solution, CO2	3402	8/8/2007	8.88	2,874	903	87	3	3	797	2	1.17	100	1,067	2,300
	´	foam													<b>'</b>	′
12-7	Sep 2001	No information on stimulation	118	8/8/2007	5.93	10,022	2379	462	284	102	4,365	22	46.00	0	432	8,830
41-9	Aug 1979, Oct 2004	6% KCl solution, 70Q CO2 WF125, 7 1/2% HCl	15,593	8/20/2007 8	.29	2,342	654	30	18	5	693	6	3.94	17	615	1,814
		solutions														
42X-9	Feb 1999	No information on stimulation	10,083	8/20/2007 8	.15	7,739	2247	106	9	7	793	13	13.72	0	4,301	6,745
12-10	Oct 2001	WF125, 6% KCl solution, CO2 foam	1,465	8/20/2007 8	.08	2,876	827	90	10	6	808	9	7.52	29	1,012	2,302
14-10	Apr 2001	6% KCl and 10% methanol solution with additives and CO2	3,225	9/19/2007 6	.30	6,661	1770	116	284	41	1,202	1,960	150.90 0		1,739	5,760
23-10W	Dec 2002	KCl solution, CO2	5,892	8/20/2007 8	.00	3,742	1054	86	12	5	694	46	4.46	0	1,783	3,093
31-10 W	Jun 1994, Jan 2002	6% KCl solution, CO2 foam, 7 ½ HCl solution	15,504	8/20/2007 8		4,639	1497	25	13	6	1,044	6	14.39	12	2,025	3,913
32-10B	Mar 2002	6% KCl solution, CO2	4,727	8/14/2007 8		5,063	1593	17	10	6	1,022	4	3.36	10	2,023	4,300
32-10D 32-10C	Feb 2005	WF125 with CO2	7,099	8/20/2007 8		1,779	421	15	15	3	131	175	1.82	0	630	1,300
33X-10	Feb 1965	"MCA", 15% HCl solution	7,022	3/29/1965 N		NA	1298	NA	11	3	940	305	NA	72	1.342	3,971
33-10	Apr 1999	6% KCl solution, CO2, linear gel, 15% HCl solution	2,547	8/20/2007 7		4,409	1220	218	12	6	894	46	5.03	0	2,254	3,703
41-10	Jan 2002	6% KCl solution, CO2 foam	157	8/14/2007 5		21,177	2499	1,911	1,771	131	5,945	2.063	70.60	0	3.358	19,020
43-10	Sep 1994, Feb 2002	6% KCl solution, CO2 foam, gel	28,467	8/28/2007 6		5,064	1656	57	6	3	1,280	292	71.95	0	1,873	4,301
11-11	May 2001	WF125 in 6% KCl and 10% methanol with CO2 foam	9,051	8/13/2007 7		2477	656	68	30	5	432	12	59.80	0	1,048	1,938
		and additives														
12-11	Oct 1993, Nov 2004	2% KCl solution, CO2 foam	8,451	8/14/2007 7		2,576	753	120	22	6	411	135	50.25	0	1,062	2,028
12-11B	Dec 2004	CO2 with gelled water	731	8/14/2007 8		2,941	816	194	11	9	633	7	5.66	31	1,296	2,362
21-11	Mar 1979	2, 3, and 7 ½% HCl solutions with additives, "YE4P5D fluid"	335	8/13/2007 7	.61	3,304	938	123	40	11	1,079	9	27.45	0	762	2,693
44-11	Feb 2002	6% KCl solution with CO2 foam and gel	1,643	8/28/2007 5	.59	2,140	510	29	39	3	363	255	109.20 0	Ì	647	1,630
33-12	Mar 2006	6% KCl solution, CO2, "clean fluid"	5520	8/14/2007 7		2,718	745	84	18	8	611	43	4.47	0	993	2,158
42X-12	Jan 1974	15% HCl solution, Possible recompletion in 2004	295	8/14/2007 7		1,619	303	144	23	3	545	14	13.30	0	90	1,154
21-14	Dec 2004	Slickwater with CO2	1,886	8/28/2007	7.53	5,242	1361	253	55	15	1,522	7	4.80	0	1,431	4,464
13-1 <b>(B)</b>		The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	1,000	4/26/2012	10.86	,	2700	6000	39	1.6	88	2100	1.67	17000	<2	30000
13-2 <b>(B)</b>				4/24/2012	9.57	1341	230	3.7	32	2.7	53	170	7.36	110	290	900
~ (1)	1	<del> </del>	<b>I</b>													
44-10 <b>(B)</b>				4/23/2012	8.64	903	280	9.6	15	2.3	7.1	16	6.45	40	240	500

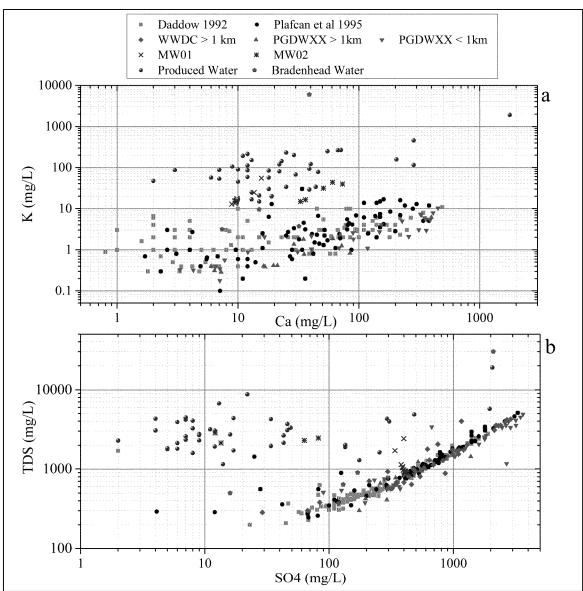
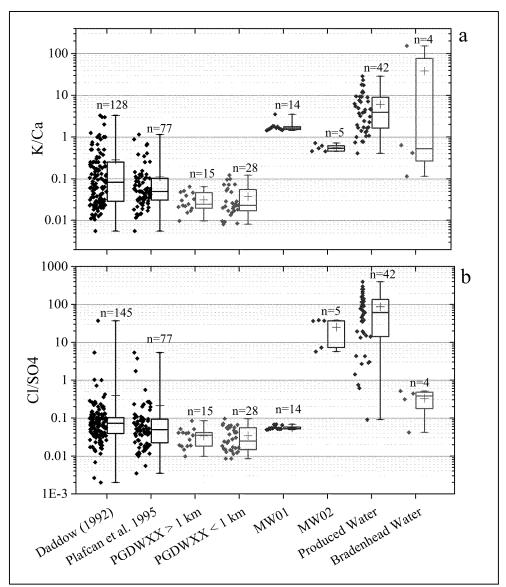


Figure SI D1. (a) Potassium concentration as a function of calcium concentration and (b) total dissolved solids (TDS) concentration as a function of sulfate concentration for the Wind River Indian Reservation (Daddow 1992)⁵, Fremont County (Plafcan et al. 1995)²⁶, domestic wells sampled by the Wyoming Water Development Commission (WWDC) greater than 1 km from production wells, domestic wells (PGDWXX) less than and greater than 1 km from production wells, EPA monitoring wells MW01 and MW02, produced water samples, and bradenhead water samples. Mean values are represented for domestic well locations sampled more than once. Produced water and bradenhead locations were sampled once. Measurement at MW01 and MW02 represent samples collected during Phase III, IV, and V sample events to illustrate variability. TDS values for PGDWXX wells estimated from Daddow (1995) TDS (mg/L) = 0.785*specific conductance (μS/cm)-130 (n=151,  $r^2$ =0.979)



**Figure SI D2.** (a) Ratio of potassium to calcium and (b) chloride to sulfate concentrations for the Wind River Indian Reservation (Daddow 1992)⁵, Fremont County (Plafcan et al. 1995)²⁶, domestic wells (PGDWXX) less than and greater than 1 km from production wells, EPA monitoring wells MW01 and MW02, produced water samples, and bradenhead water samples. Mean values are represented for domestic well locations sampled more than once. Produced water and bradenhead locations were sampled once. Measurement at MW01 and MW02 represent samples collected during Phase III, IV, and V sample events to illustrate variability.

**Table SI D2.** String gas and bradenhead gas samples collected at production wells having sustained casing pressure. Concentrations in mole fractions x 100. Data obtained using API number in Table SI C1

API num	ber in Tab	le SI C	1												<b>4</b> 100000011000100010			A	•				
Well	Sample Date	Gauge Pressure (MPa)	T (C)	Nitrogen	Carbon Dioxide	Methane	Ethane	Propane	iso-butane	Butane	iso-pentane	Pentane	Hexanes	Heptanes	Octanes	Nonanes	Decanes +	Benzene	Toluene	Ethylbenzene	xylenes	wns	C1/C1-C5)
String Gas	Samples																						
13-1	6/11/2012	0.31	19	0.7266	0.0000	91.9740	4.7594	1.3181	0.4097	0.3223	0.1541	0.0885	0.0968	0.0780	0.0443	0.0030	0.0000	0.0116	0.0099	0.0004	0.0035	100.0002	0.934104
22-1	6/11/2012	2.69	19	0.8759	0.0709	92.8305	4.8352	0.0000	0.4877	0.4158	0.1787	0.1067	0.0997	0.0598	0.0259	0.0018	0.0000	0.0095	0.0003	0.0001	0.0014	99.9999	0.945434
13-2	3/5/2012	0.04	?	0.5499	0.0947	91.0554	4.3084	1.5168	0.5086	0.4560	0.3103	0.1995	0.3069	0.2921	0.2429	0.0188	0.0547	0.0331	0.0390	0.0006	0.0123	100.0000	0.933556
13-2B 32-2	6/21/2012 6/21/2012	0.10 0.26	29 27	0.7071 0.6555	0.0733 0.0052	91.0681 92.4055	4.8186 4.4755	1.4356 1.1925	0.4963 0.3879	0.4280 0.3180	0.2419 0.1612	0.1538 0.0966	0.1977 0.1117	0.1692 0.0908	0.1231 0.0596	0.0141	0.0053 0.0017	0.0267 0.0140	0.0231 0.0115	0.0013	0.0168	100.0000 100.0002	0.930177 0.93824
33-2B	3/5/2012	0.00	21	0.6409	0.0940	92.1420	4.4226	1.3698	0.3864	0.3142	0.1595	0.0954	0.1176	0.1014	0.0925	0.0131	0.0123	0.0129	0.0138	0.0008	0.0108	100.0000	0.936936
13-3W	4/4/2012	0.26	15	0.3936	0.0502	91.7674	4.4037	1.5981	0.4771	0.4425	0.2330	0.1477	0.1640	0.1525	0.0942	0.0117	0.0045	0.0236	0.0215	0.0027	0.0122	100.0002	0.93298
22-3	6/11/2012	0.37	19	0.6833	0.0005	94.3455	3.3703	0.6320	0.2546	0.1749	0.1493	0.0771	0.1324	0.1120	0.0416	0.0047	0.0022	0.0149	0.0003	0.0014	0.0030	100.0000	0.956853
32-3	4/4/2012	0.27	13	0.3921	0.1865	94.5473	3.6026	0.8409	0.1526	0.1131	0.0410	0.0218	0.0259	0.0323	0.0220	0.0037	0.0018	0.0048	0.0060	0.0006	0.0049	99.9999	0.953812
44-3C	4/4/2012	1.79	21	0.4216	0.1036	94.4928	3.3318	0.8565	0.2389	0.1772	0.0932	0.0517	0.0695	0.0763	0.0559	0.0069	0.0000	0.0125	0.0072	0.0006	0.0040	100.0002	0.955341
43-4	4/4/2012	0.22	18	0.3756	0.0295	95.5235	3.1025	0.5134	0.1551	0.0871	0.0564	0.0247	0.0438	0.0485	0.0261	0.0037	0.0005	0.0060	0.0019	0.0002	0.0015	100.0000	0.962442
44-4 12-5	4/4/2012 6/11/2011	0.26 2.96	18 19	0.3952 0.9390	0.1602 0.0000	93.4057 91.3650	3.4166 4.9090	1.2606 1.5679	0.4024 0.4548	0.2753 0.3678	0.1580 0.1574	0.0866 0.0912	0.1206 0.0803	0.1420 0.0419	0.0984 0.0172	0.0193	0.0096	0.0211	0.0127	0.0054	0.0102	99.9999 99.9999	0.948813 0.929442
43-9	4/4/2012	0.32	19	0.5128	0.6048	93.4457	3.6813	0.9650	0.2221	0.1402	0.0846	0.0912	0.0803	0.0989	0.0663	0.0013	0.0032	0.0167	0.0119	0.0002	0.0009	100.0000	0.950869
13-10	12/23/2011	0.28	-12	0.4951	0.0592	93.8277	3.7263	0.9381	0.2886	0.2159	0.1154	0.0656	0.1011	0.1036	0.0596	0.0000	0.0000	0.0021	0.0020	0.0000	0.0000	100.0003	0.949927
31-10	5/14/2012	0.65	-11	0.3529	0.0006	93.9675	3.8277	0.9373	0.3053	0.2356	0.1307	0.0653	0.0851	0.0703	0.0190	0.0000	0.0000	0.0024	0.0003	0.0000	0.0000	100.0000	0.948847
32-10C	3/5/2012	?	?	0.4696	0.1336	94.0435	3.5933	0.8749	0.2624	0.1923	0.1063	0.0628	0.0875	0.0693	0.0518	0.0010	0.0330	0.0097	0.0087	0.0000	0.0002	99.9999	0.952177
41-10B	3/2/2012	0.22	21	0.5704	0.0467	92.6355	4.2192	1.0353	0.3903	0.3289	0.1784	0.1130	0.1568	0.1450	0.1242	0.0106	0.0039	0.0174	0.0194	0.0044	0.0007	100.0001	0.94207
42-10B 44-10	3/5/2012 4/23/2012	0.30	-11	0.4577 0.3580	0.0592 0.2090	93.3702 95.0794	3.8301 3.5282	1.1094 0.4236	0.3318 0.1392	0.2681 0.0760	0.1430 0.0502	0.0841 0.0222	0.1161 0.0462	0.1048 0.0445	0.0851 0.0208	0.0083	0.0044	0.0126	0.0116	0.0031	0.0004	100.0000 100.0000	0.946365 0.959144
12-11	6/25/2012	0.19	14	0.3545	0.3991	95.1965	3.0569	0.3532	0.1780	0.0498	0.0302	0.0222	0.0402	0.1036	0.0200	0.0000	0.0040	0.0013	0.0005	0.0006	0.0034	100.0000	0.964678
12-11W	6/11/2012	0.18	19	0.4691	0.0575	94.1256	3.3829	0.8745	0.2632	0.2075	0.1173	0.0695	0.1113	0.1372	0.1090	0.0133	0.0133	0.0194	0.0163	0.0009	0.0122	100.0000	0.95404
21-11	6/11/2012	0.17	19	0.4672	0.1165	94.1805	3.7227	0.0000	0.3247	0.2825	0.1680	0.1070	0.1679	0.1887	0.1626	0.0231	0.0081	0.0274	0.0280	0.0023	0.0229	100.0001	0.958164
32-11	10/6/2011	0.22	13	0.5223	0.0097	93.7030	3.8213	0.9190	0.3210	0.2361	0.1410	0.0732	0.0947	0.0793	0.0513	0.0029	0.0000	0.0139	0.0089	0.0025	0.0000	100.0001	0.948866
41-11B	3/2/2012	0.21	?	0.8591	0.1052	92.4548	3.9281	0.7011	0.4578	0.3977	0.2541	0.1654	0.2434	0.1975	0.1412	0.0085	0.0386	0.0230	0.0209	0.0026	0.0009	99.9999	0.946826
	ad Gas Samp			T	T	T		T	T					T		T	T	T	T	T			
13-1 BH 22-1 BH	6/11/2012 6/11/2012	0.33 0.15	19 19	2.8060 3.0339	0.0000	92.2935 91.4958	3.9441 3.8633	0.0000	0.3635 0.3655	0.2491 0.0565	0.1345 0.1382	0.0674 0.0025	0.0757 0.0328	0.0390 0.0161	0.0173 0.0179	0.0025	0.0000	0.0069	0.0001	0.0004	0.0000	100.0000 100.0001	0.955873 0.949195
13-2 BH	3/5/2012	?	?	3.4581	0.0000	90.7353	3.8201	1.0743	0.3865	0.2301	0.1382	0.0023	0.0528	0.0285	0.0179	0.0020	0.0001	0.0001	0.0003	0.0000	0.0005	100.0001	0.945975
13-2B BH	6/21/2012	1.17	31	0.7833	0.0000	92.4048	4.5145	1.2547	0.4110	0.3039	0.1178	0.0788	0.0668	0.0272	0.0093	0.0008	0.0000	0.0037	0.0013	0.0001	0.0014	100.0001	0.93758
32-2 BH	6/21/2012	0.72	26	0.6373	0.0000	92.4717	4.2972	1.1004	0.3680	0.2957	0.1703	0.1059	0.1694	0.1836	0.1302	0.0072	0.0002	0.0297	0.0253	0.0009	0.0070	100.0000	0.940988
33-2B BH	3/5/2012	0.00	21	0.7500	0.0000	91.9483	4.5196	1.4354	0.3864	0.3251	0.1814	0.1162	0.1582	0.1029	0.0503	0.0000	0.0056	0.0123	0.0080	0.0000	0.0002	99.9999	0.93496
13-3W BH	4/4/2012	0.19	18	0.5851	0.0000	92.4747	4.1781	1.6185	0.3771	0.3383	0.1425	0.0863	0.0788	0.0592	0.0371	0.0049	0.0007	0.0082	0.0064	0.0004	0.0037	100.0000	0.936966
22-3 BH	6/11/2012	0.07	19	0.7972	0.0000	92.2055	4.3671	1.4490	0.3797	0.3076	0.1496	0.0874	0.0941	0.0685	0.0377	0.0117	0.0125	0.0111	0.0078	0.0042	0.0093	100.0000	0.93689
32-3 BH 44-3C BH	4/4/2012 4/4/2012	1.51 1.24	12 13	0.6943 0.7282	0.0000	93.1825 92.5420	4.3036 4.4161	1.1017 1.3389	0.3078 0.3818	0.2283 0.3086	0.0891 0.1263	0.0444 0.0694	0.0274 0.0529	0.0106 0.0222	0.0062 0.0081	0.0005 0.0006	0.0005 0.0001	0.0015 0.0031	0.0011	0.0005	0.0001 0.0004	100.0001 99.9997	0.942566 0.937846
43-4 BH	4/4/2012	0.81	18	1.0322	0.0000	92.4099	4.3012	1.4523	0.3484	0.3080	0.1203	0.0034	0.0323	0.0222	0.0072	0.0000	0.0002	0.0031	0.0010	0.0008	0.0004	99.9999	0.938331
44-4 BH	4/4/2012	0.48	18	0.7962	0.0000	91.2149	4.5748	1.8933	0.5013	0.4390	0.1898	0.1209	0.1229	0.0870	0.0418	0.0027	0.0003	0.0112	0.0036	0.0001	0.0000	99.9998	0.928463
12-5 BH	6/11/2011	0.00	19	99.4568	0.0503	0.1119	0.0111	0.3174	0.0074	0.0052	0.0081	0.0069	0.0132	0.0060	0.0043	0.0000	0.0002	0.0012	0.0000	0.0000	0.0000	100.0000	0.247293
43-9 BH	4/4/2012	0.17	17	1.5314	0.0002	90.4485	4.2953	2.0623	0.6302	0.4586	0.2044	0.1247	0.1145	0.0731	0.0352	0.0035	0.0005	0.0105	0.0041	0.0002	0.0028	100.0000	0.92873
13-10 BH	12/23/2011	0.16	-12	1.3915	0.0000	91.9284	3.9110	1.4602	0.4180	0.3632	0.1730	0.1094	0.1271	0.0540	0.0310	0.0000	0.0000	0.0328	0.0003	0.0000	0.0000	99.9999	0.94023
31-10 BH	5/14/2012	0.14	-12	0.8255	0.0005	92.0103	4.5227	1.5013	0.3920	0.3318	0.1379	0.0830	0.0826	0.0602	0.0370	0.0099	0.0000	0.0011	0.0020	0.0024	0.0000	100.0002	0.934598
32-10C BH 41-10B BH	3/5/2012 3/2/2012	0.07 1.17	21 21	1.4023 0.7897	0.0000	92.2150 93.3746	4.0826 4.2654	1.3552 0.9129	0.3486 0.2833	0.2593 0.2509	0.1280 0.0666	0.0720 0.0303	0.0711 0.0150	0.0373 0.0061	0.0153	0.0018	0.0041	0.0047	0.0018	0.0005	0.0003	99.9999 100.0000	0.941122 0.944761
41-108 BH 42-108 BH	3/2/2012	0.07	?	1.1921	0.0000	93.3746	4.2654	1.3753	0.2833	0.3002	0.1512	0.0303	0.0150	0.0061	0.0000	0.0000	0.0006	0.0009	0.0034	0.0000	0.0003	100.0000	0.944761
44-10 BH	4/23/2012	0.14	-11	1.3997	0.0000	91.5877	4.2577	1.5803	0.4681	0.3907	0.1312	0.0727	0.0600	0.0342	0.0100	0.0000	0.0000	0.0003	0.0001	0.0000	0.0002	99.9998	0.935627
12-11 BH	6/25/2012	0.33	19	0.7963	0.0000	93.8511	3.7449	0.8768	0.2674	0.1839	0.0988	0.0524	0.0618	0.0406	0.0166	0.0022	0.0002	0.0066	0.0001	0.0002	0.0000	99.9999	0.950785
12-11W BH	6/11/2012	0.76	19	0.9415	0.0000	92.7397	4.2221	1.1349	0.3341	0.2626	0.1281	0.0743	0.0792	0.0511	0.0219	0.0022	0.0002	0.0074	0.0001	0.0003	0.0003	100.0000	0.942155
21-11 BH	6/11/2012	0.83	19	1.2156	0.0000	93.7351	3.8083	0.8327	0.1713	0.1057	0.0367	0.0189	0.0186	0.0236	0.0218	0.0031	0.0003	0.0037	0.0004	0.0004	0.0039	100.0001	0.951619
32-11 BH	10/6/2011	0.07	11	3.1695	0.0000	85.6361	4.8457	2.5594	1.1795	1.1772	0.7327	0.4374	0.1702	0.0403	0.0228	0.0066	0.0033	0.0023	0.0074	0.0010	0.0085	99.9999	0.904711
41-11B BH	3/2/2012	0.97	?	1.0533	0.0000	92.7414	4.3634	0.7554	0.3824	0.2953	0.1407	0.0796	0.0849	0.0514	0.0255	0.0025	0.0125	0.0060	0.0048	0.0000	0.0010	100.0001	0.944076

# D.6 Summary of Organic Compounds Detected in Produ ced Water Samples

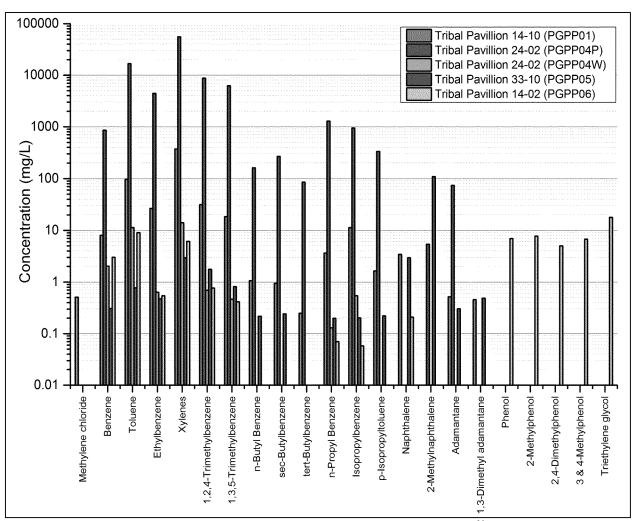
Table SI D3. Summary of organic compounds detected in produced water by EPA Region 8 and Zymax (contractor

to EPA³⁰). PGPPXX are EPA sample identification codes.

	Tribal Pavillion 14-10 (PGPP01) EPA R8	Tribal Pavillion 24-2 (PGPP04P) EPA R8	Tribal Pavillion 24-22 (PGPP04W) Zymax	Tribal Pavillion 33-10 (PGPP05) EPA R8	Tribal Pavillion 33-10 (PGPP05) Zymax	Tribal Pavillion 14-2 (PGPP06) EPA R8	Tribal Pavillion 14-2 (PGPP06) Zymax
Volatile Analysis (mg/L)							•
Methylene chloride	0.51 J	<50 U	NA	<0.025 U	NA	<0.025 U	NA
Benzene	8.02 J	860 J	2.053	0.306 J	0.379	3.02 J	1.953
Toluene	97.5 J	16800 J	11.329	0.774 J	1.284	9.07 J	7.288
Ethylbenzene	26.6 J	4410 J	0.632	0.476 J	0.579	0.542 J	0.262
m,p-Xylene	298 J	46000 J	11.513	2.18 J	3.684	4.76 J	4.292
o-Xylene	73.6 J	9430 J	2.64	0.797 J	1.307	1.37 J	1.1
1,2,4-Trimethylbenzene	31.6 J	8730 J	0.695	1.77 J	2.621	0.765 J	0.632
1,3,5-Trimethylbenzene	18.6 J	6250 J	0.465	0.818 J	1.566	0.414 J	0.366
n-Butyl Benzene	1.06 J	162 J	< 0.005	0.218 J	0.179	<0.025 U	< 0.050
sec-Butylbenzene	0.95 J	270 J	0.007	0.243 J	0.655	<0.025 U	0.062
tert-Butylbenzene	0.25 J	86 J	NA	<0.025 U	NA	<0.025 U	NA
n-Propyl Benzene	3.64 J	1290 J	0.13	0.198 J	0.803	0.07 J	0.11
Isopropylbenzene	11.4 J	948 J	0.542	0.202 J	3.427	0.058 J	0.337
p-Isopropyltoluene	1.64 J	334 J	NA	0.222 J	NA	<0.025 U	NA
Naphthalene	3.43 J	<200 U	<0.005 U	2.97 J	< 0.050	0.21 J	< 0.050
Adamantane	0.52 J	74 J	NA	0.305 J	NA	<0.025 U	NA
1,3-Dimethyl adamantane	0.46 J	<50 U	NA	0.488 J	NA	<0.025 U	NA
Semivolatile Analysis (mg/L)							
Phenol	NA	<2.0 U	NA	<2.0 U	NA	6.96 J	NA
2-Methylphenol	NA	<2.0 U	NA	<2.0 U	NA	7.76 J	NA
2,4-Dimethylphenol		<2.0 U	NA	<2.0 U	NA	5.00 J	NA
3 & 4-Methylphenol	NA	<2.0 U	NA	<2.0 U	NA	6.76 J	NA
Naphthalene	NA	30 J	NA	37.8 J	< 0.050	<0.40 U	NA
2-Methylnaphthalene	NA	5.4 J	<0.005 U	110 J	< 0.050	<0.40 U	NA
Adamantane	NA	47.2 J	NA	6.4 J	NA	<1.12 U	NA
1,3-Dimethyl adamantane	NA	9.8 J	NA	8.2 J	NA	<1.12 U	NA
Triethylene glycol	ND	ND	NA	ND	NA	17.8 (TIC) N	À

J – estimated concentration

U – below reporting limit
TIC – tentatively identified compound



**Figure SI D3.** Organic compounds (volatile and semivolatile analyses) detected by EPA³⁰ in produced water at Tribal Pavillion 14-10 (PGPP01), Tribal Pavillion 33-10 (PGPP05) and Tribal Pavillion 14-02 (PGPP06) and product present with water at Tribal Pavillion 24-02 (PGPP04P). Triethylene glycol was a tentatively identified compound (gas chromatography area at least 10% as large as the area of the nearest internal standard and a mass spectrometry match quality greater than 90%).

### E – EPA Monitoring Well Construction, Purging, and Sample Results

### E.1 Monitoring Well Construction

In June 2010, EPA installed two monitoring wells, MW01 and MW02, using mud rotary drilling. Monitoring well construction schematics for MW01 and MW02 are provided in Figures SI E1 and SI E2, respectively. We modified schematics previously illustrated in EPA's draft report²⁷ to be more consistent with the prime contractor (Shaw Environmental) and subprime contractor (Boart-Longyear) and USGS (during redevelopment) daily logs. We typed and chronologically combined handwritten daily logs (not provided here) to gain a better understanding of activities during monitoring well construction.

## Water Used for Drilling Mud

Boart-Longyear used a water supply truck to transport municipal water from Riverton, WY to mix bentonite for MW01 and MW02. This truck was not used for any other purpose. Water was not stored in tanks prior to use. Municipal water was sampled by the City of Riverton on 7/26/2010 (the same time as drilling). It is unlikely that water used to mix drilling mud impacted analytical results at MW01 and MW02 for the following reasons. (1) No volatile petroleum hydrocarbons were detected. The reporting limit for benzene, toluene, ethylbenzene, o-xylene, m, p-xylenes, naphthalene, 1,2,4-trimethylbenzene, and 1,3,5-trimethylbenzene was 0.50 μg/L. (2) With the exception of chlorine disinfection products, choroform and trihalomethanes, detected at 2.3 and 2.7 μg/L respectively, no other volatile organic compounds were detected. Choroform and trihalomethanes were not detected in aqueous samples from MW01 and MW02 indicating loss of these compounds via volatilization and/or degradation during drilling. (3) No semivolatile organic compounds were detected. (4) No additives (e.g., biocides) were added to the water during transport and use.

### Additives Used for Drilling Mud

Boart-Longyear used a number of additives (Table SI E1) in water-based drilling mud to avoid heaving of shale and a product, Aqua-Clear PFD, to facilitate removal of mud after drilling. MSDSs indicated that: (1) Quik-Gel was comprised of bentonite (60%), crystalline silica quartz (1-5%), crystalline silica cristobalite (0-1%), and crystalline silica tridymite (0-1%); (2) EZ-Mud Gold contained "no hazardous substances"; (3) Quik-Trol Gold was a cellulose derivative with a 60-100% polysaccharide concentration; (4) dense soda ash was 100% sodium carbonate (Na₂CO₃); (5) Penetrol contained 1-5% of diethanolamine and 10-30% coco diethanolamide; and (6) Aqua-Clear contained 30-60% of an anionic polyacrylamide.

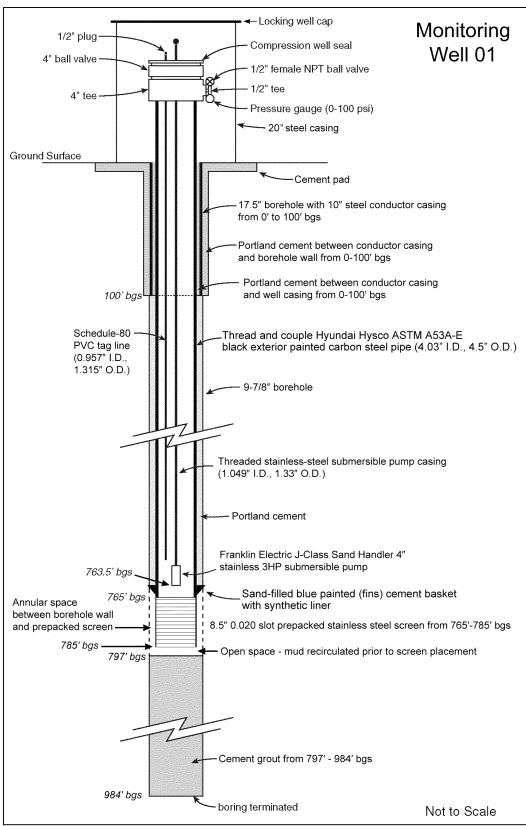


Figure SI E1. Well schematic for MW01 modified from EPA²⁷

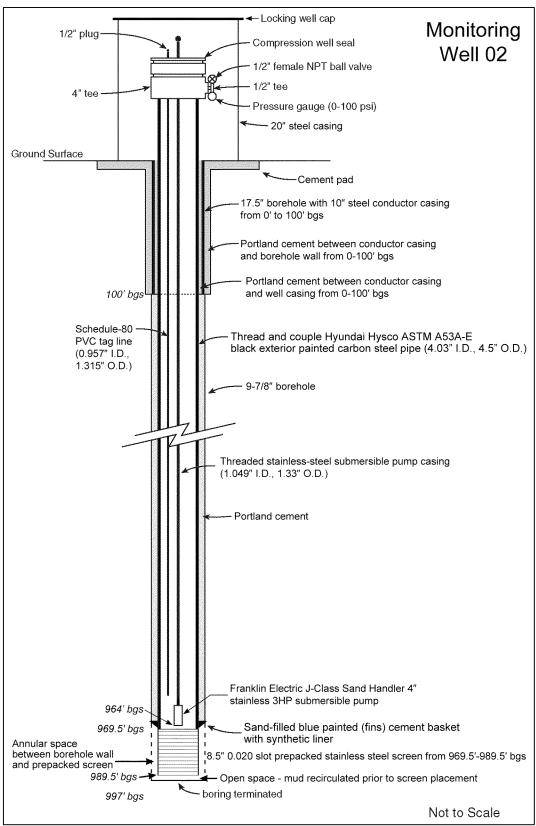


Figure SI E2. Well schematic for MW02 modified from EPA²⁷

**Table SI E1.** Summary of products used for mud rotary drilling, mass ratios of product use, analyses of aqueous extracts of products, and maximum concentration of detection in MW01 and MW02.

Parameter	Aqua-Clear PFD	Penetrol	EZ-Mud Gold	Dense Soda Ash	Quik-Gel	Quik-Trol Gold	MW01	MW02
Manufacturer	Haliburton	Haliburton H		OCI Chemicals		Haliburton		
Specified use of additive	Dispersant – assist mud removal		shale/clay stabilizer	Спетисиз	bentonite	clarifier		
form	liquid	liquid	solid	solid	solid	solid		
mass ratio in extract	1:20	1:20	1:100	1:100	1:100	1:100		
mass ratio in water used for mud or development at MW01	1:467	1:2347	1:236	1:1211	1:36	1:634		
Normalization factor for MW01	23.4	117.6	2.36	12.1	0.36	6.34		
mass ratio in water used for mud or development at MW02	1:467	not used	1:1252	not used	1:36	1:1252		
Normalization factor for MW02	23.4		12.5		0.36	12.5		
Concentration in Aqueous 1	Extract and Estimate	d Concentration	in Aqueous P	ortion of Drilli	ng Mud in Par	enthesis	Max	imum
Upper and	d Lower sets of conce	ntrations refer	to MW01 and I	MW02, respect	ively		Concen	tration in
								ing Wells
pH of aqueous extract of product	7.96	8.51	6.64	11.2	8.35	NA	11.9	12
Specific Conductance (mS/cm)	13.3 (0.57) 13.3 (0.57)	0.47 (0.004) not used	0.24 (0.10) 0.24 (0.02)	15.5 (1.28) not used	0.20 (0.56) 0.20 (0.56)	NA NA	3.265	3.812
DOC (mg/L)	1640 (70.2)	1500 (12.78)	388 (164)	0.58 (0.05)	2.11 (5.86)	NA	9.43	19.7
	1640 (70.2)	not used	388 (31.0)	not used	2.11 (5.86)	NA		
Cl (mg/L)	214 (9.16)	85 (0.72)	2.22 (0.94)	7.03 (0.58)	ND	NA	23.3	466
	214 (9.16)	not used	2.22 (0.18)	not used	ND	NA		
SO ₄ (mg/L)	121 (5.18)	597 (5.09)	ND	ND	3.53 (9.81)	NA	428	81.8
	121 (5.18)	not used	ND	ND	3.53 (9.81)	NA		
K (mg/L)	0.40 (0.02)	0.63 (0.005)	1.16 (0.49)	0.12 (0.01)	0.09 (0.25)	NA	54.9	44.0
	0.40 (0.02)	not used	1.16 (0.09)	not used	0.09 (0.25)	NA		
acetone (µg/L)	ND	ND	ND	NA	NA	NA	79.5	1460
	ND	ND	ND	NA	NA	NA		
tert-butyl alcohol (µg/L)	ND	ND	ND	NA	NA	NA	< 5.0	6120
	ND	ND	ND	NA	NA	NA		
isopropanol (μg/L)	85(J) (3.64)	43(J) (0.37)	27(J) (11.4)	NA	NA	NA	212	862
d 17 (7)	85(J) (3.64)	not used	27(J) (2.16)	NA	NA	NA	.1.00	7.40
ethanol (μg/L)	59(J) (2.53)	58(J) (0.49)	ND	NA NA	NA	NA NA	<1.00	7.49
benzene (μg/L)	59(J) (2.53) ND	not used ND	ND ND	NA NA	NA NA	NA NA	<0.50	246
benzene (µg/L)	ND ND	ND ND	ND ND	NA NA	NA NA	NA NA	\0.50	240
toluene (µg/L)	ND ND	ND ND	ND ND	NA NA	NA NA	NA NA	< 0.50	677
tordene (µg/L)	ND ND	ND ND	ND	NA NA	NA NA	NA NA	\0.50	077
ethylbenzene (µg/L)	ND	ND	ND	NA	NA	NA	< 0.50	101
emproenzene (µg/2)	ND	ND	ND	NA	NA	NA	10.50	101
xylenes (μg/L)	ND	ND	ND	NA	NA	NA	< 0.50	1063
-3 (48 –)	ND	ND	ND	NA	NA	NA		
trimethylbenzenes (µg/L)	ND	ND	ND	NA	NA	NA	<1.00	265
40 /	ND	ND	ND	NA	NA	NA		
naphthalene	ND	2.00 (0.02)	ND	NA	NA	NA	<1.00	7.2
•	ND	not used	ND	NA	NA	NA		
ethylene glycol (μg/L)	ND	ND	ND	NA	NA	NA	<5000 <	5000
	ND	ND	ND	NA	NA	NA		
diethylene glycol (µg/L)	ND	ND	ND	NA	NA	NA	60.0	1610
	ND	ND	ND	NA	NA	NA	1	l

ND - not detected

 $NA-not\ analyzed$ 

J – estimated (below the level of quantification)

EPA stored samples of products used for drilling in glass mason jars containing lids, transported products with a chain of custody form by vehicle to its Office of Research and Development (ORD) laboratory in Ada, OK, and archived products in a refrigerator at 4°C prior to extraction with water. Analysis for organic compounds were not conducted on water extracts of Quik Gel and Quik-Trol Gold due to the gel nature of extracts and concern of analytical equipment damage. The dissolved organic

carbon of dense soda ash was only 0.58 mg/L and based on MSDS, was not expected to be a source of organic compounds. EPA's analysis of extracts is noteworthy in that we could find no other published studies in which an organization collected and analyzed samples of products used for drilling mud during installation of monitoring wells.

With the exception of dense soda ash, the pH of extracts were well below that maximum pH levels (~12) observed in MW01 and MW02. Dense Soda Ash was not used at MW02. Alkalinity of soda ash is dominated by carbonate not hydroxide as observed in MW01. The pH of drilling mud in which dense soda ash was mixed in MW01 varied between 8 and 9 standard units. Thus, additives had no effect on pH measurements during sampling at monitoring wells.

To estimate expected concentrations of compounds in additives in water used for drilling mud, we normalized aqueous extraction concentrations by a normalization factor defined by

 $Normalization \ Factor = \frac{mass \ ratio \ in \ water \ used \ for \ drilling \ mud \ or \ well \ development}{mass \ ratio \ in \ aqueous \ extract}$ 

For instance, the mass ratio of the water extract of Aqua-Clear PFD was 1:20 while use in water used for well development was 1:467 resulting in a normalization factor of 1/20 divided by 1/467 or 23.4. Results are provided in Table SI E1.

At MW02, Boart-Longyear used 21 sacks or 1,050 pounds of Quik-Gel for drilling. The initial mass of bentonite used at MW01 was not provided in the logs. However, the mass of bentonite used at MW01 is expected to be similar to MW02 given that the target depth (almost 305 m or 1,000 feet) was the same at both wells. A log entry on 6/11/10 at 10:20 from MW02 indicates that 17,000 L (4,500 gallons) of water was used to mix mud for drilling at this well. The volume of water used to mix mud at MW01 was not specified in the drilling logs. However, both wells were drilled to the same depth under the same subsurface conditions so the volume of water used at MW01 would be expected to be similar to that used at MW02.

Concentrations of potassium in monitoring wells were well below concentrations and normalized concentrations in extracts. The extract and normalized concentration of chloride in Aqua-Clear PFD was lower and far lower than detected in MW02. During the Phase V sampling event, acrylamide was added to the target list of analytes and was not detected in any samples from MW01 and MW02 ( $< 10\,\mu g/L$ )³³ indicating that any compounds associated with Aqua-Clear PFD were removed during well development. With the exception of naphthalene detected at  $2.0\,\mu g/L$  in a Penetrol extract (normalized concentration of  $0.02\,\mu g/L$  in MW01), petroleum hydrocarbons were not detected in extracts. The maximum

concentrations and normalized concentration of isopropanol in extracts 85 was  $11.4 \,\mu\text{g/L}$ , respectively compared to 212 and 862  $\,\mu\text{g/L}$  at MW01 and MW02, respectively. BTEX compounds (benzene, toluene, ethylbenzene, and xylenes) were not detected in extracts but were detected at MW02.

EPA collected composite samples of cuttings and sent them with a chain of custody form to TestAmerica Laboratories in Denver, Colorado for Toxic Characteristic Leaching Procedure (TCLP). Samples were analyzed for TCLP volatile organic compounds using gas chromatography-mass spectrometry (GC-MS) in accordance with EPA SW-846 Methods 1311/8260B, for TCLP semivolatile organic compounds (GC-MS) in accordance with EPA SW-846 Methods 1311/8270C, for TCLP metals in accordance with EPA SW-846 Methods 1311/6010B, and for TCLP mercury in accordance with EPA SW-846 Methods 1311/7470A. Acetone, toluene, and m & p-xylene were detected in one sample at 6.9, 0.63, and 1.0 μg/L, respectively, concentrations far lower than that detected in MW02. Considering all these factors, it is unlikely that additives used for drilling mud impacted sample results in MW01 and MW02.

#### Well Development

Well development criteria stated in EPA's Monitoring Well Installation were as follows: water samples < 10 Nephelometric Turbidity Units (NTUs), or 3 purge volumes if < 10 NTU prior to attainment of 3 purge volumes, or 5 purge volumes if < 10 NTU is not achieved after three purge volumes. Daily logs indicate that 33,320 L (8815 gallons) or 24.5 purge volumes of water was removed from MW01 prior to the first round of sampling in October 2010 in which turbidity of sampled water was 7.5 NTUs. Hence, well development criteria were met at MW01. MW02 was a low yield well. Daily logs indicate that 5,760 L (1524 gallons) or 3.2 purge volumes of water was removed prior to the first sampling event in October 2010 in which the turbidity of sampled water was 24 NTUs. Elevated turbidity was caused by gas flow and pump cavitation due to gas flow. For instance, during the Phase V sampling event, during which removal of 5 purge volumes had been attained, turbidity was measured at 4.5 NTUs prior to pump cavitation and 15.7 NTUs after pump cavitation. Thus, well development criteria was ultimately achieved for both monitoring wells. Turbidity is not expected to have any impact on analysis of organic compounds nor on inorganic analyses since samples were filtered.

### Steel Well Casing

Boart-Longyear used thread and couple Hyundai HYSCO ASTM A53A-E steel pipe for well casing at both MW01 and MW02. A 6.1 m (20 ft) stainless-steel pre-packed screen was attached to casing via flush threads. EPA specified the use of metal casing to ensure sufficient tensile strength, especially at

joints during well placement. The tensile strength of steel and stainless-steel joints is over an order of magnitude greater than polyvinyl chloride (PVC) joints. The WYDEQ (Well Construction Standards, Chapter 11, Part G) explicitly allows for the use of ASTM A53 steel casing for well construction.

Materials used for well casing and screens can impart both negative and positive bias in detection and quantification of target analytes. Steel is an alloy consisting primarily of iron (Fe). The maximum allowable concentrations of manganese (Mn), copper (Cu), nickel (Ni), chromium (Cr), molybdenum (Mo), and vanadium (V) in ASTM A53A-E³⁸, steel pipe are 0.95, 0.40, 0.40, 0.15, and 0.08% by weight, respectively. Houghton and Berger³⁹ noted a slight enrichment of Fe and Mn in water from wells constructed of steel compared to wells constructed from PVC and acrylonitrile-butadiene-styrene (ABS).

Interaction can also occur with stainless steel. Hewitt⁴⁰ conducted static and dynamic (flushing) experiments on PVC, PTFE, stainless steel-SS-304 (SS-304), and stainless steel-316 (SS-316) casing materials in glass cylinders containing well water with low dissolved oxygen (DO) (< 0.5 mg/L) and observed corrosion of both SS-304 and SS-316 during testing (pH 7.6 - 7.8). Low concentrations of Cu, Cr, and Ni leached from both virgin SS-304 and SS-316. However, leaching of Cr and Ni increased significantly with corrosion. Hewitt⁴⁰ observed that concentrations of cadmium (Cd), Fe, and lead (Pb) decreased indicating sorption to casing. Hewitt⁴⁰ stated that reduction of Fe was consistent with precipitation of Fe(OH)₂ and that iron oxides provided active exchange sites for sorption of these elements.

In an EPA report, Aller et al.⁴¹ state that potentially corrosive conditions exist for steel in ground water having low pH (< 7) and elevated DO (> 2 mg/L), hydrogen sulfide (H₂S) (> 1 mg/L), TDS (> 1000 mg/L), CO₂ (> 50 mg/L), and Cl (> 500 mg/L) and that use of steel is not considered prudent in most natural geochemical environments. Subsequent to well development, purged water from MW01 and MW02 was largely devoid of dissolved oxygen during Phase III, IV, and V sampling events with a pH level in excess of 11 standard units.

In its Draft RCRA Ground-Water Monitoring Guidance, EPA⁴² states that use of carbon steel, low-carbon steel, and galvanized steel is not recommended for monitoring well construction in most natural geochemical environments and use of Type 304 and Type 316 stainless steel is unsuitable for use when monitoring for inorganic constituents. In an EPA Issue Paper, Pohlmann and Alduino⁴³ state that when corrosion is a concern, use of stainless-steel casing is not appropriate. In another EPA Issue Paper, Llopis⁴⁴ states that if samples are to be analyzed for metals, metal casing of any type should not be used. Thus, when installing monitoring wells to sample both metals and organic compounds, there are no consistent regulatory guidelines on use of materials for well casing.

During the week of April 30th, 2012 (after cessation of Phase V sampling), a drilling crew from USGS removed the 3 HP submersible pump in MW02, examined the casing and screen with an optical televiewer, and attempted to redevelop the well. The optical televiewer indicated that the screen and casing was intact. During re-development, sediment was removed from the base of the screen. Four subsamples of the material were sent to Gulf Coast Accutest Laboratories for analysis of metals with the following range of results: aluminum (1950-2720 mg/kg), antimony (2.5-3.4 mg/kg), arsenic (3.3-10 mg/kg), cadmium (<0.26-2.1 mg/kg), chromium (79.9-108 mg/kg), copper (168-719 mg/kg), lead (16.2-56.3 mg/kg), nickel (49.4-64.9 mg/kg), selenium (<0.26 mg/kg), and titanium (52.2-80.5 mg/kg). Results of metals analysis indicated that this sediment was either scrapings from steel pipe or a combination of scrapings from steel pipe and corrosion material removed from steel casing during development and redevelopment activities. During the Phase V sampling event, dissolved concentrations of Cd, Pb, Fe, Mn, Cu, Ni, Cr, Mo, and V at MW01 and MW02 were less than reporting limits at 1.0, 1.0, 67, 14.0, 2.0, 1.0, 2.0, 17, and 10 μg/L, respectively. Hence, the use of metal casing and presumed corrosion in areas of swabbing did not impart a positive bias on sample results for metals at MW01 and MW02.

However, corrosion can impact measured pH. Marsh and Lloyd⁴⁵ attributed elevation of pH in steel casing to corrosion and precipitation reactions mediated by carbonic acid and hydrogen sulfide. In both reactions, hydrogen ion is consumed and hydrogen gas is produced. During purging of capped artesian monitoring wells, Marsh and Lloyd⁴⁵ observed that pH decreased abruptly (e.g., pH 8.8 to pH 7.2) after a short period of time in wells where water flowed through the entire length of casing to the surface. However, there was little variation in pH in monitoring wells having sampling tubes placed within screened intervals. In contrast to observations by Marsh and Lloyd⁴⁵, pH reduction in MW01 during purging was gradual with the trend of pH reduction unrelated to removal of stored casing water. Thus, corrosion was not a causative factor of elevated pH at MW01 and MW02.

Black steel ASTM A53 pipe has a lacquered outside finish as opposed to a bare or galvanized finish. Manufactures coat the outside of steel pipe with a black paint to prevent rust and corrosion. However, sampled water does not come in contact with the exterior of well casing. Photographs (DiGiulio et al.²⁷) of casing indicate no apparent mill varnish or visual signs of oil and grease prior to or after casing decontamination procedures. Thus, it is unlikely that black varnish on the exterior of metal casing was responsible for detection of organic compounds in MW01 and MW02. Also, a non-hydrocarbon based pipe dope (Jet Lube WellGuard) was used on well casing joints. Thus, well casing is not responsible for detection of hydrocarbons in monitoring wells.

During conventional monitoring well construction, a bentonite slurry seal is typically placed on top of a primary or secondary filter or sand pack to limit the downward movement of a cement-based grout (ASTM⁴⁶, EPA⁴²). As documented in the draft⁴⁷ and final⁴⁸ workplans for well installation, this method of well completion was planned for both MW01 and MW02. However, as documented in field logs, during drilling, Shaw and Boart-Longyear advised EPA against the use of a conventional screen and sand pack for well completion at MW01 and MW02 due potential difficulty in sand pack placement (displacement of high density drilling mud with sand) and well development (removal of mud from sand pack). Shaw and Boart-Longyear recommended the use of pre-packed screens and cement baskets (filled with sand at the surface) in lieu of conventional screens and sand packs. EPA concurred with this approach for well completion.

An additional reason for not utilizing a bentonite slurry as a sealing agent is the presence of localized upward hydraulic gradients. Localized upgradient gradients are documented in the Wind River Formation²⁶, was present in a domestic well during the Phase II sampling event²⁷, and was observed at 4 production wells during Bradenhead testing conducted by Encana in 2012. A cement-bentonite grout may not set when a strong uplift is present^{49,50}. Under these conditions, pumped bentonite grout never sets up to anything more than thick paste⁵¹. In addition, a bentonite grout backfill would not have been volumetrically stable with overlying cement application since the specific gravity of cement grout was greater than that of the bentonite slurry. A cement-based grout has the widest regulatory acceptance and is the most commonly used to seal the annular space of deep wells⁴⁶ such as MW01 and MW02.

#### Cement Baskets

Cement baskets with blue metal "fins" and a rubber or synthetic liner were threaded to stainless-steel casing containing the stainless-steel pre-packed screens. The joint attaching stainless-steel casing to stainless-steel screen was reinforced with spot welding to increase the structural integrity of the joint. This was necessary to properly position the screen into the borehole prior to descent to target depth. McKay electrodes were used for welding. The MSDS for this product did not indicate the presence of organic compounds.

The composition of the cured (not applied in the field) blue paint on metal springs and rubber liner were not specified by EPA. Organic compounds in cured paint exist in cross-linked polymer matrix and generally considered resistant to leaching⁵². However, little is published on leaching of organic compounds from cured paint. Alben et al.⁵³ studied leaching of organic contaminants from epoxy-coated flat steel panels, with emphasis on the rate of leachate production and leachate composition. Methyl isobutyl ketone (MIBK), o-, m-, and p-xylene represented a major portion (51%) of leachate from the

epoxy coating. These findings were supported by field studies indicating the presence of MIBK and xylenes in water from the effluent from 2 of 3 storage tanks that were monitored one month after application of an epoxy coating⁵³. The extent of leaching of organic contaminants from epoxy resin linings was found to be strongly dependent on the duration of the curing process with longer curing periods producing more stable linings.

It is unlikely that blue paint on cement baskets was a causative factor for detection of 2-butoxyethanol and other organic compounds detected in MW01 and MW02 because of the following reasons. (1) MIBK and xylenes were not detected in MW01. (2) There was a low surface area for aqueous exposure (<0.05 m²), a low retention time in the screened interval during sampling especially at MW01 (20 minutes) during phase IV and phase V sampling events, and a large number of number of screen exchanges prior to sampling (especially at MW01 prior to the Phase V sampling event with > 200 exchanges).

# Cement Placement

High pH levels (~12) were observed during purging and sampling at MW01 and MW02 during Phase III, IV and V sampling events. Daily logs do not indicate that the tremie pipe for cement placement was placed directly through cement baskets or that cement was pumped directly into screened intervals at MW01 and MW02. At MW01, circulation was lost on 7/26/10 while drilling through a sandstone unit from 655 to 725 feet bgs and as shown on an electric log and borehole log descriptions. The caliper log indicates that a washout occurred at 715 feet bgs. Thus, some cement likely intruded into the formation above the screened interval at 765-785 ft bgs.

At MW01 and MW02, cement was pumped to target depths using a tremie pipe and placed in lifts to avoid buildup of pressure above the basket potentially causing basket collapse. At MW01, sand was added to the sand basket prior to setting the casing and screen in the borehole. The screen was subsequently hung and a cement plug was placed from 228.0-233.2 m (748-765 ft) bgs on 8/5/10 and left to set up overnight. The cement was tagged at 748 feet. Cement placement resumed the following day with 14 yd³ of Portland cement on top of the set plug.

At MW02, more cement, approximately 76-189 L (20-50 gallons) was utilized than expected when grouting above the cement basket. Based on a review of daily logs, the most likely explanation for this discrepancy is that the screened interval placement at MW02 was lower than reported by the driller or subcontractor. During the week of April 30th, 2012, a drilling crew from USGS removed the submersible pump in MW02, examined the casing and screen with an optical televiewer, and attempted to redevelop

MW02. A member of the crew stated that tagging tape indicated that the base of the screen of MW02 was at 989.5 ft not 980.0 ft bgs as expected. This measurement was checked a second time and the measurement tape was checked for accuracy. If the screen interval was in fact 9.5 ft lower than indicated on the driller's logs, then additional cement would have been necessary to reach the top of the cement basket overlying the screen. Threads on casing collars were visible at all joints located above the water table surface (e.g., pieces of pipe are not threaded flush at their ends). Neither cement nor mud was visible in the joints. An extra one to two inches at each couple would result in the well screen placed 4 - 8 feet deeper than expected or close to 9.5 ft as observed. Given a borehole diameter of 9.9 inches, 30 and 50 gallons of cement is equivalent to approximately 9.5 and 15.9 linear feet of cement which is close to 10.5 linear feet of distance between tagged cement at 958 ft and the top of the screened interval at 968.5 ft bgs.

### E.2 Purging at MW02

MW02 is a low flow monitoring well. During the Phase III, IV, and V sampling events, purging at MW02 was repeatedly interrupted by pump cavitation. Low flow may be due to low relative aqueous permeability due to gas flow or insufficient removal of drilling mud during well development. In May 2012, USGS unsuccessfully attempted to redevelop MW02 via swabbing⁵⁴.

During the Phase V sampling event, pre- and post-purge samples were collected at MW02 to assess potential reduction in dissolved gas and VOC concentrations due to gas flow in casing^{55,56}. MW02 was repeatedly purged over a 6-day period (Figure SI E3) to remove one borehole volume (2000 L) of water and subsequently sampled when sufficient water was present to support analysis per EPA guidelines^{42,57}.

USGS⁵⁸ has a "rule of thumb" recommendation to avoid sampling a well that has not recovered to within 90% of its static water level within a 24-hour period and has had less than one borehole volume of water removed during purging. Based on the slow recharge rate of MW02, USGS elected not to physically participate in sampling MW02⁵⁴. Instead, EPA collected samples at MW02 and provided them to USGS for analyses at a commercial laboratory⁵⁹ similar to MW01⁶⁰. Recovery occurs more rapidly in a low yield well having a low blank casing to screened interval ratio typical of shallow wells. MW02 consisted almost entirely of blank casing. Recovery to 90% of static water level required recovery of 202 m of water level rise in a 24-hour period.

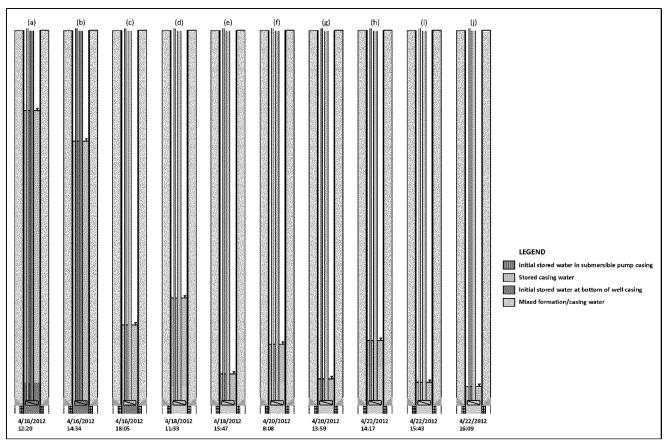


Figure SI E3. Illustration of purging and sampling sequence (date and times provided) at MW02 for Phase V sampling event. Vertical scale reflects relative lengths of screen, casing, and water levels: (a) Pre-purge condition. Dark gray color denotes water stored in submersible pump casing remaining from the Phase IV sampling event. Mustard colored water denotes water in casing from recovery following the Phase IV sampling event and targeted for removal during the first sample set. Light gray colored water denotes stored casing water from recovery during Phase III and IV sampling events. (b) Water is removed (170L or 45 gal) from the submersible pump casing, replaced with water from above the pump inlet, and sampled. (c) Water above pump inlet is removed (964 L or 255 gal). (d) Recovery occurs (132 L or 35 gallons). Light blue color indicates mixing of water initially present in the screened interval with incoming formation water. (e) Water above pump inlet removed (491 L or 130 gal) from casing. (f) Recovery occurs (167 L or 44 gallons) with further mixing of water in the screened interval. (g) Water above pump inlet removed (215 L or 57 gal). (h) Recovery occurs (189 L or 50 gal) with further mixing of water in the screened interval. (i) Water in submersible pump casing is removed (165 L or 45 gal) and replaced with mixed casing/formation water. (j) Mixed casing/formation water is sampled. Total volume of water removed during the Phase V sampling event prior to collection of the second sample was 2011 L or 532 gal equivalent to 1.04 borehole volumes.

### E.3 Purging and Wellbore Model Development at MW01

In the commonly used "well volume' approach to purging, three casing volumes are typically removed prior to sampling⁵⁸. It is assumed that water in blank casing is uniformly removed during purging prior to sampling. However, little or no mixing of water in blank well casing actually occurs above a pump inlet upon stabilization of drawdown^{61,62}. Placement of a submersible pump inlet directly above a screened interval, as was done at both MW01 and MW02 (Figures SI E1 and SI E2), minimizes

collection of purge water requiring disposal and takes advantage of flow mechanics to ensure minimal or no contact with blank well easing during sample collection.

EPA⁶³ used a wellbore plug flow model based on flow rate and drawdown to evaluate percent collection of casing and formation water as a function of purge volume and time at MW01. To evaluate removal of dissolved solids in well casing and better evaluate collection of formation water as a function of purge volume, we modified EPA's approach to include mixing in a screened interval. Mixing in a well screen causes a slower transition from casing water to formation water than would occur from plug flow alone.

Prior to commencement of purging, we assume that the concentration of a solute in a screened interval, pre-packed screen, and annular space between the pre-packed screen and borehole wall has an initial vertically integrated initial concentration ( $C_0$ ) and water in blank casing above the screened interval has an initial vertically integrated initial solute concentration ( $C_0$ ) (Figure SI E4a). Depending upon variation between  $C_0$  and  $C_0$ , differentiation of screen and casing concentrations results in complex hypothetical concentration profiles in the sampling train at the start of purging which dissipate rapidly upon removal of one casing or borehole volume (simulations not illustrated).

At the commencement of purging, water is removed from submersible pump casing. Combined downward and upward flow occurs in blank casing above and below the pump inlet respectively (Figure SI E4b) as drawdown occurs in the well. We assume that water in submersible pump and well casing undergoes unmixed plug flow. In the screened interval, radial flow occurs from the surrounding formation and mixes with water initially in the borehole and screen. The mass balance mixing model in the screened interval used is similar to that used by others⁶⁴. This mixed water then undergoes upward flow in the casing to the pump inlet (Figure SI E4b). As drawdown stabilizes, all of the water entering the pump inlet is from the formation (Figure SI E4c). Sampling then occurs after water level recovery (Figure SI E4d) to ensure that all water entering the inlet and flowing to the sampling train is directly from the formation in the event of a slight change in pumping rate due to pump operation. Without allowing for some level of recovery above the pump inlet, a slight and unintentional increase in pumping rate could cause a small but measureable increase in drawdown and again induce some degree of mixing between formation and casing water. This procedure was followed by EPA at MW01 during all sampling events.

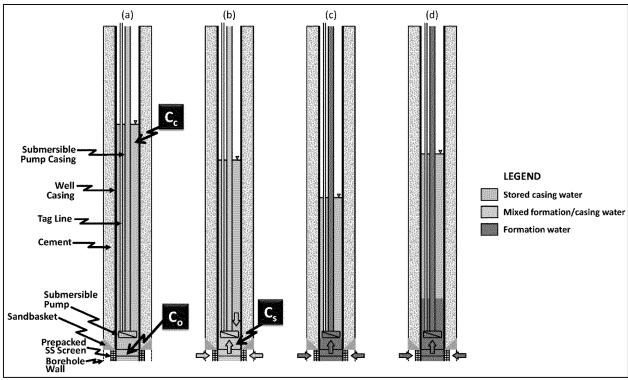


Figure SI E4. Plug flow - screen mixing model to support evaluation of purging: (a) Prior to purging, the concentration of a solute in the screened interval (and surrounding borehole) and overlying casing is equal to an initial value  $C_0$  and a constant concentration  $C_C$  respectively. (b) During drawdown at commencement of purging, both downward and upward plug flow is assumed in casing above and below a pump inlet, respectively. Radial flow occurs from the surrounding formation with subsequent mixing of formation water and water initially in the borehole and screen. (c) As drawdown stabilizes, all of the water entering the pump inlet is directly from the formation. (d) Water level recovery is allowed to occur to ensure that all water entering the inlet is directly from the formation in the event of slight water level perturbation during pumping.

Model development is summarized as follows. Casing volume (Vc) [L³] is defined as:

$$V_{C} = \frac{\pi}{4B} \left[ L_{WC} D_{ID-WC}^{2} - L_{PC} \left( D_{OD-PC}^{2} - D_{ID-PC}^{2} \right) - L_{TL} \left( D_{OD-TL}^{2} - D_{ID-TL}^{2} \right) - L_{SP} D_{OD-SP}^{2} + L_{PC*} D_{ID-PC}^{2} \right]$$

 $L_{wc}$  = length of water column in well (depth to base o f screen - depth to static water level) [L]

 $L_{PC}$  = length of submerged pump casing (depth to top o f pump - static water level) [L]

 $L_{PC^*}$  = length of submersible pump casing to the surface (static water level) [L]

 $L_{\text{TL}}$  = length of submerged tag line (depth of tag line - static water level) [L]

 $L_{SP}$  = length of submersible pump [L]

 $D_{\text{ID-WC}}$  = inside diameter of well and screen casing (cm) [L]

 $D_{\text{OD-PC}}$  = outside diameter of submersible pump casing [L]

 $D_{\text{ID-PC}}$  = inside diameter of submersible pump casing [L]

 $D_{OD-TL}$  = outside diameter of tag line [L]

 $D_{\text{ID-TL}}$  = inside diameter of tag line [L]

 $D_{SP}$  = diameter of submersible pump [L]

B = Dimensional constant (units of length and volu me are in cm and liters respectively, B = 1000).

The term  $L_{WC}D_{ID-WC}^2$  accounts for water storage in casing, including the screened interval, without modification for internal components. The term  $L_{PC}\left(D_{OD-PC}^2 - D_{ID-PC}^2\right)$  accounts for the volume of submerged submersible pump casing material. The term  $L_{SP}D_{OD-SP}^2$  accounts for the volume of the submersible pump. The term  $L_{PC} * D_{ID-PC}^2$  accounts for water storage in the submersible pump casing above the static water level. Valves within submersible pump casing allowed water in casing to extend to land surface. Borehole volume VB  $[L^3]$  is defined as:

$$V_{B} = V_{C} + \frac{\pi}{4R} \left[ \Phi L_{SS} \left( D_{OD-PP}^{2} - D_{OD-WC}^{2} \right) + L_{SS} \left( D_{BH}^{2} - D_{OD-PP}^{2} \right) \right]$$

 $L_{SS}$  = length of stainless-steel pre-packed screen [L]

 $D_{OD\text{-WC}}$  = outside diameter of steel well casing [L]

D_{OD-PP} = outside diameter of pre-packed screen [L]

 $D_{BH}$  = diameter of borehole [L]

 $\Box$  = effective porosity of pre-packed screen (assume d 0.4).

The term  $\phi L_{SS} \left( D_{OD-PP}^2 - D_{OD-WC}^2 \right)$  accounts for water storage in the pre-packed screen. The term  $L_{SS} \left( D_{BH}^2 - D_{OD-PP}^2 \right)$  accounts for water storage in the annular space between the pre-packed screen and borehole wall. During drawdown, the relative concentration of a solute entering a sampling train at the surface can be expressed by:

 $C_P$  = concentration exiting the submersible pump casi  $m_{\rm e}$  at the surface at time increment i [ML⁻³]

 $C_F$  = constant concentration in formation [ML  $^{-3}$ ]

 $C_{\rm C}$  = constant storage water casing concentration [ML

Š .

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 $C_{BP}$  = concentration entering pump inlet at time incre  $Q_{BP}$  = flow of water to the pump from beneath the inle  $Q_{AP}$  = flow of water to the pump from above the inlet  $Q_{T} = Q_{AP} + Q_{BP}$  at time increment i [L³T⁻¹].

At the start of purging, all water originates from storage in submersible pump casing. Thus, when

$$V_i < V_{PC}, \quad \left(\frac{C_p}{C_F}\right)_i = \left(\frac{C_C}{C_F}\right)_i$$

 $V_i$  = cumulative volume of water extracted water volu me at time i [L³]  $V_{PC}$  = volume of water in submersible easing [L ³].

At the start of purging, the initial concentration of solute below the pump inlet and above the screened interval is equivalent to  $C_C$  but transitions to water from the screened interval over time. Thus, when

$$V_{i(BP)} < V_{SP}, \quad \left(\frac{C_{BP}}{C_F}\right)_i = \left(\frac{C_C}{C_F}\right)_i$$

and

$$V_{i(BP)} > V_{SP}, \quad \left(\frac{C_{BP}}{C_F}\right)_i = \left(\frac{C_S}{C_F}\right)_i$$

$$V_{i(BP)} = \Delta V_{i(BP)} + \Delta V_{i-1(BP)}$$

 $V_{SP}$  = volume of water initially stored between the pu mp inlet and screened interval  $V_{i(BP)}$  = cumulative volume of water removed from below t he pump inlet at time increment i  $C_S$  = concentration exiting the screened interval at time increment i [ML-3].

The cumulative volume of water extracted below the pump at time increment i is calculated by adding the cumulative volume of water extracted below the pump at time increment i-1 to the change in extracted volume below the pump which is calculated by

$$\Delta V_{i(BP)} = \Delta V_i \left( \frac{Q_{BP}}{Q_T} \right)_i$$

and

$$\Delta V_i = V_i - V_{i-1}$$

The fraction of water originating below the pump to total water extracted is calculated by:

$$\left(\frac{Q_{BP}}{Q_T}\right)_i = 1 - \left(\frac{Q_{AP}}{Q_T}\right)_i$$

and

$$\left(\frac{Q_{AP}}{Q_T}\right)_i = \frac{\Delta D_i}{\Delta D_i^*}$$

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$$\Delta D_i = D_i - D_{i-1}$$

$$\Delta D_i^* = \frac{\Delta V_i}{A_C}$$

$$A_{C} = \frac{\pi L_{CD}}{4B} \left( D_{ID-WC}^{2} - D_{OD-PC}^{2} - D_{OD-TL}^{2} \right)$$

 $D_i$  = total drawdown at time i [L]

 $\Box D_{i^*} = \text{the change in drawdown at time } i \text{ if all water du} \qquad \text{ring drawdown comes from above the pump.} \\ A_C = \text{volume per length of casing associated with dra} \qquad \text{wdown } [L^2] \ (7.12 \ \text{liters/m drawdown at MW01}) \\ L_{CD} = \text{characteristic drawdown length } [L] \ (1 \ \text{m at MW01}) \ ).$ 

During recovery,

$$\Delta D_i < 0$$
 and  $Q_{AP} = 0$   $Q_T = 0$ 

The concentration of solute in water exiting the screened interval then is calculated using a mass balance mixing equation:

$$V_S \frac{dC_S}{dt} = C_F Q_{BP} - C_S Q_{BP}$$

Since Q_{BP} is a function of time (calculated in increments using drawdown and flow data), C_S/C_F varies in increments of time

where

$$\Delta \alpha_i = \alpha_i - \alpha_{i-1}$$

$$\alpha_i = \frac{V_{BP(i)}}{V_S}$$

 $\Box$  = cumulative screen volume exchanges at time incr ement i.

V_s = screen volume (casing + porosity of pre-packed screen + annular space between pre-packed screen and borehole wall).

At time 0,  $C_8$  equals initial concentration ( $C_0$ ).  $V_8$  is a constant calculated by:

$$V_S = V_B - V_C + \frac{\pi}{4B} L_{SS} D_{ID-WC}^2$$

Input parameters to support modeling are summarized in Table SI E2.

**Table SI E2.** Well design and input parameters for calculation of casing, borehole, and screen exchange volumes during Phase V sampling event

Label	MW01		MW02	
	m	liters	m	liters
Depth below ground surface to static head	62.2		60.5	
Depth below ground surface to base of screen	239.3		298.7	
Length of submersible pump (L _{SP} )	0.635		0.635	
Depth of base of submersible pump	232.7		297.2	
Depth of top of submersible pump casing	232.1		296.6	
Depth of schedule 80 PVC tag line	232.1		296.6	
Length of water column in well (Lwc)	177.1		238.2	
Length of water in submerged pump casing (L _{PC} )	232.1		296.6	
Length of submerged tag line (L _{TL} )	169.9		236.0	
Length of stainless-steel pre-packed screen (Lss)	6.10		6.10	
Inside diameter of schedule 40 steel well casing (IDwc)	0.102		0.102	
Outside diameter of schedule-40 steel well casing (ODwc) 0	114		0.114	
Outside diameter of submersible pump casing ( <b>OD</b> _{PC} )	0.034		0.034	
Inside diameter of submersible pump casing (ID _{PC} )	0.027		0.027	
Outside diameter of schedule 80 PVC tag line ( <b>OD</b> _{TL} )	0.033		0.033	
Inside diameter of schedule 80 PVC tag line (ID _{TL} )	0.024		0.024	
Outside diameter of submersible pump (OD _{SP} )	0.089		0.089	
Diameter of borehole (D _{BH} )	0.251		0.251	
Outside diameter of pre-packed screen (ODPP)	0.216		0.216	
Effective porosity of pre-packed screen $(\varphi) = 0.45$				
Length from Bottom of Pump to top of Screen (Lps)	0.457		0.0	
Well casing volume (V _C )		1358		1792
Borehole volume (V _B )		1504		1942
Screen plus borehole volume (Vs)		200.6		196.8
Volume above screen and below pump (V _{SP} )		3.76		0.0
Liters per meter of drawdown (Ac)		6.45		6.45
Volume of water in submersible pump casing (V _{PC} )		129		165

Table SI E3a. Summary of Organic Compound Detections in MW01

Target Organic Compounds	EPA	EPA	USGS	EPA	EPA	EPA	EPA	EPA	EPA	EPA	EPA	EPA	USGS	EPA
	Phase III	Phase IV	Phase V	Phase V	Phase V	Phase V	Phase V	Phase V	Phase V	Phase V	Phase V	Phase V	Phase V	Phase V
	1			0412-4	0412	0412-2	0412-3	0412-5	0412-7	0412-6	0412-8	0412-9		0412-10
Borehole Volumes	0.3	0.7	1.6 - 3.0	1.6	1.8	2.1	2.3	2.4	2.6	2.7	2.9	3.0	3.0	3.3
dissolved organic carbon (mg/L)	8.510	9.430	NA	NA	5.63°/5.75°	NA	NA	NA	NA	NA	NA	NA	NA	3.360
diesel range organics (µg/L)	634 ^{R8}	924 ^{R8}	180(J) ^T /190(J) ^T	555 ^{R8}	484 ^{R8} /476 ^{R8}	NA NA	NA	NA	379 ^{R8}	NA NA	NA	NA NA	85(J) ^T /83(J) ^T	267 ^{R8}
gasoline range organics (µg/L)	389 ^{R8}	592 ^{R8}	700(J+) ^T /760(J+) ^T	584 ^{R8}	528 ^{R8} /539 ^{R8}	531 ^{R8}	493 ^{R8}	461 ^{R8}	418 ^{R8}	444 ^{R8}	402 ^{R8}	410 ^{R8}	730(J+) ^T /710(J+) ^T	328 ^{R8}
benzene (μg/L)	<2.5 ^{R8}	<0.50 ^S	<0.16 ^T /<0.16 ^T	<0.50 ^S	<0.50 ^{\$}	<0.50 ^S	<0.50 ^{\$}	<0.50 ^S	<0.50 ^{\$}	<0.50°s	<0.50 ^S	<0.50 ^S	<0.16 ^T /<0.16 ^T	<0.50 ^S
benzene (μg/L)	12.3	<0.25(J-) ^{R8}	VO.10 / VO.10	VO.50	<0.25 ^{R8} /<0.25 ^{R8}	V0.50	NO.50	VO.50	VO.50	V0.50	₹0.50	₹0.50	V0.10 / V0.10	<0.25 ^{R8}
toluene (μg/L)	0.75 ^{R8}	0.59(B) [§]	<0.17 ^T /<0.17 ^T	<0.50 ⁸	<0.50°/<0.50°	<0.50 ^s	<0.50 ⁸	<0.50 ^s	<0.50 ⁸	<0.50°s	<0.50 ^s	<0.50 ^s	<0.17 ^T /<0.17 ^T	<0.50 ^S
4-6-)		<0.56(J-) ^{R8}			<0.25 ^{R8} /<0.25 ^{R8}									<0.25 ^{R8}
m+p-xylene (μg/L)	<2.5 ^{R8}	0.49(J) ^S	<0.34 ^T /<0.34 ^T	<0.50 ^S	<0.50 ^s /<0.50 ^s	<0.50 ^s	<0.50 ^s	<0.50 ^s	<0.50 ^s	<0.50 ^s	<0.50°s	<0.50°s	<0.34 ^T /<0.34 ^T	<0.50 ^s
. ,,		0.89(B,J-)R8			<1.00 ^{R8} /<1.00 ^{R8}									<1.00 ^{R8}
o-xylene (μg/L)	<2.5 ^{R8}	0.38(J) [§]	<0.19 ^T /<0.19 ^T	<0.50 ^S	<0.50 ⁸ /0.06(J) ⁸	<0.50 ^S	<0.50 ^s	<0.50 ^S	<0.50 ^S	<0.50 ^{\$}	<0.50 ⁸	<0.50 ⁸	<0.19 ^T /<0.19 ^T	<0.50°s
		<0.25(J-)R8			<0.25 ^{R8} /<0.25 ^{R8}									<0.25 ^{R8}
ethylbenzene (μg/L)	<2.5 ^{R8}	0.21(J) ^S	<0.16 ^T /<0.16 ^T	<0.50 ^S	<0.50 ^S /<0.50 ^S	<0.50 ^S	<0.50 ^S	<0.50 ^S	<0.50 ^S	<0.50 ^s	<0.50 ^s	<0.50 ^s	<0.16 ^T /<0.16 ^T	<0.50 ^s
		<0.25(J-) ^{R8}			<0.25 ^{R8} /<0.25 ^{R8}									<0.25 ^{R8}
isopropylbenzene (μg/L)	<2.5 ^{R8}	<0.25(J-) ^{R8}	<0.19 ^T /<0.19 ^T	NA	<0.25 ^{R8} /<0.25 ^{R8}	NA	NA	NA	NA	NA	NA	NA	<0.19 ^T /<0.19 ^T	<0.25 ^{R8}
n-butylbenzene (μg/L)	<2.5 ^{R8}	<0.25(J-) ^{R8}	<0.32 ^T /<0.32 ^T	NA	<0.25 ^{R8} /<0.25 ^{R8}	NA	NA	NA	NA	NA	NA	NA	<0.32 T/<0.32 T	<0.25 ^{R8}
sec-butylbenzene (µg/L)	<2.5 ^{R8}	<0.25(J-) ^{R8}	<0.17 ^T /<0.17 ^T	NA	<0.25 ^{R8} /<0.25 ^{R8}	NA	NA	NA	NA	NA	NA	NA	<0.17 ^T /<0.17 ^T	<0.25 ^{R8}
tert-butylbenzene (μg/L)	<2.5 ^{R8}	<0.25(J-) ^{R8}	<0.16 ^T /<0.16 ^T	NA	<0.25 ^{R8} /<0.25 ^{R8}	NA	NA	NA	NA	NA	NA	NA	<0.16 ^T /<0.16 ^T	<0.25 ^{R8}
n-propylbenzene (μg/L)	<2.5 ^{R8}	<0.25(J-) ^{R8}	<0.16 ^T /<0.16 ^T	NA	<0.25 ^{R8} /<0.25 ^{R8}	NA	NA	NA	NA	NA	NA	NA	<0.16 ^T /<0.16 ^T	<0.25 ^{R8}
p-isopropyltoluene (μg/L)	<2.5 ^{R8}	<0.25(J-) ^{R8}	<0.20 ^T /<0.20 ^T	NA	<0.25 ^{R8} /<0.25 ^{R8}	NA	NA	NA	NA	NA	NA	NA	<0.20 ^T /<0.20 ^T	<0.25 ^{R8}
styrene (μg/L)	<2.5 ^{R8}	<0.25(J-) ^{R8}	<0.17 ^T /<0.17 ^T	NA	<0.25 ^{R8} /<0.25 ^{R8}	NA	NA	NA	NA	NA	NA	NA	<0.17 T/<0.17T	<0.25 ^{R8}
1,3,5-trimethylbenzene (µg/L)	<2.5 ^{R8}	0.38(J) ^S	NA	<1.00 ^S	<1.00°/0.15(J)°	<1.00 ^S	<1.00 ^S	<1.00 ^S	<1.00 ^S	<1.00 ^S	<1.00 ^S	<1.00 ^S	NA	<1.008
		<0.25(J-) ^{R8}			<0.25 ^{R8} /<0.25 ^{R8}									<0.25 ^{R8}
1,2,4-trimethylbenzene (μg/L)	<2.5 ^{R8}	0.49(J) ^{\$}	<0.15 ^T /<0.15 ^T	<1.00 ^S	<1.00 ^S /0.27(J) ^S	<1.00 ^S	<1.00 ^S	<1.00 ^S	<1.00 ^S	<1.00\$	<1.00 ^S	<1.00 ^S	<0.15 ^T /<0.15 ^T	<1.00 ^S
	1	<0.25(J-) ^{R8}			<0.25 ^{R8} /<0.25 ^{R8}									<0.25 ^{R8}
1,2,3-trimethylbenzene (µg/L)	NA Po	0.33(J) ^S	<0.27 ^T /<0.27 ^T	<1.00 ^S	<1.00 ⁸ /0.26(J) ⁸	<1.00 ^S	<1.00 ^S	<1.00 ^S	<1.00 ^S	<1.008	<1.008	<1.008	<0.27 ^T /<0.27 ^T	<1.00 ^S
naphthalene (µg/L)	<2.5 ^{R8}	<1.08	<0.22 ^T /<0.22 ^T	<1.00 ^S	<1.00 ⁸ /3.78 ⁸	<1.00 ^S	<1.00 ⁸	<1.00 ^S	<1.00 ^S	<1.00°	<1.00 ⁸	<1.00 ⁸	<0.22 ^T /<0.22 ^T	<1.008
	0 4 0 D 0	<0.25(J-) ^{R8}	a and som Top as on T	<1.00 ^{R8}	<0.25 ^{R8} /<0.25 ^{R8}				<1.00 ^{R8}				0.00 = T	<0.25 ^{R8}
1-methylnapthalene (μg/L)	<0.10 ^{R8}	<0.50 ^{R8}	0.0096(J) ^T /0.01(J) ^T	<1.00 ^{R8}	<1.00 ^{R8} /<1.00 ^{R8}	NA	NA	NA	<1.00 ^{R8}	NA	NA	NA	<0.0057 ^T /<0.0058 ^T	<1.00 ^{R8}
2-methylnapthalene (μg/L)	<0.10 ^{R8}	<0.50 ^{R8}	0.0110(J) ^T /0.011(J) ^T	<1.00 ^{R8}	<1.00 ^{R8} /<1.00 ^{R8}	NA	NA	NA	<1.00 ^{R8}	NA	NA	NA	0.0072(J) ^T /0.006(J) ^T	<1.00 ^{R8}
phenol (µg/L)	10.7 ^{R8}	19.0 ^{R8}	10(J) ^T /11 ^T	9.65 ^{R8}	8.09(J+) ^{R8} /8.42 ^{R8}	NA	NA	NA	6.68 ^{R8}	NA	NA	NA	6.1(J) ^T /6.6(J) ^T	5.42 ^{R8}
2-methylphenol (µg/L)	<0.10 ^{R8}	<0.50 ^{R8}	<1 ^T /<1.1 ^T	<2.00 ^{R8}	<2.00 ^{R8} /<2.00 ^{R8}	NA	NA	NA	<2.00 ^{R8}	NA	NA	NA	<0.99 T/<1.0T	<2.00 ^{R8}
3&4-methylphenol (µg/L)	0.34 ^{R8}	1.85 ^{R8}	$0.95(J)^{T}/1.1(J)^{T}$	<5.00 ^{R8}	<5.00 ^{R8} /<5.00 ^{R8}	NA	NA	NA	<5.00 ^{R8}	NA	NA	NA NA	0.47(J) ^T /0.46(J) ^T	<5.00 ^{R8}
2,4-dimethylphenol (µg/L)	<0.10 ^{R8}	<0.50 ^{R8}	<0.61(J-) ^T /<0.62(J-) ^T	<2.00 ^{R8}	<2.00 ^{R8} /<2.00 ^{R8}	NA Starte	NA Transfer	NA 82.2 (P.S	<2.00 ^{R8}	NA SECUE	NA NA	NA SO S ( P S	<0.59(J-) ^T /<0.59(J-) ^T	<2.00 ^{R8}
isopropanol (µg/L)	NA	212 ⁸	<13(J-) ^T /<13(J-) ^T	65.0(J) ^S	69.8(J) ⁸ /69.2(J) ⁸	74.8(J) ^S	76.8(J) ^S	82.2(J) ^S	62.6(J) ⁸	77.4(J) ^S	80.0(J) ^S	68.5(J) ^S	<13(J-) ^T /<13(J-) ^T	69.3(J) ⁸
n-propanol (µg/L)	NA NA	<100s	NA	<100°s	1.7(J†) ^S /<100 ^S	<100s	<100 ^s	<100 ^S	<100 ^s	<100 ^S NA	<100 ^S	<100 ^S	NA	<100
methanol (μg/L)	NA	NA	NA	NA	<5000 ^A /<5000 ^A 863(J†) ^S /831(J†) ^S	NA	NA	NA	NA	NA.	NA	NA	NA	<5000A
athemat (upff )	NA	NA	NA	NA	13.7 (J†) ⁸ /<100 ⁸	<100s	<100°s	<100s	<100°s	<100°s	<100°s	<100°s	NA	<100°s
ethanol (µg/L)	NA NA	<5.0 ^{\$}	NA <11 ^T /<11 ^T	<5.0 ^{\$}	<5.0°	<5.0°	<5.0°	<5.0°	<5.0°	<5.0°	<5.0°	<5.0°	<11 ^T /<11 ^T	<5.0°
tert butyl alcohol (µg/L) acetone (µg/L)	NA NA	79.5(J-) ^{R8}	<1.9 ^T /<1.9 ^T	<5.0°	<5.0°	<5.0°	<5.0°	<5.0°	<5.0°	<5.0°	<5.0°	<5.0°	<1.9 ^T /<1.9 ^T	<5.0°
acetone (µg/L)	INA	79.3(3-)	1.9 /~1.9	₹3.0	<5.0(C) ^{R8} /<5.0(C) ^{R8}	3.0	₹3.0	₹3.0	√3.0	3.0	3.0	3.0	1.9.7<1.9	<5(C)R8
2-butanone (μg/L)	NA	<0.50(J-) ^{R8}	<2 ^T /<2 ^T	NA	<0.25 ^{R8} /<0.25 ^{R8}	NA	NA	NA	NA	NA	NA	NA	<2 ^T /<2 ^T	<0.25 ^{R8}
4-methyl-2-pentanone (μg/L)	NA	2.6(J-) ^{R8}	<0.98 ^T /<0.98 ^T	NA NA	1.39(J)/1.37(J)	NA NA	NA	NA NA	NA NA	NA NA	NA NA	NA NA	<0.98 ^T /<0.98 ^T	0.59 (J)
benzoic acid (µg/L)	212 ^{R8}	457(J) ^{R8}	$340(J+)^{T}/360(J+)^{T}$	735(J.D) ^{R8}	221(D) ^{R8} /309(D) ^{R8}	NA	NA	NA	310(D) ^{R8}	NA	NA	NA	190(J+) ^T /200(J+) ^T	237(D) ^{R8}
ethylene glycol (µg/L)	NA	NA	<8630 ^T /<8630 ^T	NA	<5000 ^A /<5000 ^A	NA	NA	NA	NA	NA	NA	NA	<8630 ^T /<8630 ^T	<5000 ^A
propylene glycol (µg/L)	NA NA	NA	<18700 ^T /<18700 ^T	NA NA	<5000 ^A /<5000 ^A	NA NA	NA NA	NA NA	NA NA	NA NA	NA NA	NA NA	<18700 ^T /<18700 ^T	<5000 ^A
diethylene glycol (µg/L)	NA	226(J+)R3	<7730 ^T /<7730 ^T	60.0(DR3	53.9(D ^{R3} /53.9(D ^{R3}	NA	NA	NA	34.1(DR3	NA	NA	NA	<7730 ^T /<7730 ^T	26.4(J)R3
triethylene glycol (µg/L)	NA	46(J-) ^{R3}	<8450 ^T /<8450 ^T	12.7(J-) ^{R3}	11.5(J-) ^{R3} /11.6(J-) ^{R3}	NA	NA	NA	4.9(J-) ^{R3}	NA	NA	NA	<8450 ^T /<8450 ^T	2.9 (J-) ^{R3}
tetraethylene glycol (µg/L)	NA	7.3 (J-,B) ^{R3}	NA	<10.0(J-) ^{R3}	<10.0(J-) ^{R3} /<10.0(J-) ^{R3}	NA	NA	NA	<10.0 (J) ^{R3}	NA	NA	NA	NA	<10.0 (J-) ^{R3}
2-butoxyethanol (µg/L)	<0.25 ^{R8}	<10(J-)R3	NA	5.1(J-) ^{R3}	3.5(J-) ^{R3} /3.0(J-) ^{R3}	NA NA	NA	NA	1.5 (J-) ^{R3}	NA	NA	NA	NA	<5.0(J-)R3
2 outon) chianoi (pg/2)	-0.25	12.7 ^{R8}	1,71	<1.00 ^{R8}	<1.00 ^{R8} /5.78 ^{R8}	1421	141	1424	3.49 ^{R8}	1 111				<1.00 ^{R8}
ethyl ether (µg/L)	<0.25 ^{R8}	<0.25(J-) ^{R8}	<0.26 ^T /<0.26 ^T	NA	<0.25 ^{R8} /<0.25 ^{R8}	NA	NA	NA	NA	NA	NA	NA	<0.26 ^T /<0.26 ^T	<0.25 ^{R8}
nonylphenol (µg/l)	NA	NA	NA	0.65(J-,B) ^L	0.60(J-,B) ^L /0.57(J-,B) ^L	NA	NA	NA	0.65(J,B) ^L	NA	NA	NA	NA	0.24(J-,B) ^L
octylphenol (µg/L)	NA	NA	NA	0.16(J) ^L	$0.14(J)^{L}/0.13(J)^{L}$	NA	NA	NA	0.10 (J) ^L	NA	NA	NA	NA	0.051(J) ^L
acrylamide (µg/L)	NA	NA	NA	<0.20 ^L	<0.20 ^L /<0.20 ^L	NA	NA	NA	<0.20 ^L	NA	NA	NA	NA	<0.20 ^L
lactate (µg/L)	NA	69(J) ⁸	NA	NA	<100(R) ^{\$} /<100(R) ^{\$}	NA	NA	NA	NA	NA	NA	NA	NA	<100(R) ^S
formate (µg/L)	NA	112 ⁸	NA	NA	<100(R) ^{\$} /<100(R) ^{\$}	NA	NA	NA	NA	NA	NA	NA	NA	<100(R) ^S
acetate (µg/L)	NA	8050 ^s	NA NA	NA	3420(D) ^S /5960(D) ^S	NA NA	NA	NA	NA	NA	NA	NA	NA	6080 ^S
propionate (µg/L)	NA	309 ⁸	NA	NA	75(J) ⁸ /95(J) ⁸	NA	NA	NA	NA	NA NA	NA	NA	NA	0.084(J) ^S
adamantine (µg/L)	<2.5 ^{R8}	<0.25(J-) ^{R8}	NA	<1.00 ^{R8}	<0.25 ^{R8} /<0.25 ^{R8}	NA	NA	NA	<1.00 ^{R8}	NA NA	NA NA	NA NA	NA	<0.25 ^{R8}
		0.20(0)		11.00	1 2.20 / 10.20	- 14.4			-1.00	1 - ** *	1 - 14 4	1 - ** *	1	.0.20
1,3-dimethyl adamantine (µg/L)	<2.5 ^{R8}	<0.25(J-) ^{R8}	NA	<1.00 ^{R8}	<0.25 ^{R8} /<0.25 ^{R8}	NA	NA	NA	<1.00 ^{R8}	NA	NA	NA	NA	<0.25 ^{R8}

Table SI E3b. Summary of Field Parameters, Major Ions, and Dissolved Metals at MW01

Inorganics	EPA	EPA	USGS	EPA	EPA	EPA	EPA	EPA	EPA	EPA	EPA	EPA	USGS	EPA
	Phase III	Phase IV	Phase V	Phase V 0412-4	Phase V 0412	Phase V 0412-2	Phase V 0412-3	Phase V 0412-5	Phase V 0412-7	Phase V 0412-6	Phase V 0412-8	Phase V 0412-9	Phase V	Phase V 0412-10
Borehole Volumes	0.3	0.7	1.6-3.0	1.6	1.8	2.1	2.3	2.4	2.6	2.7	2.9	3.0	3.0	3.3
Field Parameters	0.0		1.0.0.0	1 1.0	1.0	1	1 40			# * * · · · · · · · · · · · · · · · · ·	#1.7			1 22
pH	11.91	11.79	11.4	11.43	11.34/11.34	11.20	11.16	11.08	11.01	10.94	10.89	10.80	10.7	10.71
specific conductance (µS/cm)	3265	2352	1621	1539	1489/1489	1413	1393	1371	1354	1336	1335	1318	1373	1307
dissolved oxygen (mg/l)	0.17	0.03	<0.20	0.01	0.00/0.00	0.00	0.00	0.01	0.01	0.00	0.01	0.00	< 0.20	0.01
oxidation reduction potential (mV)	114	-116	-343.7	-395	-388/-388	-393	-394	-391	-397	-395	-385	-383	-389.8	-379
turbidity (NTU)	7.5	7.9	NM	NA	2.0	NA	NA	NA	NA	NA	NA	NA	NM	2.6
alkalinity (mg/l CaCO3)	430	388	215	NA	213/213	NA	NA	NA	NA	NA	NA	NA	174/182	181
Major Ions														
nitrate + nitrite (mg N/l)	0.150(B)O	<0.100°	<0.019 ^T /<0.019 ^T	NA	0.120°/<0.050°	NA	NA	NA	NA	NA	NA	NA	<0.02 T	<0.050°
ammonia (mg N/l)	4.61°	4.25°	$0.79(B)^{T}/0.79(B)^{T}$	NA	1.81 ^o /1.60 ^o	NA	NA	NA	NA	NA	NA	NA	0.34(B) ^T	0.490°
SO4 (mg/L)	398°	339°	380 ^T /380 ^T	391°	390°/388°	397º	394°	406°	407°	401°	411°	413°	410 ^T	428°
S (mg/L)	158(J)	141(J)	NA	187(J) ^S	177(J) ^S /171(J) ^S	202(J) ^S	198(J) ⁸	210(J) ^S	210(J) ⁸	208(J) ^S	210(J) ⁸	214(J) ⁸	NA	200(J) ^S
Cl (mg/l)	23.3°	23.1°	26 ^T /26 ^T	21.0°	19.4°/20.9°	22.0°	21.0°	21.2°	21.0°	21.5°	21.6°	20.8°	27 ^T	21.2°
Br (mg/l)	NA	<3.00°	$0.2(J)^{T}/0.2(J)^{T}$	<1.00°	<1.00°/<1.00°	<1.00°	<1.00°	<1.00°	<1.00°	<1.00°	<1.00°	<1.00°	0.2(J) ^T	<1.00°
F (mg/l)	1.55°	1.88°	3 ^T /3 ^T	2.24°	2.290/2.330	2.370	2.11°	2.29°	2.01°	2.330	2.13°	2.06°	3T	2.01°
K (mg/l)	54.98	24.7 ^s	15.0 ^T /16.0 ^T	17.8 [§]	17.3 ⁸ /17.2 ⁸	16.2 ⁸	16.0 ^s	15.7 ^s	15.3 ^s	15.0 ^S	14.5 ⁸	14.4 ^S	13.0 ^T	13.6 ^s
Na (mg/l)	334 ⁸	304 ^s	270 ^T /280 ^T	273 ^{\$}	276 ⁸ /277 ⁸	271 ⁸	264 ⁸	265 ⁸	265 ⁸	264 ⁸	264 ⁸	268 ⁸	280 ^T	264 ⁸
Ca (mg/l)	15.68	13.6§	9.4 ^T /9.4 ^T	9.80 ^{\$}	9.87/9.91 ^s	9.75 ⁸	9.67 ^{\$}	9.69 ⁸	9.67 [§]	9.66 [§]	9.61 ^s	9.65 ⁸	8.90 ^T	9.47 ⁸
Mg (mg/l)	0.05(B) ^S	0.12 ⁸	$0.14(J)^{T}/0.15(J)^{T}$	0.13 [§]	0.14 ⁸ /0.15 ⁸	0.14 [§]	0.15 ^S	0.15 ⁸	0.16 ⁸	0.16 [§]	0.16 [§]	0.17 ^S	0.17(J) ^T	0.17 ⁸
Si (mg/L)	8.02(J) ⁸	10.2(J) ⁸	9.0 ^T /8.7 ^T	12.00(J+) [§]	10.50(J+) ^S /10.50(J+) ^S	10.10(J+) [§]	9.95(J+) ^{\$}	9.54(J+) ^{\$}	9.09(J+) ^{\$}	8.81(J+) ^S	8.43(J+) ⁸	8.18(J+) ^S	6.4 ^T	7.69(J+) [§]
Dissolved Metals	• '	• '					1		1					
Ag (μg/L)	<51 ⁸	<51s	<0.033 ^T /<0.033 ^T	<14 ⁸	<14 ^S /<14 ^S	<14 ⁸	<148	<14 [§]	<14§	<14 [§]	<14 ⁸	<14 ⁸	<0.033 ^T	<14 [§]
Al (μg/L)	422(Л) ⁸	382(J) ⁸	170 ^T /170 ^T	205(J) ⁸	234(J) ^S /245(J) ^S	211(J) ⁸	<494 [§]	<494 [§]	<494 [§]	<494 ⁸	<494 ⁸	<494 ⁸	100 ^T	<494 [§]
As (µg/L)	<51 ^s	<51 ⁸	$0.62(J)^T/<0.33^T$	0.40(J) ^C	0.49(J) ^c /0.71(J) ^c	<1.00°C	0.53(J) ^C	0.28(J) ^C	0.82(J) ^C	0.47(J) ^C	0.43(Л) ^с	0.59(J) ^C	<0.33 ^T	<1.00°
B (µg/L)	154(J) ⁸	117(J) ⁸	130 ^T /130 ^T	142(J) ⁸	136(J) ^{\$} /136(J) ^{\$}	131(J) ⁸	130(J) ⁸	128(J) ⁸	126(J) ^S	125(J) ^S	123(J) ^S	121(J) ^S	120 ^T	119(J) ^S
Ba (μg/L)	41(J) ^s	26(J)	23 ^T /20 ^T	21(J) ^s	21(J) ⁸ /21(J) ⁸	20(J) ^s	20(J) [§]	20(J) ^{\$}	20(J) [§]	20(J) [§]	20(J) ^{\$}	20(J) ^{\$}	21 ^T	19(J) [§]
Be (μg/L)	<4 ^S	<4 ^S	<0.08 ^T /<0.08 ^T	<10 ^S	<10 ^S /<10 ^S	<10 ⁸	<10 ^S	<10 ^S	<10 ^S	<10 ^S	<10°s	<10°s	<0.08 ^T	<10 ⁸
Cd (µg/L)	<4	<4 s	<0.1 T/<0.1T	<1.00°	<1.00°/<1.00°	<1.00°	<1.00°	<1.00°	<1.00°	<1.00°	<1.008	<1.008	<0.1 ^T	<1.00°
Co (μg/L)	<4 S	<4 ^S	<0.054 ^T /<0.054 ^T	<4 ^S	<4 ^S /<4 ^S	<4 ^S	<4 ^S	<4 ^S	<4 ^S	<4 ^S	<4 ^S	<4 ^S	<0.004 ^T	<4 ^S
Cr (µg/L)	<4 ^S	<4 ^S	<0.5 ^T /<0.5 ^T	<2.00°	2.2 ^S /<2.00 ^S	<2.00 ^S	<2.00°s	<2.00 [§]	<2.00 [§]	<2.00 ^S	<2.00°	<2.00 ^S	<0.5T	<2.00°
Cu (µg/L)	<98	<9 [§]	<0.56 ^T /<0.56 ^T	<2.00 ^S	<2.00 ^{\$} /<2.00 ^{\$}	<2.00 ^S	<2.00 ^{\$}	<2.00 ^{\$}	<2.00 ^{\$}	<2.00°	<2.00 ^{\$}	<2.00 ^{\$}	< 0.56 ^T	<2.00°
Fe (µg/L)	<63 [§]	>63 [§]	<22T/<22T	<67 [§]	<67 ^S /<67 ^S	<67§	<67 ^s	<67 ^s	<67 [§]	<67 ^s	<67 ^S	<67 ⁸	<22 ^T	<67 ^s
Hg (μg/L)	NA	NA	<0.027T/<0.027T	NA	NA	NA	NA	NA	NA	NA	NA	NA	<0.027 ^T	NA
Li (μg/L)	NA	NA	44 ^T /45 ^T	NA	NA	NA	NA	NA	NA	NA	NA	NA	33 ^T	NA
Mn (μg/L)	<4 S	<4 ⁸	<0.31 ^T /1 ^T	<14 [§]	<14 ^S /<14 ^S	<14 ⁸	<14 ^S	<14 ⁸	<14 ⁸	<14 ^S	<14 ^S	<14 ^S	0.42(J) ^T	<14 ^S
Mo (μg/L)	20 ⁸	<7s	10 ^T /9.7 ^T	7(J) ⁸	7(J) ^{\$} /8(8) ^{\$}	5(J) ⁸	<17 ⁸	<17 ^s	<17 ⁸	<17 ⁸	<17 ⁸	<17 ⁸	7.6 ^T	<17 ^s
Ni (μg/L)	1(J) ^S	3(J) ⁸	<0.3 ^T /<0.3 ^T	<1.00 ^s	<1.00 ⁸ /0.39(J) ⁸	<1.00 ^S	0.23(J) ^S	<1.00 ⁸	<1.00 ⁸	<1.00 ^S	<1.00 ^S	<1.00 ^S	<0.3 ^T	<1.00 ^S
P (μg/L)	<0.014 ⁸	<0.014 ⁸	57 ^T /89 ^T	<0.06 ^{\$}	<0.06 ⁸ /<0.06 ⁸	<0.06 ^{\$}	<0.06 ⁸	<0.06 ⁸	<0.06 ⁸	<0.06 ^s	<0.06 ⁸	<0.06 ⁸	61 ^T	<0.06 ^s
Pb (μg/L)	<11s	<11s	<0.18 ^T /<0.18 ^T	<1.008	<1.00°/<1.00°	<1.008	<1.008	<1.00 ⁸	<1.008	<1.008	<1.00s	<1.00°	<0.18 ^T	<1.008
Sb (μg/L)	R [§]	R [§]	<0.4 ^T /0.54(B) ^T	<2.00°	<2.00 ^{\$} /<2.00 ^{\$}	<2.00 ^{\$}	<2.00 ⁸	<2.00\$	<2.00\$	<2.00 ^{\$}	<2.00 ^{\$}	<2.00 ^{\$}	<0.4 ^T	<2.00 ^{\$}
Se (μg/L)	<16 ^s	<16 ⁸	<0.7/<0.7	<5.00 ^S	<5.00 ^S /<5.00 ^S	<5.00 ^S	<5.00 ^s	<5.00 ^s	<5.00 ^{\$}	<5.00 ^S	<5.00 ^S	<5.00 ^S	<0.7 ^T	<5.00 ^{\$}
Sr (μg/L)	801 ^s	441 ^s	300 ^T /310 ^T	328 ⁸	315 ⁸ /314 ⁸	312 ⁸	309 ⁸	307 ^s	304 ⁸	301 ^s	298 ^{\$}	301 ^s	280 ^T	291 ^s
Ti (μg/L)	<4 ^S	<4 ⁸	<0.6 ^T /<0.6 ^T	<7\$	<7 ^{\$} /<7 ^{\$}	<7\$	<7 ^{\$}	<7s	<7 ^{\$}	<7 ^{\$}	<7 ^{\$}	<7 ^{\$}	<0.6 ^T	<7 ^{\$}
Tl (μg/L)	<37 [§]	R ^{\$}	<0.05 ^T /<0.05 ^T	<1.00 ^S	<1.00 ^{\$} /<1.00 ^{\$}	<1.00 ^S	<1.00\$	<1.00\$	<1.00\$	<1.00 ^{\$}	<1.00\$	<1.00\$	<0.05 ^T	<1.00\$
U (μg/L)	NA	NA	<0.05 ^T /<0.05 ^T	NA	NA	NA	NA	NA	NA	NA	NA	NA	<0.05 ^T	NA
V (µg/L)	4(J) ⁸	NA	$0.6(J)^{T}/<0.5^{T}$	<10 ⁸	<10 ^S /<10 ^S	<10 ⁸	<10 ⁸	<10 ⁸	<10 ^s	<10 ⁸	<108	<108	<0.5 ^T	<10 ⁸
Zn (μg/L)	<24 ⁸	<24 ⁸	<2 ^T /<2 ^T	<50 ⁸	<50 ⁸ /<50 ⁸	<50 ⁸	<50 ⁸	<50 ⁸	<50 ⁸	<50 ⁸	<50 ⁸	<50 ⁸	<2 ^T	<50 ^{\$}

Laboratories (Superscript)

Shaw Environmental, Ada, OK (Contractor to EPA) О

EPA ORD Ada, OK EPA Region 8 Laboratory, Golden, CO U.S. Geological Survey National Water Quality Laboratory EPA Region 3 Laboratory, Fort Meade, MD R8 R3 U ALS Environmental (Contractor to EPA)

A E Chemtech Consulting (contractor to EPA) Eberline Laboratory (contractor to USGS)

Data Qualifiers

Not analyzed NA

Estimated (non-attainment of quality control criteria or below reporting limit. R3 and ORD Las Vegas analysis are estimated because of method development)

Estimated (biased low due <70% matrix spike recovery in USGS samples, exceedance of holding time in R8 Phase IV samples, or other quality assurance factors) J+

Estimated (biased high due to >130% matrix spike recovery in USGS samples or other quality assurance factors)
Estimated (method development on alcohols)^{65,66}

В Analyte in sample < 10X and < 5X concentration detected in a blank for EPA and USGS data respectively

Relative percent difference outside acceptance criteria D

R Sample result rejected due to serious deficiencies in analysis

Acetone result in Phase V corrected from EPA (2012)

EPA ORD, Las Vegas, NV

Test America Laboratory (Contractor to USGS and EPA)

Table SI E4a. Summary of Organic Compound Detections in MW02

Cable SI E4a. Summary of Organic Com           Compound	EPA	EPA	EPA	EPA	USGS
	Phase III	Phase IV	Phase V	Phase V	Phase V
			0412-1	0412-2	0412-2
Borehole Volumes	0.1	0.6	0.0	1.0	1.0
dissolved organic carbon (mg/L)	14.5°	19.7 ^o	19.4 ^o	15.5°	13 ^T
diesel range organics (µg/l)	1440(J) ^{R8}	$4050(D)^{R8}/4200(D)^{R8}$	4150 ^{R8}	2100 ^{R8}	670 ^T
gasoline range organics (µg/l)	3710 ^{R8}	2800 ^{R8} /3200 ^{R8}	4500 ^{R8}	5290 ^{R8}	6800 ^T /7700 ^T
benzene (µg/l)	246 ^{R8}	183 ^s /191 ^s	166 ^s	232 ^s	250 ^T /260 ^T
		139(J-) ^{R8} /164(J-) ^{R8} 482 ⁸ /464 ⁸	175(J) ^{R8} 402 ^S	$247(J)^{R8}$	
toluene (µg/l)	617 ^{R8}			607 ^s	690 ^T /710 ^T
		336(J-) ^{R8} /424(J-) ^{R8}	437(J) ^{R8}	677(J) ^{R8}	
ethylbenzene (µg/l)	67.0 ^{R8}	68.7 ^s /62.0 ^s	61.1 ^s	101 ^s	$100^{\mathrm{T}}/100^{\mathrm{T}}$
		$21.5(J-)^{R8}/27.0(J-)^{R8}$	57.0(J) ^{R8}	89.6(J) ^{R8}	
m,p - xylenes (μg/l)	572 ^{R8}	630 ^S /554 ^S	549 ^s	894 ^S	1000 ^T /1000 ^T
	P.O.	$280(J-)^{R8}/354(J-)^{R8}$	578(J) ^{R8}	973(J) ^{R8}	T T
o-xylene (µg/l)	178 ^{R8}	175 ^S /160 ^S	161 ^s	245 ⁸	260 ^T /250 ^T
	no	$81.6(J-)^{R8}/102(J-)^{R8}$	164(J) ^{R8}	253(J) ^{R8}	T T
isopropylbenzene (μg/l)	11.0 ^{R8}	$<12.5(J-)^{R8}/<12.5(J-)^{R8}$ 9.0		9.40(J) ^{R8}	$11(J)^{T}/12(J)^{T}$
n-butylbenzene (μg/l)	<6.25 ^{R8}	$<12.5(J-)^{R8}/<12.5(J-)^{R8}$ 0.3		<5.0 ^{R8}	<6.4 ^T /<6.4 ^T
sec-butylbenzene (μg/l)	<6.25 ^{R8}	$<12.5(J-)^{R8}/<12.5(J-)^{R8}$ 1.0		<5.0 ^{R8}	<3.4 ^T /<3.4 ^T
tert-butylbenzene (μg/l)	<6.25 ^{R8}	$<12.5(J-)^{R8}/<12.5(J-)^{R8}$ 0.8		<5.0 ^{R8}	<3.2 ^T /<3.2 ^T
n-propylbenzene (μg/l)	5.75(J) ^{R8}	$<12.5(J-)^{R8}/<12.5(J-)^{R8}$ 9.9	(J) R8	11.8(J) ^{R8}	$13(J)^{T}/12(J)^{T}$
p-isopropyltoluene (μg/l)	<6.25 ^{R8}	<12.5(J-) ^{R8} /<12.5(J-) ^{R8}	1.36(J) ^{R8}	<5.0 ^{R8}	<4.0 ^T /<4.0 ^T
styrene (µg/l)	<6.25 ^{R8}	$<12.5(J-)^{R8}/<12.5(J-)^{R8}$ 0.4		<5.0 ^{R8}	<3.4 ^T /<3.4 ^T
1,3,5-trimethylbenzene (µg/l)	35.5 ^{R8}	43.6 ⁸ /35.0 ⁸	39.5 ^s	71.4 ^s	86 ^T /91 ^T
1,2,4-trimethylbenzene (µg/l)	69.2 ^{R8}	84.1 ^s /67.2 ^s	77.0 ^s	148 ⁸	$140^{\mathrm{T}}/150^{\mathrm{T}}$
		$18.5(J-)^{R8}/23.0(J-)^{R8}$			
1,2,3-trimethylbenzene (μg/l)	NA	28.8 ⁸ /23.8 ⁸	27.6 ^s	45.5 ^s	45 ^T /46 ^T
naphthalene (μg/l)	1.41 ^{R8} /4.25(J) ^{R8}	4.61 ^s /3.87 ^s	4.89 ^s	7.49 ^s	$7.2(J)^{T}/7.9(J)^{T}$
		3.32 ^{R8} /<5.0 ^{R8}	$7.19(J)^{R8}/4.29^{R8}$	$7.20(J)^{R8}/4.78^{R8}$	
		<12.5(J-) ^{R8} /<12.5(J-) ^{R8}			
1-methylnapthalene (μg/l)	$0.66^{R8}$	1.03 ^{R8} /<5.00 ^{R8}	2.23 ^{R8}	2.85 ^{R8}	$3.5^{\mathrm{T}}$
2-methylnapthalene (μg/l)	1.15 ^{R8}	1.75 ^{R8} /<5.0 ^{R8}	4.08 ^{R8}	5.52 ^{R8}	6.7 ^T
phenol (µg/l)	13.7 ^{R8}	14.5 ^{R8} /29.2 ^{R8}	32.7(J-) ^{R8}	16.0 ^{R8}	23 ^T
2-methylphenol (μg/l)	13.8 ^{R8}	10.3 ^{R8} /20.9 ^{R8}	22.2 ^{R8}	20.8(J) ^{R8}	25 ^T
3&4-methylphenol (μg/l)	26.2 ^{R8}	$16.9(D)^{R8}/34.6(D)^{R8}$	39.8 ^{R8}	33.5 ^{R8}	45 ^T
2,4-dimethylphenol (μg/l)	28.6 ^{R8}	$23.2(D)^{R8}/46.3(D)^{R8}$	36.6(J+) ^{R8}	32.0 ^{R8}	67 ^T
isopropanol (μg/l)	NA	581 ^s /583 ^s	862 ^s	802 ^s	<260 ^T
n-propanol (μg/l)	NA	<100 ^S /<100 ^S	63(J-) ^S	$11.8(J^{\dagger})^{S}/<100(J_{-})^{S}$	NA
methanol (μg/l)	NA	NA	<5000 ^A	<5000 ^A	NA
				592(J†) ^s	
tert-butyl alcohol (µg/l)	NM	4470 ^{\$} /4580 ^{\$}	5910 ^s	5395(†) ⁸ /6120 ⁸	6300 ^T /6300 ^T
acetone (µg/l)	NA	$641(J-)^{R8}/616(J-)^{R8}$	1460 ^s	231 ^S	$350^{T}/450^{T}$
		DO DO	982(J) ^{R8}	157(J) ^{R8}	T T
2-butanone (MEK) (μg/l)	NA	120(J-) ^{R8} /118(J-) ^{R8}	208(J) ^{R8}	86.2(J) ^{R8}	<120 ^T /<40 ^T
4-methyl-2-pentanone (MIBK) (μg/l) N	A	$12.5(J-)^{R8}/<12.5(J-)^{R8}$	<0.25 ^{R8}	<5.0 ^{R8}	<20 ^T
benzoic acid (µg/l)	244 ^{R8}	$209(D)^{R8}/364(D)^{R8}$	513 ^{R8}	110(D) ^{R8}	190 ^T
ethylene glycol (μg/l)	NA	NA	<5000 ^A	<5000 ^A	<8630 ^T
propylene glycol (μg/l)	NA	NA	<5000 ^A	<5000 ^A	<18700 ^T
diethylene glycol (R3) (µg/l)	NA	$1570(J+)^{R3}/1610(J+)^{R3}$	1260(J-) ^{R3}	378(J) ^{R3}	<7730 ^T
triethylene glycol (R3) (µg/l)	NA	$310(J-)^{R3}/293(J-)^{R3}$	262(J-) ^{R3}	72.3(J) ^{R3}	<8450 ^T
tetraethylene glycol (R3) (μg/l)	NA	$27.2(J,B)^{R3}/29.0(J-,B)^{R3}$	22.6(J-) ^{R3}	3.6(J) ^{R3}	NA
2-butoxyethanol (μg/l)	NA	$<0.10(J-)^{R3}/<0.10(J-)^{R3}$	6.8(J-) ^{R3}	<5.0 ^{Ŕ3}	$TIC^T$
		$<0.10(J-)^{R8}/<0.10(J-)^{R8}$	<1.0 ^{R8}	<1.0 ^{R8}	
ethyl ether (μg/l)	<6.25 ^{R8}	$12.5(J-)^{R8}/<12.5(J-)^{R8}$	1.94(J) ^{R8}	<5.0 ^{R8}	<5.2 ^T
nonylphenol (μg/l)	NA	NA	28(J-) ^L	7.4-7.9(J-) ^L	NA
octylphenol (µg/l)	NA	NA	2.9 (J-) ^L	0.5-0.7(J) ^L	NA
acrylamide (µg/L)	NA	NA	<0.20 ^L	<0.20 ^L	NA
lactate (µg/L)	NA	213 ⁸ /253 ⁸	250 ^s	<100 ^S	NA
formate (µg/L)	NA	558 ^S /584 ^S	R	R	NA
acetate (µg/L)	NA	4310 ^S /4200 ^S	4800 ^s	2840(J) ^S	NA
propionate (µg/L)	NA	808 ^s /687 ^s	844 ^s	687(J) ^S	NA
adamantine (μg/L)	<6.25 ^{R8}	<12.5(J-) ^{R8} /<12.5(J-) ^{R8}	<0.25 ^{R8}	<5.0 ^{R8}	NA
	>0.20 ^{R8} /<6.25 ^{R8}	$<0.10(J-)^{R8}/<5.0(J-)^{R8}$	<0.25 ^{R8}	<5.0 ^{R8}	NA
1,3-dimethyl adamantine (μg/L)	<i>&gt;</i> 0.20 /<6.23	<0.10(3-) /<3.0(3-)			
1,3-dimethyl adamantine (μg/L) methylene blue active substances	NA	NA	<0.20 ^T	<0.20 ^T	$0.12(J)^{T}$

Table SI E4b. Summary of Field Parameters, Major Ions, and Dissolved Metals at MW02

Compound	EPA Phase III	EPA Phase IV	EPA Phase V 0412-1	EPA Phase V 0412-2	USGS Phase V 0412-2
Borehole Volumes	0.1	0.6	0.0	1.0	1.0
Field Parameters	-			-	-
pH	12.01	11.78	11.96	11.81	NM
specific conductance (µS/cm)	3812	3099	3313	2888(J)	NM
dissolved oxygen (mg/l)	0.0	0.02	0.02	0.01	NM
oxidation reduction potential (mV)	121	-108	-154	-148	NM
turbidity (NTU)	28.8	24.0	4.5	15.7	NM
alkalinity (mg/l CaCO3)	456	482	390	254	NM
Major Ions					
nitrate + nitrite (mg N/L) (mg/L)	0.379(B) ^o	<0.100°/<0.100°	0.056°	0.095°	<0.019
ammonia (mg N/L)	1.95°	2.88°/2.82°	2.61°	1.23°	0.81(B)
SO4 (mg/l)	12.1°	62.6°/62.5°	81.8°	13.5°	14
S (mg/L)	6.8(B)	$25.1(J)^{S}/25.0(J)^{S}$	32.1(J) ^S	7.38(J) ^S	NA
Cl (mg/l)	466°	457°/456°	469°	495°	520
Br (mg/l)	NA	<3.00°/<3.00°	<1.00°	<1.00°	1.9
F (mg/l)	1.01°	$1.54(J)^{\circ}/1.49(J)^{\circ}$	1.50°	1.16°	1.6
K (mg/l)	39.5(J) ^s	43.6(J) ⁸ /44.0(J) ⁸	31.4(J) ^S	16.6(J) ^S	15.0
Na (mg/l)	420(J) ^s	448(J) ^S /449(J) ^S	429(J) ^S	379(J) ^s	400(B)
Ca (mg/l)	73.3 ^s	60.5 ⁸ /60.6 ⁸	50.8 ⁸	36.1 ^s	33.0
Mg (mg/l)	<0.05 ^s	$0.03(J)^{S}/0.02(J)^{S}$	<0.10 ^s	<0.10 ^s	49(J)
Si (mg/L)	3.00(J) ^S	2.94(J) ⁸ /2.93(J) ⁸	4.89(J+) ^S	5.00(J+) ^S	15.0
Dissolved Metals	5.00(3)	2.5 1(0) 72.55(0)	1.05(01)	3.00(3+)	13.0
Ag (µg/L)	<51 ^S	<51 ^S	<14 ^S	<14 ^S	< 0.033
Al (μg/L)	577(J) ⁸	684(J) ^{\$} /736(J) ^{\$}	660(J) ^S	816(J) ^S	700
As (µg/L)	<51 ^S	<51 ^S /<51 ^S	3.1 ^s	3.4 [§]	3.1(J)
Β (μg/L)	103(J) ⁸	$109(J)^{S}/108(J)^{S}$	114(J) ^S	108(J) ^S	110
Ba (μg/L)	210(J) ^S	93(J) ⁸ /93(J) ⁸	95(J) ^S	147(J) ^S	150
Be (μg/L)	<4 ^S	<4 ^S /<4 ^S	<10 ^S	<10 ^S	<0.08
Cd (µg/L)	<4 ^S	<4 ^S /<4 ^S	<1.00 ^S	<1.00 ^s	<0.1
Co (µg/L)	<4 ^S	<4 ^S /<4	<4 ^S	<4 ^S	0.085
Cr (µg/L)	<4 ^S	<4 ^S /<4 ^S	<2.00 ^s	<2.00 ^s	4.5
Cu (µg/L)	<9 ^S	<9 ^S /<9 ^S	<2.00 ^S	4.4 ^S	3.7
Fe (µg/L)	<63 ⁸	19(J) ^{\$} /<63 [§]	<67 ^S	151 ^S	400
Hg (µg/L)	NA	NA	NA	NA	<0.027
Li (µg/L)	NA	NA	NA	NA	25
Mn (µg/L)	<4 ^S	<4 ^S /<4 ^S	<14 ^S	<14 ^S	5.6
Mo (μg/L)	14 ^s	13 ⁸ /14 ⁸	6(J) ^S	<14 ^S	2.1
Ni (μg/L)	4 ^S	$2^{S}/2(J)^{S}$	4.3 ⁸	2.6 ^S	6
P (µg/L)	<0.014 ^s	$0.014(B)^{S}/0.024(B)^{S}$	<0.06 ^s	<0.06s	65
Pb (μg/L)	<11 ^S	<11 ^S /<11 ^S	<1.00 ^S	<1.00 ^s	<0.018
Sb (μg/L)	R ^S	R ^S /R ^S	<2.00 ^S	<2.00 ⁸	1.3(B)
Se (μg/L)	14(J) ^S	<16 ⁸ /9(J) ⁸	4.7(J) ^S	4.9(J) ^S	<0.7
Sr (µg/L)	2020 ^s	1780 ^S /1790 ^S	1260 ^s	806 ^s	780
Ti (µg/L)	<4 ^S	<4 ^S /<4 ^S	<7 ^S	<7 ^S	2.7(J)
Tl (μg/L)	<37 ^s	R ^S /R ^S	<1.00 ^S	<1.00 ^s	<0.05
U (μg/L)	NA NA	NA	NA	NA NA	<0.05
V (µg/L)	<7 ^S	<7 ^S /<7 ^S	<10 ^S	<10 ^S	2.1(J)
Zn (µg/L)	<24 ⁸	32 ⁸ /24 ⁸	<50 ^S	<50 ^S	49

<u>Laboratories</u> (Superscript)

Shaw Environmental, Ada, OK (Contractor to EPA)

O

EPA ORD Ada, OK

L EPA ORD, Las Vegas, NV R8 EPA Region 8 Laboratory, Golden, CO

R3 EPA Region 3 Laboratory, Fort Meade, MD T Test America Laboratory (Contractor to USGS and EPA)

USGS Laboratory A ALS Environmental (Contractor to EPA)

U USGS Laboratory C Chemtech Consulting (contractor to EPA)

#### Data Qualifiers

NA Not analyzed

Estimated because of non-attainment of certain quality control criteria or concentration below quantitation limit. R3 and ORD Las Vegas analysis are estimated because of method development.

- J- Result is estimated because but may be biased low due <70% matrix spike recovery in USGS samples, exceedance of holding time in R8 Phase IV samples, or other quality assurance factors.
- Result is estimated but may be biased high due to >130% matrix spike recovery in USGS samples or other quality assurance factors.
- J(†) Estimated because of method development on alcohols (Shaw 2012,,b)
- B Analyte in sample < 10X and < 5X concentration detected in a blank for EPA and USGS data respectively
- D Relative percent difference outside acceptance criteria
- R Sample result rejected due to serious deficiencies in analysis

Table SI E5. Light Hydrocarbon and Isotope Analysis of Production Wells and EPA Monitoring Wells

	BH	C ₁	C ₂	C ₃	C ₄	14C1	$\delta^{13}C_1$	$\delta DC_1$	$\delta^{13}C_2$	δDC ₂	δ ¹³ C ₃	δDC ₃	$\delta^{13}iC_4$	δ ¹³ nC ₄
	vol	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(%	(%)	(%)	(‰)	(%)	(%)	(‰)	(%)	(%)
I-b(1003)					-	pmc)								
Johnson and Rice (1993) Tribal Pavillion 14-6 (WR) (g)	T	T	T		T	NA	-39.24	NA	NA NA	l NA	I NA	NA NA	NA	NA
Govt 21-5 (WR) (g)						NA NA	-39.24	NA NA	NA NA	NA NA	NA NA	NA NA	NA NA	NA NA
· / W					_									
Tribal Pavillion 41-9 (FU) (g)						NA	-38.04	NA	NA NA	NA	NA NA	NA	NA	NA
Tribal Pavillion 14-11 (FU) (g)						NA	-38.4	NA	NA	NA	NA	NA	NA	NA
Blankenship Fee 4-8 (FU) (g)						NA	-38.08	NA	NA	NA	NA	NA	NA	NA
Phase II	_					1	20.75	1 202 41	2 4 0 2 1	1 4 5 2 5 1	1 24 221	1 1 1 7 2 1	25.00	T 25 25
Tribal Pavillion 14-10 (WR)						NA	-38.75 ^I	-203.4 ^I	-26.93 ^I	-162.5 ^I	-24.93 ^I	-147.2 ^I	-25.83 ^I	-25.26 ^I
(PGPP01)					_	37.	20.07					+	+	
Tribal Pavillion 43-10 (FU)						NA	-39.07 ^I	-212.99 ^I	-25.99 ^I	-157.5 ^I	-19.40 ^I	NA	NA	-23.87 ^I
(PGPP02)							20.04		1			7		
Tribal Pavillion 24-2 (WR)						NA	-39.26 ¹	-204.9 ^I	-26.79 ^I	-166.2 ^I	-25.33 ^I	-148.0 ⁱ	-25.66 ^I	-25.05 ^I
(PGPP04)					_									
Tribal Pavillion 33-10 (FU)						NA	-39.05 ¹	-207.3 ^I	-26.21 ¹	-161.1 ¹	-18.46 ^I	-101.7 ^I	-23.96 ^I	-23.64 ^I
(PGPP05)	_						20.201	24.5.25	24.42	4 40 01	2101	4 . 7 . 7	2.5.25	2 ( 0 7)
Tribal Pavillion 14-2 (FU)						NA	-39.28 ¹	-215.3 ^I	-26.42 ^I	-162.3 ^I	-24.01 ^I	-145.2 ^I	-25.33 ^I	-24.87 ^I
(PGPP06)														
MW01			1 6	0	I	T			1	1		T		
EPA Phase III	0.3	16.0 ^s	2.23 ^s	0.79 ^s	0.158 ^s	NA	-38.89 ^T	-191.3 ^I	-26.55	NA	-23.85 ¹	NA	NA	NA
EPA Phase III(g)						<0.21	-39.44 ^I	-209.1 ^I	-26.63	-165.0 ^I	-23.76 ^I	-143.7 ^I	NA	NA
EPA Phase IV	0.7	17.93 ^s	2.95 ^s	1.25 ^s	0.172(J) ^S	NA	-38.88 ^I	-211.6 ^I	-26.70	NA	-24.40 ^I	NA	-25.3 ^I	-24.4 ^I
EPA Phase IV(g)						NA	-39.25 ¹ / -39.28 ¹	-211.2 ^I / -210.1 ^I	-26.67 ¹ / -26.67 ¹	-166.8 ^I / -167.4 ^I	-23.74 ^I / -23.91 ^I	-146.1 ^I / -146.6 ^I	NA	NA
USGS Phase V	1.6-3.0	27.5 T/30.5T	3.6(J+) ^T /	1.4 ^T /	NA	2.22 ^w	NA	NA	NA	NA	NA	NA	NA	NA
		26 ^{UC} /26 ^{UC}	$4.0(J+)^{T}$	1.3 ^T										
EPA Phase V 0412-4	1.6	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
EPA Phase V 0412	1.8	17.3 S/17.3 S	2.38 ^s /	0.763 ^s /	0.199 ^s /	NA	-38.2 ^I	-205.3 ^I	-26.5 ^I	NA	NA	NA	NA	NA
			2.21 ^s	0.663 ^s	0.169 ^s									
EPA Phase V 0412-2	2.1	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-3	2.3	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-5	2.4	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-7	2.6	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-6	2.7	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-8	2.9	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-9	3.0	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
USGS Phase V	3.0	25.5 ^T /27.0 ^T	3.2(J+) ^T /	1.1 ^T /	NA	1.53 ^w	-38.54 ^I	-208.0 ^I	NA	NA	NA	NA	NA	NA
		$28^{UC}$	$3.3(J+)^{T}$	$1.0^{\mathrm{T}}$									1	
EPA Phase V 0412-10	3.3	18.8 ^s	18.8 ^s	0.715 ^s	0.184 ^s	NA	-38.5 ^I	-205.9 ^I	-26.6 ^I	NA	NA	NA	NA	NA
MW02			1	ı								-		
EPA Phase III	0.1	18.99 ^s	3.20 ^s	1.82 ^s	NA	NA	-41.83 ^I	-203.8	-26.4 ^I	NA	-24.28 ^I	NA	NA	NA
EPA Phase III(g)						<0.2 ^I /	-41.85 ^I /	-209.4 ^I /-	NA NA	NA NA	NA NA	NA NA	NA	NA
	1	1		1		<0.21	-41.72 ¹	209.2 ^I	1		1	1	1	1
EPA Phase IV	0.6	18.82 ^s	2.55 ^S	2.26 ^s		NA	-41.30 ^I /	-210.7 ^I /	-26.25 ^I /	NA	-24.29 ^I /	NA	-25.3 ^I /	-24.3 ^I /
	1			1		1	-41.37 ^I	-208.2 ^I	-26.28 ^I	1	-24.28 ^I	1	-25.3 ¹	-24.5 ¹
EPA Phase IV(g)						NA	-41.05 ¹ /	-208.9 ^I /	-26.10 ^I /	-170.5 ^I /	-24.05 ^I /	NA	NA NA	NA
	1	1		1		1*	-41.01 ¹	-210.8 ^I	-26.09 ^I	-171.4 ^I	-24.06 ^I	1	1	1
EPA Phase V 0412-1	0.0	19.10 ^s	3.06 ^s	1.58 ^s	0.380 ^s	NA	-41.2 ^I	-209.1 ^I	-26.2 ^I	NA	NA NA	NA	NA	NA
EPA Phase V 0412-2	1.0	22.00 ^s	3.07 ^s	1.78 ^s	0.517 ^s	NA NA	-41.2 ^I	-199.6 ^I	-26.3 ^I	NA NA	NA NA	NA NA	NA NA	NA NA
USGS Phase V 0412-2	1.0	32.00 ^s	4.90 ^s	2.20 ^s	NA	NA NA	NA	NA	NA	NA NA	NA NA	NA NA	NA NA	NA NA
BH - Borehole	1.0	34.00	1 4.70	2.20	IVA	11/12	INA	INA	INA	INA	INA	IVA	IVA	1 11/1

BH - Borehole

S - Shaw Environmental

T – Test America

UC – USGS Reston Chlorofluorocarbon Laboratory W – Woods Hole Oceanogrpahic Institute

Table SI E6. Dissolved Inorganic Carbon, Water Isotopes, Tritium, SF6, and He in MW01 and MW02

	Borehole Volumes	DIC (mg/L)	δ ¹³ DIC (‰)	δ ² H (‰)	δ ¹⁸ Ο (‰)	Tritium (pCi/L)	SF ₆ (fg/kg)	He (10 ⁻⁹ cm ³ /g water)	Rn-222 (pCi/L)	Rn-226 (pCi/L)	Rn-228 (pCi/L)
MW01	•••••	***************************************					***************************************				
EPA Phase III	0.3	26.9°	-12.18 ^I	-113.8 ^I	-13.8 ^I	NA	NA	NA	NA	NA	NA
EPA Phase IV	0.7	12.7°	-12.01I	-109.5 ¹	-13.3I	NA	NA	NA	NA	NA	NA
USGS Phase V	1.6-3.0	20 ^T /19 ^T	-14.39 ^w	-113 ^{US} / -113 ^{US}	-13.32 ^{US} / -13.32 ^{US}	0.60 ^{UM}	<1.00 ^{UC}	1170 ^{UC} / 1190 ^{UC}	1060 ^U	0.087 ^E	0.16(R) ^E
EPA Phase V 0412-4	1.6	NA	NA	-112.9 ^I	-13.3 ^I	NA	NA	NA	NA	NA	NA
EPA Phase V 0412	1.8	15.2°/ 15.2°	-11.70 ^I / 12.13 ^I	-113.1 ¹ / -113.0 ¹	-13.2 ¹ / -13.3 ¹	<0.80 ^I / <0.80 ^I	NA	NA	NA	NA	NA
EPA Phase V 0412-2	2.1	NA	NA	-113.0 ^I	-13.3 ^I	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-3	2.3	NA	NA	-113.0 ^I	-13.3 ^I	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-5	2.4	NA	NA	-113.1 ^I	-13.3 ^I	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-7	2.6	NA	NA	-113.2 ^I	-13.3 ^I	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-6	2.7	NA	NA	-113.2 ^I	-13.4 ^I	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-8	2.9	NA	NA	-113.3 ^I	-13.4 ^I	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-9	3.0	NA	NA	-113.4	-13.3 ^I	NA	NA	NA	NA	NA	NA
USGS Phase V	3.0	21 ^T	-14.11 ^W	-113 ^{US}	-13.39 ^{US}	0.30 ^{UM}	<1.00 ^{UC}	2940 ^{UC}	NA	0.100 ^E	0.23 ^E
EPA Phase V 0412-10 3.3		19.1°	-11.94 ^I	-113.6 ^I	-13.3 ^I	< 0.80 ^I	NA	NA	NA	NA	NA
MW02											
EPA Phase III	0.1	20.4°	NA	-117.4 ^I	-14.6 ^I	NA	NA	NA	NA	NA	NA
EPA Phase IV	0.6	1.40°/ 1.39°	DIC too low	-113.4 ^I / -113.5 ^I	-14.2 ^I / -14.3 ^I	NA	NA	NA	NA	NA	NA
EPA Phase V 0412-1	0.0	1.25°	DIC too low	-116.3 ^I	-14.2 ^I	< 0.801	NA	NA	NA	NA	NA
EPA Phase V 0412-2	1.0	2.26°	DIC too low	-116.8 ^I	-14.2 ^I	<0.80 ^I	NA	NA	NA	NA	NA
USGS Phase V 0412-2 1.	þ	4.6 ^T	NA	NA	NA	NA	NA	NA	NA	NA	NA

E - Eberline Laboratory (contractor to USGS)

### E.5 Discussion of Potential Cement-pH Interaction

Elevated pH levels (>11 standard units) were observed during purging and sampling at MW01 and MW02 during Phase III, IV and V sampling events (Figure SI E5). During a period of extensive purging at MW01 (over 5000 L) during the Phase V sampling event, specific conductance decreased from 3.93 to 1.31 mS/cm before stabilizing and pH decreased from 12.14 to 10.70.

Simulations were conducted to evaluate whether trends in pH and specific conductance were due to insufficient purging. Observed specific conductance and pH as a function of time during the Phase V sampling event; calculated casing, borehole, and screen exchange volumes; estimated fraction of stored casing water in the sampling train; and simulated sample train/formation concentration ratios  $(C_P/C_F)$  as a function of hypothetical initial screen/formation concentration ratios  $(C_0/C_F)$  and initial casing/formation concentration ratios  $(C_C/C_F)$  are illustrated in Figure SI E6a. In all calculations, the initial concentration in the screen  $(C_0)$  was set equal to casing concentration  $(C_C)$  or  $C_0/C_F = C_C/C_F$ . Pumping rate and observed drawdown are illustrated in Figure SI E6b.

Simulations indicated that the fraction of casing to formation water entering the sampling train at MW01 during the Phase V sampling event fell below 0.1% at 0.81 borehole volumes and was at 0.003% during the time of first EPA sample collection during the Phase V sampling event. During purging, there

I - Isotech

U - U.S. Geological Survey National Water Quality Laboratory

UC - USGS Restn Chlorofluorocarbon Laboratory

UM – USGS Menlo Park Tritium Laboratory

US – USGS Reston Stable Isotope Laboratory

W – Woods Hole Oceanogrpahic Institute

were 26 screen exchange volumes (casing volume of screen plus annular space outside screen). Regardless of the initial hypothetical condition, when  $C_0/C_F$  and  $C_C/C_F$  were less than unity (i.e., initial concentration in casing and well screen less than surrounding formation), sampling train concentration reached 99% of formation concentration by 0.81 borehole exchanges. When initial hypothetical values of  $C_0/C_F$  and  $C_C/C_F$  were set at values greater than unity (initial concentration in casing and well screen greater than the surrounding formation due to potential well construction effects), sample train concentration reached 101% constant formation concentration by 1.26, 1.48, 1.65, and 1.84 borehole volumes for  $C_0/C_F$  and  $C_C/C_F$  values of 1.5, 3, 10, and 100, respectively. When  $C_0/C_F$  and  $C_C/C_F$  was set to an extreme value of 1000, sample train concentration reached 101% constant formation concentration by 2.27 borehole volumes. Thus, trends in pH observed during purging are due to interaction with formation media, not the wellbore.

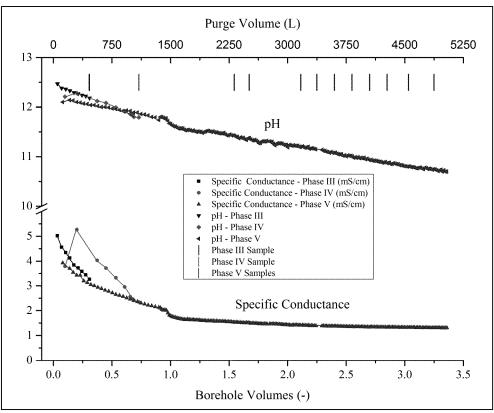


Figure SI E5. Trends in pH and specific conductance during purging at MW01 during Phase III, IV, and V sampling events as a function of purge volume and borehole volumes (1 borehole volume  $\sim 1500$  L). Times of sample collection illustrated by straight bars

pH declined during purging during all three sampling events in an approximately linear fashion (Figures SI E6). Specific conductance declined rapidly and then stabilized after approximately one borehole volume. If reduction in pH and specific conductance were due to dissolved solids remaining in well casing as a result of drilling and/or well construction materials, this would correspond to  $C_0/C_F =$ 

 $C_C/C_F$  values between 10 - 100 for pH and 3 for specific conductance. Reduction in pH and specific conductance and pH during purging occurred much more slowly than would be expected if dissolved solids remained in well casing as a result of well construction effects.

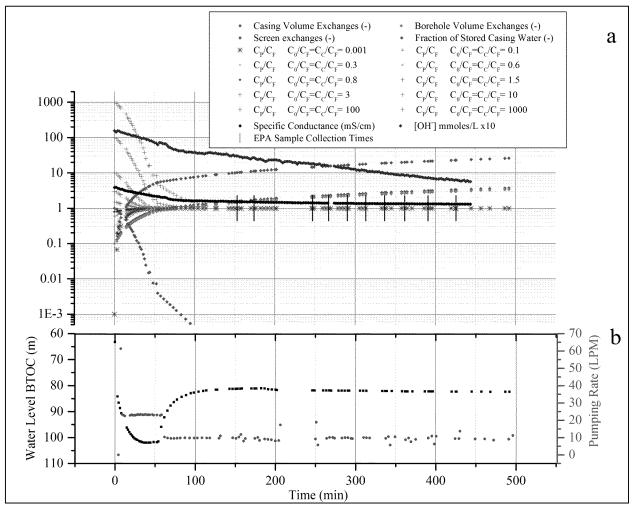


Figure SI E6. (a) Observed decrease in pH (in mmoles/L) and specific conductance during purging as a function of time during the Phase V sampling event in MW01. Increase in casing volumes (up to 3.8), borehole volumes (up to 3.4), and screen exchanges (up to 26), and EPA sample collection times (approximately 30 minutes in duration) illustrated. Simulation of fraction of store casing water in sample train (0.003% at first sample collection), sample train ( $C_P$ ) / formation ( $C_F$ ) concentration ratios as a function of initial screen  $C_0$  and casing  $C_C$  /formation ( $C_F$ ) concentration ratios using a casing plug flow – screen mixing wellbore process model illustrated. (b) Rise in water level in well casing as a result of reduced pumping rate in MW01 during Phase V sampling.

The pH of produced water samples varied from 5.6 to 9.0 standard units (Figure SI E7a). However, pH measurements from produced water samples were primarily from production wells where CO₂ foam was used for hydraulic fracturing. There was substantial variation in hydraulic fracturing practices over time and throughout the field. Potassium hydroxide (KOH) was used for hydraulic fracturing. In ground water having sodium - sulfate (Na-SO₄) type composition, small quantities of KOH addition could result in pH approaching 12 units²⁷. Water flowing to the surface at Tribal Pavillion 13-1

during Bradenhead testing had a pH of 10.86 and nearly all Bradenhead gas samples were devoid of CO₂ (Table SI D3) suggesting elevated pH above intervals of stimulation. There was also an anomalous trend of increasing pH with depth in domestic wells (Figure SI E7b).

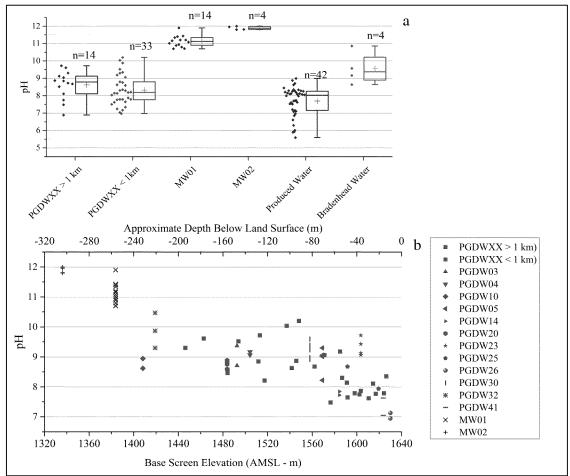


Figure SI E7. (a) Box and whisker plots of minimum, quartiles, median (line), mean (cross), and maximum values of pH of domestic wells (PGDWXX) greater than 1 km from a production well, domestic wells less than 1 km from a production wells, MW01, MW02, produced water, and Bradenhead water samples. Mean values are represented for domestic well locations sampled more than once. Produced water and bradenhead locations were sampled once. Measurement at MW01 and MW02 represent samples collected during Phase III, IV, and V sample events to illustrate variability. (b) pH levels in domestic wells (PGDWXX) less than and greater than 1 km of a production well (red and blue respectively) and monitoring wells as a function of absolute mean seal level (AMSL). All data points are illustrated for locations sampled more than once.

Water from MW01 and MW02 was highly undersaturated with respect to portlandite (Ca(OH)₂) at -4.3 and -2.3 during the Phase V sampling event, respectively. Water in contact with hydrating cement is saturated or oversaturated (saturation index greater than 0) to portlandite⁶⁷⁻⁶⁹ and remains oversaturated prior to degradation (e.g. carbonation)⁷⁰⁻⁷³. Calcium concentrations in MW01 and MW02 were typical of domestic wells (Figure SI E8a) displaying random scatter with depth (Figure SI E8b). Calcium concentrations should be significantly elevated in the presence of cement interaction⁷⁴.

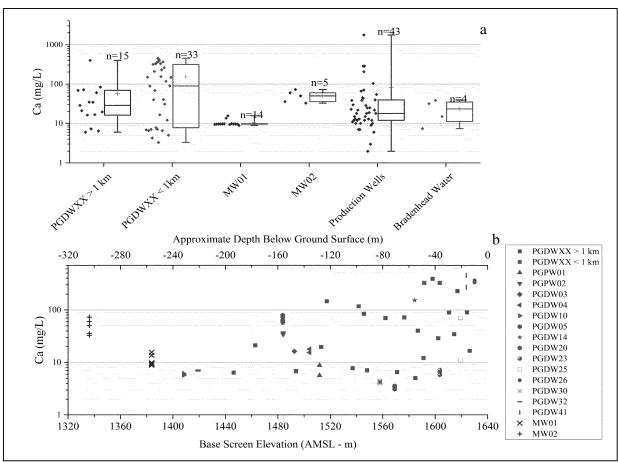


Figure SI E8. (a) Box and whisker plots of minimum, quartiles, median (line), mean (cross), and maximum values of Ca of domestic wells (PGDWXX) greater than 1 km from a production well, domestic wells less than 1 km from a production wells, MW01, MW02, produced water, and Bradenhead water samples. Mean values are represented for domestic well locations sampled more than once. Produced water and bradenhead locations were sampled once. Measurement at MW01 and MW02 represent samples collected during Phase III, IV, and V sample events to illustrate variability. (b) Ca levels in domestic wells (PGDWXX) less than and greater than 1 km of a production well (red and blue respectively) and monitoring wells as a function of absolute mean seal level (AMSL). All data points are illustrated for locations sampled more than once.

Another explanation of elevated pH in MW01 at the start of purging with decrease during purging could be progressive intake of formation water more distal from the screen that has undergone less degassing. Water underwent vigorous degassing and foaming during purging at MW01 and MW02 indicating total dissolved gas pressure (TDGP) significantly above atmospheric pressure (Figure SI E9). During the Phase IV sampling event, pump cavitation occurred at MW02 after removal of 1287 L of water with 40 m of hydrostatic head from the base of the borehole indicating 4.7 atm or 0.48 MPa TDGP (atmospheric pressure = 0.86 atm). Degassing in the immediate vicinity of the borehole could result in removal of carbon dioxide and conversion of bicarbonate/carbonate to non-carbonate alkalinity:

$$HCO_3^- \to CO_{2(g)} + OH^-$$
  
 $CO_3^{2-} + H_2O \to CO_{2(g)} + 2OH^-$ 

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During purging at MW01 in the Phase V sampling event, DIC increased from 15.2 to 19.1 mg/L as pH decreased from 11.34 to 10.71. During development of MW01 in August 2010, prior to gas entry, documented by measurement of lower explosive levels in well casing, pH varied from 8.72 to 9.06 standard units during removal of 33,300 L of water.



Figure SI E9. Photograph of foam in YSI flow cell during purging at MW01

## E.6 Discussion of Potential Cement-Potassium Inter action

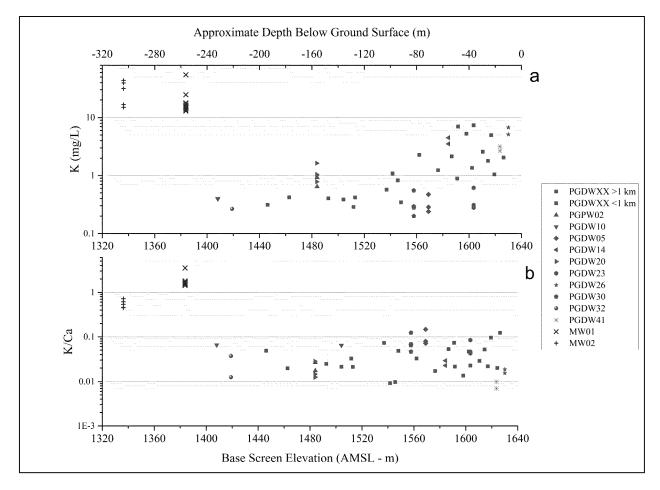
Similar to pH, elevated potassium may be the result of interaction with cement. Alkalis in cement are present as readily soluble sulfates ( $K_2SO_4$  and  $Na_2SO_4$ ) and less soluble oxides ( $K_2O$  and  $Na_2O$ ) in the major clinker minerals^{70-72,75} leading to high alkali and sulfate concentrations during the first hours of hydration⁷⁶.

Potassium and calcium concentrations were positively correlated in domestic well and monitoring wells with apparent random scatter in bradenhead and produced water samples (Figure SI D1). With exception of EPA monitoring wells, potassium concentrations generally decreased with depth (Figure SI 10a) which was reduced to random scatter when potassium was normalized by calcium concentrations (Figure SI E10b).

Potassium concentrations decreased during purging at MW01 during the Phase V sampling event while calcium, silicon, chloride, and fluoride remained fairly constant or decreased at a slower rate (Figure SI E11a). Concentrations of sodium and strontium decreased (Figures SI E12b, c) while sulfate increased during purging (Figures SI E11b). Given that soluble sulfates are associated with curing of

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cement, sulfate concentrations should decrease rather than increase during purging. Unlike potassium but similar to calcium, strontium did not decrease during purging during the Phase V sampling event but decreased compared to Phase III and Phase IV sampling events (Figure SI 11c) potentially indicating temporal variability rather than interaction with œment.

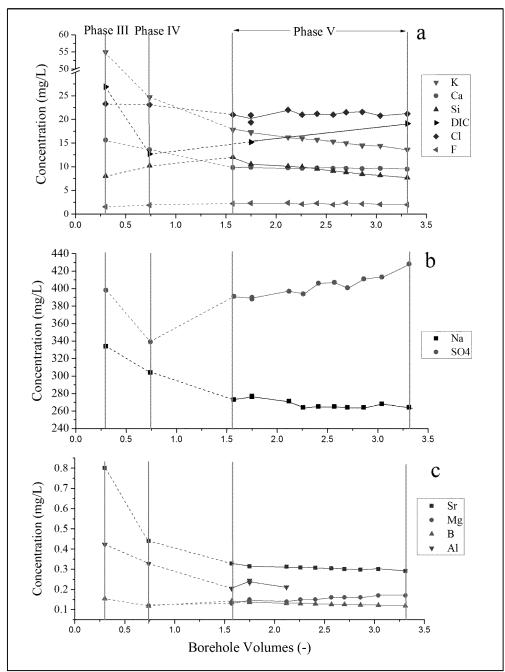


**Figure SI E10**. (a) Potassium concentration and (b) potassium/calcium concentration ratios for domestic wells (PGDWXX) less than and greater than 1 km of a production well, monitoring wells MW01 and MW02, production wells, and bradenhead samples as a function of absolute mean sea level (AMSL). Domestic wells are identified when sampled more than once.

### E.7 Discussion of Potential Cement-Glycol Interacti on

Polar organic compounds, including diethylene glycol (DEG) are used to reduce the energy required to grind clinker material for cement⁷⁷⁻⁸⁰. Thus, it is plausible that detection of glycols in monitoring wells is due to interaction with cement. Smith et al.⁸¹ determined bulk concentrations of glycols and 2-butoxyethanol (2-BE), and a number of selected organic compounds in 5 Type I/II Portland cement samples and conducted a 5-day leaching study on the cured cement sample having the highest bulk concentrations of glycols. DEG, triethylene glycol (TEG), and tetraethylene glycol (TREG) were

detected after the last aqueous exchange at concentrations of 97, 250, and 52  $\mu$ g/l, respectively. 2-BE was not detected.



**Figure SI E11.** Concentration variation of a) potassium (K), calcium (Ca), silicon (Si), dissolved inorganic carbon (DIC), chloride (Cl), and fluoride (F); (b) sodium (Na) and sulfate (SO₄); and (c) Strontium (Sr), magnesium (Mg), boron (B), and aluminum (Al) during purging at MW01 as a function of borehole volume during Phase III, IV, and V sampling events.

During its national study on hydraulic fracturing, EPA conducted analysis of glycols using high performance liquid chromatography with dual mass spectrometry (HPLC-MS/MS) at five retrospective

study areas with non-detection at 83 domestic wells sampled ⁸²⁻⁸⁶. Glycols were only detected in a produced water sample ⁸⁶. Using HPLC-MS/MS analysis, glycols were detected at domestic wells sampled in the Pavillion investigation. The discrepancy in detection of glycols in leachate and domestic well samples may be due variation in use of cement for domestic well construction, product variability, and exposure factors (i.e. dilution, cross-sectional exposure area, etc.) commonly used to evaluate impact of construction materials on water quality.

In EPA Method 1315⁸⁷, a solution to diffusive mass transfer through a semi-infinite media (Crank⁸⁸) is utilized to evaluate mass flux from monolithic samples:

$$Flux = D\rho \left(\frac{\partial C}{\partial x}\right)_{x=0} = \frac{D\rho C_0^*}{\sqrt{\pi Dt}}$$

Flux = diffusive flux ( $\mu g/m$  ² s)

 $C_0^*$  = initial concentration in cement ( $\mu g/kg$ )

 $\rho$  = density of cement (kg/m  3 )

D = diffusion coefficient of diffusing species (m  2 /s)

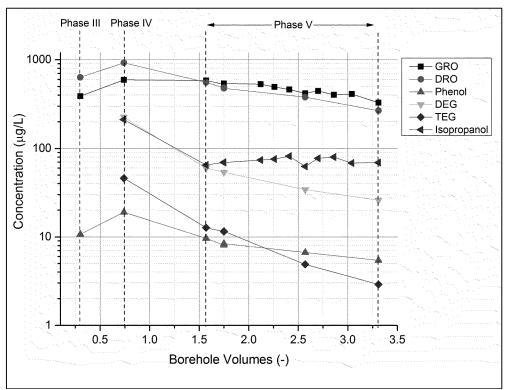
t = time(s).

Using this approach, concentration in a well during purging (C_{well}) (µg/L) can then be estimated by

$$C_{well} = \frac{(flux)(SA)}{flow}$$

To evaluate mass flux from cement at MW01, an unrealistic worst-case scenario of complete encasement of cement around a 22 cm (8.5") diameter pre-packed screen was assumed (surface area =  $4.13 \text{ m}^2$  or  $6406 \text{ in}^2$ ) with bulk DEG concentration of 37,000 µg/kg from Smith et al. Diffusivity of cured cement was set equal to  $10^{-12} \text{ m}^2/\text{s}$  (EPA 2010b) with density of 1850 kg/m³ (density of cement varies from  $1200 - 2500 \text{ kg m}^{-3}$ ). An average flow rate of 16 LPM (flow from MW01 during the Phase V sampling event varied from 8 to 24 LPM) was assumed. The hypothetical concentration of DEG in MW01 decreased from 2.0 µg/L at day 1 to below detection at 0.083 µg/L on day 600 - the approximate time for Phase V sampling after curing of cement. Using the maximum bulk concentration determined by Smith et al. for TEG (79,000 µg/kg) a hypothetical concentration of TEG in MW01 decreased from 43.5 µg/L at day 1 to below detection at 0.178 µg/L on day 600 - L

Glycols decreased during purging in the Phase V sampling. However, compound classes and compounds (GRO, DRO, phenols) not associated with cement also decreased during purging (Figure SI E12) suggesting alternative explanations such as aquifer physical and chemical heterogeneity.



**Figure SI E12.** Concentration of diethylene glycol (DEG) and triethylene glycol (TEG), as a function of borehole volume during Phase III and IV sampling events and while purging during the Phase V sampling event. Concentrations of gasoline range organics (GRO), diesel range organics (DRO), phenol, and isopropanol included for comparison.

A number of investigators have documented non-uniform concentration trends (increasing or decreasing trends as opposed to erratic variation) during purging⁸⁹⁻⁹⁴. Keith et al.⁸⁹ identified a number of potential causative factors for observation of solute concentration trends during purging: physical heterogeneity, chemical heterogeneity, screening of wells over multiple water bearing units. Analytical and numerical modeling indicate that concentration trends during purging could be a function of convergent flow⁹⁵, lithologic layers of varying hydraulic conductivity⁹⁶⁻⁹⁸, anisotropy⁹⁸, the ratio of hydraulic conductivity of the sandpack (in this case open borehole around pre-packed screen) to surrounding formation⁹⁶, well design⁹⁸, and boundary conditions⁹⁸.

Concentration variation during purging could also be due to vertical ambient borehole flow prior to purging. Vertical ambient flow in long-screened monitoring wells such as MW01 and MW02 is well documented⁹⁹⁻¹⁰³. A monitoring well is an open conduit requiring little head differential to induce substantial cumulative flow over an extended period of time between sampling events^{94,100,104-106}.

Significant solute redistribution can occur at head differentials below the sensitivity currently available instrumentation 104.

# Section F - Potential Impact of Unlined Pits on Domestic Wells

Table SI F1. Summary of disposal of drilling mud and production fluids in from production wells

	Unlined Pits Used to Dispose Invert Mud	Unlined Pits Used to Dispose WBM	Unknown Disposal of WBM	Disposal of WBM at Lozier Area	WBM Used on Location	WBM Disposed in Lined Pits	Offsite Disposal of WBM	Totals
Pits Likely Used for Disposal of Production Fluids	41	3	0	0	0	0	0	44
No Production Fluids	16	4	0	0	0	7	0	27
Offsite Disposal of Production Fluids	0	0	10	8	19	26	47	110
Totals	57	7	10	8	19	33	47	181

WBM – water based mud

^{† -} used to construct berms or spread out on site

**Table SI F2.** Summary of disposal of drilling mud and production fluids in pits, results of soil and surficial ground-water sampling, volumes of soil excavation, distance and direction of domestic wells with 600 m of pits, review of completion and stimulation record by WOGCC³¹ of production wells associated with unlined pits, and recommendations

by WOGCC³² for further or no further investigation.

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Production Well Abbreviation	Drilling Mud Used Below Surface Casing	Pit Used or Likely Used to Dispose Drilling Mud and Cuttings Onsite	Pit Used or Likely Used for Disposal of Production Fluids?	Stimulated Prior to Jan 1995?	Number of Soil Screening Locations	Maximum Soil Confamination (mg/kg) and Number of Soil Samples	Excavation Volume (yd²)	Ecxcavation Criterion (mg/kg TPH)	Number of Ground-Water Sampling Locations	Maximum Ground-Water Confamination in Surficial Deposits (ugl) and Number of Ground-Water Samples	Surficial Geology	Domestic Wells Within 600 m of Production Wells (Depth, Distance Direction from Production well)	Stimulation Record Reviewed by WOGCC (2014)	Adequate Site Assessment as Judged by WOGCC (2015)	Further Investigation Recommended by WOGCC (2015)	9
MHR 1	"Chem Gel"	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Qa	PGDW41	Yes	NI	No	Completed amd P&A in 1953. No production or
14-12	Invert	Yes ^U	Yes	Yes	20	GRO:340 (n=23) DRO:4300 (n=23) Benzene: ND (n=20) Toluene: ND (n=20) Ethylbenzene: 0.066 (n=20) Xylenes: 0.085 (n=20)	~1,306	1,000	7	GRO: ND (n=7) DRO: 1,300 (n=7) Benzene: ND (n=7) Toluene: ND (n=7) Ethylbenzene: ND (n=7) Xylenes: ND (n=7)	Qa	(31m,314m,NW) PGDW22 (?m,261m,SW) PGDW32 (206m,563m,SE) P22660.0P (53m,407m,SE) P22661.0P (15m,535m SE)	No	VRP	VRP	stimulation.  Acid stimulation in 1960. Hydraulic fracturing in 1964 with "salt water." Well flowed "diesel and load water." Acid stimulation with additives in 1980. No description of where flowback and other production fluids were disposed. No produced water from 1978 (records start) through 1983 (shut-in). Sundry notice in Jan 1998 for offsite disposal of production fluids. Encana waiting approval from WYDEQ for closure.
23-7	Q-Broxin Gel	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Qa	CR UW09/250 (?,361m, NE)	No	NI	Yes	Well completed and P&A in 1961. Q-BROXIN Gel used. Well history missing from well completion report. Production and stimulation unlikely.
W 1	"Gel"	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	?	None	No	NI	No	Well completed and P&A in 1961. Production and stimulation unlikely.
23-2	Invert	Yes ^u	Yes	Yes	10	TPH: ND (n=2)	0	1,000	0	Not sampled	Qa	None	No	No	Yes	Well completed in 1962. Hydraulic fracturing in 1965  – no description. No description of where flowback and other production fluids were disposed. Production records from 1978. No produced water until 2004. Sundry notice for offsite disposal of production fluids in Jan 1998. Two separate pit locations.
22-35	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	?	None	No	NI	No	Completed & P&A in 1963. Stimulation unlikely.
GOL 1	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Qa	None	No	NI	No	Well completed in 1963. P&A in 1974. No information available on production or stimulation.
14-1	Invert	Yes ^U	Yes	Yes	5	TPH: 3790 (n=5) (Confirmation sample)	~1,400	2,500 or 4,000	0	Not sampled	Qa	PGDW36 (31m,296m,SW)	No	No	Yes	Well completed in 1963. Hydraulic fracturing with undiluted diesel fuel in 1964. In 1993, acid stimulation. No description of where flowback and other production fluids were disposed. Production records from 1978 with 789 bbls produced water prior to 1993. Sundry notice in 1993 to plug water bearing perforation. Sundry notice in Jan 1998 for offsite disposal of production fluids. Post excavation soil TPH exceeded 4000 mg/kg.
21-8	Invert	Yes ^U	Yes	?	0	Not sampled	0		0	Not sampled	Qa	None	No	NI	No	Well completed in 1963. P&A date unknown. Well history missing from well completion report.
21-5	Invert	Yes ^U	Yes	?	13	TPH: 327 (n=8) (Confirmation sample)	~60	7,000	0	Not sampled	Qa	None	No	Yes	No	Well completed in 1963. No documented stimulation until 1999. Production records from 1978. No produced water until 1995. Sundry notice for offsite disposal of production fluids in Jan 1998.
U 13-13	Invert	Yes ^U	Yes	?	5	TPH: 16 (n=5)	0	1,000	0	Not sampled	?	P60032.0W (26m,99m,W)	No	No	Yes	Well completed in 1963. Information on completion missing from well completion report. Production records from 1978. No produced water until 2007. Sundry notice for offsite disposal of production fluids in Jan 1998.
14-6	Invert	Yes ^U	Yes	?	5	TPH: 1298 (n=5) (Confirmation sample)	120	2,500	0	Not sampled		?	No	?	?	Well completion in 1963. Information on completion missing from well completion report. Production records from 1978. No produced water until 2005. Further investigation by WOGCC dependent on potential presence of nearby domestic well.
32-4	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Qa	None	No	NI	No	Completed & P&A in 1963. Stimulation unlikely.
24-14	Invert	Yes ^u	Yes	?	11	TPH: 3910 (n=4)	0	4,000	0	Not sampled	Qa	P59499.0W (34m,330m,NW) P24502.0P (55m,360m, E) PGDW34 (31m,474m, NE)	No	No	Yes	Well completed in 1963. No documented stimulation but completion record not reviewed by WOGCC (2014). Production records from 1978. No produced water until 2004 but sundry notice for offsite disposal of production fluids in Jan 1998.

Production Well Abbreviation	Drilling Mud Used Below Surface Casing	Pit Used or Likely Used to Dispose Drilling Mud and Cuttings Onsite	Pit Used or Likely Used for Disposal of Production Fluids?	Stimulated Prior to Jan 1995?	Number of Soil Screening Locations	Maximum Soil Contamination (mg/kg) and Number of Soil Samples	Exervation Volume (yd³)	Ecxcavation Criterion (mg/kg TPH)	Number of Ground-Water Sampling Locations	Maximum Ground-Water Contamination in Surficial Deposits (ugl.) and Number of Ground-Water Samples	Surficial Geology	Domestic Wels Within 600 m of Production Wels (Depth, Distance, Direction from Production well)	Stimulation Record Reviewed by WOGCC (2014)	Adequate Site Assessment as Judged by WOGCC (2015)	Further Investigation Recommended by WOGCC (2015)	Comments
44-20	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Twdr	P9334.0P (6m,430m, SW)	No	NI	Yes	Well completed and P&A in 1964. Stimulation or production unlikely. Further investigation by WOGCC dependent on confirmation of nearby domestic well.
23X-24	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Qa	None	No	NI	No	Well completed and P&A in 1964. Stimulation or production unlikely.
44-17	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Qa	PGDW03 (137m,265m,SE) PGDW04 (134m,351m,SE) P120203.0W (137m,255m,W) P23056.0P (116m,255m,W)	No	NI	Yes	Well completed and P&A in 1964. Stimulation or production unlikely. No investigation recommended by WOGCC if no nearby domestic wells.
34-33	Invert	Yes ^U	No	?	0	Not sampled	0		0	Not sampled	?	None	No	NI	No	Well completed in 1964. P&A unknown. No information on stimulation or production.
33X-10	Invert	Yes ^U	Yes	Yes	?	Sample data not available	~560	1,000	0	Not sampled	Qa	PGDW14 (58m,224m,NW) PGDW23 (53m,172m,SE) (PGDW44 229m,102m,NW) P24508.0P (53m,365m,SE)	Yes	No	Yes	Acid stimulation and well completion in 1964. Hydraulic fracturing in 1965 with "salt waterflow to pit." P&A in 1983. Invert mud up to 10% oil. Production records from 1978. No produced water to 1983.
24X-3	Invert	Yes ^U	Yes	Yes	9	GRO: 9,200 (n=15) DRO: 3,300 (n=15) Benzene: 4.2 (n=15) Toluene: ND (n=15) Ethylbenzene: 110 (n=15) Total Xylenes: 750 (n=15) Naphthalene: 8.6 (n=11)	~1,000	1,000	11	GRO: 45,200 (n=38) DRO: 59,000 (n=38) Benzene: 1,960 (n=38) Toluene: 0.17 (n=38) Ethylbenzene: 950 (n=38) Xylenes: 4,200 (n=38) Naphthalene: 267 (n=10)	Qa	P66345.0W (21m,258m,NW)	No	VRP	VRP	Well completed in 1965. Acid stimulation with solvent in 1966. No description of where flowback and other production fluids were disposed. Production records from 1978 with 9 bbls produced water in 1986 and increasing to 9,653 bbls after 1995. Invert mud up to 55% oil. Sundry notice for offsite disposal of production fluids in Jan 1998. Ground water monitoring ongoing. A remedial alternatives evaluation report is being drafted by Encana.
14-11	Invert	Yes ^U	Yes	?	12	GRO: 7,400 (n=13) DRO: 7,800 (n=13) Benzene: ND (n=4) Toluene: ND (n=4) Ethylbenzene: 5.1 (n=4) Naphthalene: 15 (n=6)	~940	1,000	8	GRO: 91,100 (n=79) DRO: 78,000 (n=79) Benzene: 476 (n=79) Toluene 15 (n=79) Ethylbenzene: 60 (n=79) Xylenes: 68 (n=79) Naphthalene: 486 (n=46)	Qa	PGDW46 (15m,119m,W) P31805.0W (31m,132m,SE) P69549.0W (31m,132m,SE) (Same well?)	No	VRP	VRP	Well completed in 1965. Well completion report and information on stimulation not available. Production records from 1978. No produced water until 2005 but sundry notice for offsite disposal of production fluids in Jan 1998. Remedial Agreement submitted to WOGCC entailing limited additional soil excavation and ground water monitoring by Encana.
13-13	"Chem Gel"	Yes ^U	Yes	Yes	0	Not sampled	0		0	Not sampled	?	None	No	NI	No	Well completed in 1966. P&A date unknown. Hydraulic fracturing with undiluted diesel fuel, 15% HCl, and 4% "salt water" in 1965. No description of where flowback and other production fluids were disposed.
31-15	Invert	Yes ^U	Yes	?	12	TPH: 70 (n=6) (Confirmation sample)	~1,500	5,500	0	Not sampled	Qa	PGDW11 (107m,230m,NE)	No	?	?	Well completed in 1968. Information on completion missing. Production records from 1978 with 8 bbls produced water in 1988 and increasing to 1,493 bbls after 2004. No description of where produced water was disposed. Sundry notice for offsite disposal of production fluids in Jan 1998. Recommendation of further investigation pending - no soil sample in area with highest PID reading (WOGCC 2015)
32-9	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Qa	PGDW42 (61m,375m,NW)	Yes	NI	Yes	Well completion and P&A after in 1968. No apparent stimulation or production. Investigation recommended by WOGCC because of proximity to a domestic well.

Production Well Abbreviation	Drilling Mud Used Below Surface Casing	Pit Used or Likely Used to Dispose Drilling Mud and Cuttings Onsite	Pit Used or Likely Used for Disposal of Production Fluids?	Stimulated Prior to Jan 1995?	Number of Soil Screening Locations	Maximum Soil Contamination (mg/kg) and Number of Soil Samples	Exeavation Volume (yd³)	Ecxcavation Criterion (mg/kg TPH)	Number of Ground-Water Sampling Locations	Maximum Ground-Water Contamination in Surficial Deposits (µg/l) and Number of Ground-Water Samples	Surficial Geology	Domestic Wells Within 600 m of Production Wells (Depth, Distance, Direction from Production well)	Stimulation Record Reviewed by WOGCC (2014)	Adequate Site Assessment as Judged by WOGCC (2015)	Further Investigation Recommended by WOGCC (2015)	Comments
WEL	"Chem Gel"	Yes	Yes	Yes	8	GRO: ND (n=8) DRO: 390 (n=8) BTEX: not analyzed Naphthalene: 0.22 (n=1)	0	1,000	2	GRO: < 0.1 mg/l (n=2) DRO: 0.32 mg/l (n=2) BTEX: <1 - <5 μg/l (n=2) Naphthalene: <1 μg/l (n=2)	Qa	(79m,361m,SE) PGDW40 (67.1m,470m,NE)	Yes	Yes	No	Well completed in 1972. P&A in 1981. Acidized in Frontier formation with HCl and KCl solutions in 1971. Potential wellhead leak and discharge to "pits" discussed in memorandum in 1980. Encana (2015) stated that a pit could not be identified.
41X-10	Invert	Yes ^U	Yes	Yes	7	GRO: ND (n=1) DRO: ND (n=1) Sample data not in well file	0		2	GRO: ND (n=2) DRO: ND (n=2) BTEX: ND (n=2) Sample data not in well file	Qa	PGDW30 (79m,273m,N) PGDW49 (15m,335m,E)	Yes	No	Yes	Well completed in 1973. P&A in 1981. Invert mud contained up to 78% oil while drilling. In 1973 and 1979, hydraulic fracturing with KCl water, gelled KCl, solvents, surfactants, and N ₂ foam. No description of where flowback and production fluids were disposed. P&A due to parted casing and water production. No production record.
41X-2	Invert	Yes ^U	Yes	?	6	TPH: 1190 (n=2)	0	2,500	0	Not Sampled	Qa	None	No	Yes	No	Invert mud up to 76% oil. No documented stimulation or gas production. Sundry notice for offsite disposal of production fluids in Jan 1998.
31X-3	Invert	Yes ^U	Yes	?	17	GRO: 66 (n=24) DRO: 1200 (n=24) Benzene: ND (n=18) Toluene: ND (n=18) Ethylbenzene: ND (n=18) Xylenes: ND (n=18) Naphthalene: 0.34 (n=1)	~4,392	1,000	5	GRO: 300 (n=5) DRO: 2,700 (n=5) Benzene: ND (n=5) Toluene: ND (n=5) Ethylbenzene: 2.4 (n=5) Xylenes: ND (n=5) Naphthalene: ND (n=1)	Qa	P197335.0W (?,301m,NW) P197336.0W (?,304m,NW)	No	Yes	No	Well completed in 1973. No documented stimulation until 2001. Production record from 1983 with 29 bbb in 1986 and 1987. No description of where produced water was disposed. Increased to 1,215 bbls after 2004. Sundry notice for offsite disposal of production fluids in Jan 1998.
42X-11	Invert	Yes ^U	Yes	?	8	GRO: 580 (n=11) DRO: 450 (n=11) Benzene: ND (n=11) Ethylbenzene: 0.52 (n=11) Toluene: ND (n=11) Xylenes: 1.1 (n=11) Naphthalene: 0.58 (n=2)	~900	1,000	7	GRO: 50,000 (n= 59) DRO: 31,000 (n=59) Benzene: 240 (n=55) Toluene: 240 (n=55) Ethylbenzene: 240 (n=55) Xylenes: 620 (n=55) Naphthalene: 236 (n=32)	Qa	None	No	VRP	VRP	Well completed in 1974. No documented stimulation but completion record not reviewed by WOGCC (2014). Production record from 1983 with 9 bbls produced water in 1986. No description of where produced water was disposed. Increased to 222 bbls after 2004. Sundry notice for offsite disposal of production fluids in Jan 1998. Encana evaluating alternatives for final remedy and ground water monitoring.
42X-12	Invert	Yes ^U	Yes	Yes	5	GRO: ND (n=5) DRO: 1,100 (n=5) BTEX: ND (n=1)	~280	2,500	0	Not sampled	Qa	None	No	Yes	No	Completed in 1974. Acid stimulation in 1974. No description of where flowback and production fluids were disposed. Production record from 1983. No produced water until 2004 after which 295 bbls produced. Sundry notice for offsite disposal of production fluids in Jan 1998.
31X-14	Invert	Yes ^U	Yes	?	6	TPH: ND (n=5) (confirmation sample)	~260	2,500	0	Not sampled	Qa	PGDW34 (31m,518m,S) P44255.0W (69m,148m,N) P41320.0W (31m,148m,N) P99671.0W (17m,148,N)	No	?	?	Well completion in 1974. No documented stimulation. Production records from 1983 with 6,546 bbls water in Feb 1985, 4 bbls in 1986 and 4 bbls in 1988. No description of where produced water was disposed. After 2007, 7,691 cumulative bbls water. Sundry notice for offsite disposal of production fluids in Jan 1998. Further investigation recommend by WOGCC pending review of pre-excavation samples.
CCD	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Qa	Converted to 9441.0P (177m,45m,W)	No	NI	No	Well completion and P&A after completion in 1974. Stimulation or production unlikely. No evidence of converted well sampled.
TR1-22	Invert	Yes ^U	Yes	Yes	0	Not sampled	0		0	Not sampled	Qa	PGDW48 (116m,397m,NW) PGDW35 (88m,449m,NW)	No	NI	Yes	Well completion in 1976. Acid stimulation and hydraulic fracturing in 1980. No description of where flowback and production fluids were disposed. P&A 1986. Well production file starts in 1978 with 5,281 bbls produced water between 1978 and 1986
1-21	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Qa	None	No	NI	No	Well completion and P&A in 1976. Stimulation or production unlikely. Investigation recommended by WOGCC pending confirmation of nearby domestic wells. No evidence of former well pad – no further investigation recommended (Encana 2015)

Production Well Abbreviation	Drilling Mud Used Below Surface Casing	Pit Used or Likely Used to Dispose Drilling Mud and Cuttings Onsite	Pit Used or Likely Used for Disposal of Production Fluids?	Stimulated Prior to Jan 1995?	Number of Soil Screening Locations	Maximum Soil Contamination (ng/kg) and Number of Soil Samples	Excavation Volume (y.d ² )	Ecxeavation Criterion mg/kg TPH)	Number of Ground-Water Sampling Locations	Maximum Ground-Water Contamination in Surficial Deposits (ugl) and Number of Ground-Water Samples	Surficial Geology	Domestic Wells Within 600 m of Production Wells (Depth, Distance, Direction from Production well)	Stimulation Record Reviewed by WOGCC (2014)	Adequate Site Assessment as Indged by WOGCC (2015)	Further Investigation Recommended by WOGCC (2015)	Comments
TP I	Invert	Yes ^U	Yes	?	0	Not sampled	0		0	Not sampled	Qa	None	No	NI *	No	Well completion in 1976. P&A date unknown. No record of stimulation. Well production file starts in 1978 with 5,607 bbls produced water from 1978 to 1980. No description of where produced water was disposed.
1-31	Invert	Yes ^U	Yes	?	0	Not sampled	0		0	Not sampled	?	PGDW06 (116m,341m,SE) PGDW12 (116m,491m,NW)	No	NI	No	Well completion in 1976. P&A in 1977. Well completion report not available.
TU 1	Invert	Yes ^u	Yes	?	0	Not sampled	0		0	Not sampled	Qa	None	No	NI	No	Completed in 1976. P&A in 1982. No record of stimulation but completion record not reviewed by WOGCC (2014). Well production file starts in 1978 with 220 bbls produced water from 1978 to 1982. No description of where produced water was disposed. Encana (2015) states that there is no evidence of former well pad.
4-8	Invert	Yes ^U	Yes	Yes	6	GRO: ND (n=6) DRO: 32 (n=6) Naphthalene: 5.3 (n=3)	0	1,000	2	GRO: 5,200 (n=2) DRO: 13,000 (n=2) Benzene: 110 (n=2) Toluene: 250 (n=2) Ethylbenzene: 240 (n=2) Xylenes: 1,200 (n=2) Naphthalene: 72 (n=2)	Qa	PGDW41 (21m,421m,SE) P66345.0W (21m,407m,SE)	Yes	VRP	VRP	Well completed in Mar 1977. Hydraulic fracturing in 1977 with "gel water" and N ₂ . No description of where flowback and production fluids were disposed. Production file starts in Jan 1978 with 36,978 bbls water from Jan 1978 to Dec 1993. No description of where produced water was disposed. Encana (2015) drafting report for site closure.
34-13	Invert	Yes ^U	Yes	?	0	Not sampled	0		0	Not sampled	?	P197335.0W (?,632m,SE) P197336.0W (?,626m,SE)	No	NI	No	Well completion in 1977. P&A date unknown. Well production file starts in 1978 with 290 bbls produced water from 1978 to 1979. No description of where produced water was disposed.
T24-11	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Twdr	None	No	NI	No	Well completed and P&A in 1978. Stimulation or production unlikely.
24-4	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Qa	None	No	NI	No	Well completed and P&A in 1978. Stimulation or production unlikely.
44-15	Invert	Yes ^U	Yes	Yes	6	TPH: 486 (n=1)	0	5,500	0	Not sampled	Qa	PGDW48 (116m,329m,SW) PGDW35 (88m,374m,W) P108128.0W (116m,115m,W) P146856.0W (116m,115m,W)	No	No	Yes	Well completed in 1978. Acid stimulation in 1976 and 1978 with HCl and KCl solutions. No description of where flowback and production fluids were disposed. Production file starts in 1983. No produced water production from 1983 to 2005. Sundry notice for offsite disposal of production fluids in Jan 1998.
21-11	Invert	Yes ^U	Yes	Yes	?	Sample results not available in pit report (WOGCC 2015) or online.	~100	1,000	?	Sample results not available in pit report (WOGCC 2015) or online.	Qa	PGDW26 (20m,229m,W)	No	VRP	VRP	Well completed 1n 1979. Acid stimulation in 1979 with HCl solution and additives. Hydraulic fracturing in 1979 with HCl solution and additives. Hydraulic fracturing in 1979 with "YE4PSD" fluid. No description of where flowback and production fluids were disposed. Production file starts in 1983. No produced water until 2005. Sundry notice for offsite disposal of production fluids in Jan 1998. Soil and ground water sampling data not available. Ground water and additional soil data were collected in October 2014. Encana (2015) is preparing a Supplemental Site Characterization report to recommend site closure.

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12-13	Invert	Yes ^U	Yes	Yes	4	GRO: ND (n=4) DRO: ND (n=4) BTEX: ND (n=1)	0	1,000	0	Not sampled	Qa	PGDW32 (206m,173m,NE) PGDW33 (9m,134m,S) P22662.0P (9m,135m, S) P22660.0P (53m,280m,N)	Yes	No	Yes	Well completed in 1979. Acid stimulation with HCl and KCl solution in 1979. Hydraulic fracturing with "versa gel" in 1981. No description of where flowback and production fluids were disposed. P&A in 2001. Production records from 1983 with 18 bbls produced water between1986-1989. No description of where produced water was disposed. Sundry notice for offsite disposal of production fluids in Jan 1998.
41-9	Invert	Yes ^U	Yes	Yes	13	TPH: 3700 (n=8)	~1,200	4,000	0	Not sampled	Qa	PGDW43 (?,176m,NW)	No	No	Yes	Well completion in 1979. Acid stimulationwith HCl, KCl solution and additives in 1979 "flowed to pit." No produced water production until 1999 after which 15,593 bbls produced most of which was after recompletion in 2004. Sundry notice for offsite disposal of production fluids in Jan 1998.
TU 2	Invert	Yes ^U	Yes	Yes	0	Not sampled	0		0	Not sampled	Qa	P24502.0P (55m,466m.NE)	No	NI	No	Well completion, acid stimulation, and P&A in 1979.  No description of where flowback was disposed.
22-10	Invert	Yes ^U	Yes	Yes	6	TPH: 201 (n=1)	0	7,000	0	Not sampled	Qa	PGDW14 (58m,399m,E) PGDW44 (229m,508m,E)	Yes	No	Yes	Well completion in 1979. Acid stimulation using HCl and KCl solutions with additives in 1979. "Flowed to pit." Production record from 1983. No produced water until after recompletion in 2005. Sundry notice for offsite disposal of production fluids in Jan 1998.
G1	invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled		PGDW15 (31m,469m,NE) PGDW13 (?,488m,NW)	No	NI	No	Well completion and P&A in 1979. Stimulation or production unlikely.
21-15	Invert	Yes ^U	Yes	Yes	7	GRO: 76 (n=1) DRO: 401 (n=1)	0	8,500	0	Not sampled	Twdr	PGDW47 (148m,350m,N) P120049.0W (148m,384m,N)	Yes	?	?	Well completion in 1979. Acid stimulation with additives in 1979 and 1982. "Flw'd to pit" Hydraulic fracturing with "Y-F4PSD" "Flow to pit" in 1979. In letter to BLM dated 8/14/2012 concerning of 1,000 gallons of a 15% HCl solution in "compromised" casing between 735 to 1,105 feet below ground surface. Production records from 1983. No produced water until 2008. Sundry notice for offsite disposal of production fluids in Jan 1998. Further investigation dependent upon consideration of domestic wells.
44-10	Invert	Yes ^U	Yes	Yes	10	TPH: 2920 (n=6)	~60	5,500	0	Not sampled	Qa	PGDW23 (53m,253m,N) PGDW11 (107m,388m, S) P200885.0W (7,199m, E) P24508.0P (53m,306m, N)	No	No	Yes	Invert mud 15-20% water. Well completed in 1979. Acid stimulation in 1979. "Flowing to pit avg 4 bpmbled well to pit" Production records from 1983 with 10 bbls water in 1986. No description of where produced water was disposed. Sundry notice for offsite disposal of production fluids in Jan 1998.
22-12	Invert	Yes ^U	Yes	Yes	8	GRO: 120 (n=9) DRO 850 (n=9) BTEX: ND (n=1)	~40-60	1,000	5	GRO: 2,900 (n=5) DRO: 3,500 (n=5) Benzene: ND (n=5) Toluene: ND (n=5) Ethylbenzene: 120 (n=5) Xylenes: 610 (n=5)	Qa	PGDW20 (140m,172m, SE) LD02 (186m,172m, SE)	Yes	VRP	VRP	Well completion 1980. In 1979 and 1980, acid stimulation with HCl solution and additives. In 1980, hydraulic fracturing with "Titan III-30 gel" and B-11 gel breaker" flushed with 2% KCl solution. No description of where flowback and production fluids were disposed. No produced water until 1995 after which 288 bbls produced. No description of where produced water was disposed. Sundry notice for offsite disposal of production fluids in Jan 1998. Encana (2015) continuing ground water monitoring.
11-14	Invert	Yes ^U	Yes	Yes	5	TPH: 16 (n=5)	0	4,000	0	Not sampled	Qa	P29496.0P (40m,164m, E) P91293.0W (3m,254m, W)	No	No	Yes	Well completion in 1980. Acid stimulation in 1980. No description of where flowback and production fluids were disposed. Production record from 1983. No produced water until 2004 after which 12,722 bbls water produced. Sundry notice for offsite disposal of production fluids in Jan 1998.
16-28	KCl Polymer	Yes ^U	No	?	0	Not sampled	0		0	Not sampled	?	None	No	NI	No	Well completion in 1980. P&A date unknown. Well completion report not available.

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F I-17	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Qa	P95171.0W (26m,404m,W) P65111.0W (27m,404m,W)	No	NI	Yes	Well completion and P&A in 1980. Stimulation or production unlikely. Recommendation pending confirmation of presence of nearby domestic wells (WOGCC 2015).
14-2	Invert	Yes ^U	Yes	Yes	?	Sample results not in pit report (WOGCC 2015) nor posted online.	~50	1,000	?	Sample results not in pit report (WOGCC 2015) nor posted online.	Qa	PGDW05 (64m,299m,SE) PGDW45 (31m,272m,SE) PGDW40 (67m,357m,NW)	Yes	VRP	VRP	Well completion in 1981. On 1/18/1981, "operator noticed large gas flow from SI wellflow was from partially opened valve on 8 5/8 x 5 ½ in annuluslaid line to pit + started flowing to pitCirc 180 bblsgel salt waterin annuluscirc fluid to pittop of cntt very poor." Acid stimulation in 1981 using HCl and KCl solutions. On 3/11/1981, "well flowing to pitapprox. 500 bbls wtr." On 3/26/1981 "reversed acid to pit." Hydraulic fracturing in 1981 using "YF4PSD, gelled water, J-347 gelling agent, J-218 breaker, J-218 breaker, J-318 breaker aid" and other additives. "Swabbed to pit" On 4/6/1981. "Well producing approx. 75 bbls wtr per daywell died to wtr build up." On 2/23/1983, surface damages paid for "inverted mud blow out" on 1/18/1981 and "condensate blow out" in Oct 1982. No produced water documented until 2005. Sundry notice for offsite disposal of production fluids in Jan 1998. Pit was reinstated into the VRP program in July 2014. Soil borings and groundwater monitoring wells installed in October 2014. Encana is drafting a report recommending site closure.
1-8-1B	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Twdr	None	No	NI	No	Well completion and P&A in 1981. Well completion report not available. Stimulation or production unlikely.
21-9	Invert	Yes ^U	Yes	Yes	47	GRO: 700 (n=67) DRO: 39,000 (n=67) Benzene: ND (n=49) Toluene: 0.094 (n=47) Ethylbenzene: 2.4 (n=47) Xylenes: 20 (n=47)	~8,522	1,000	4	GRO: ND (n=4) DRO: 880 (n=4) BTEX: ND (n=4)	Qa	PGDW42 (61m,237m,SE)		Yes	No	Well completion in 1981. Acid stimulation in 1981. Hydraulic fracturing in 1981 using "gelled water." P&A in 1992. 11 bbls produced water in 1986. No description of where flowback and production fluids were disposed.
12-3	Invert	Yes ^U	Yes	Yes	5	TPH: 161 (n=5)	0	5,000	0	Not sampled	Qa	P66345.0W (21m,327m,S) PGDW41 (21m,524m,SW)	No	?	?	Acid stimulation in 1981. No description of where flowback and production fluids were disposed. Sundry notice for offsite disposal of production fluids in Jan 1998. No produced water until 2005 after which 1,270 bbls produced. Incorrect site photo and borehole logs in investigative report. Recommendation for additional investigation will be based upon file review.
RH I	Invert	Yes ^U	No	No	0	Not sampled	0		0	Not sampled	Qa	PGDW03 (137m,382m,SE) PGDW04 (134m,521m,SE) P120203.0W (137m,377m,S) P23056.0P (116m,377m,S)	No	NI	Yes	Well completion and P&A in 1981. Well completion report not available. Stimulation or production unlikely.
1-4	Invert	Yes ^U	Yes	Yes	0	Not sampled	0		0	Not sampled	Qa	None	No	NI	No	Acid stimulation and hydraulic fracturing during well completion in 1982. No description of where flowback and production fluids were disposed. Also, 2,867 bbls produced water by Jan 1993 and 4,124 bbls produced water by Jan 1998. No description of where produced water was disposed.
14-24	KCl Polymer	Yes ^U	Yes	Yes	0	Not sampled	0		0	Not sampled	Twdr	None755m,SW)	No	NI	No	Well completion and P&A in 1982. Acid stimulation in 1982. No description of where flowback and production fluids were disposed.

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A-1	Invert	Yes ^U	Yes	Yes	0	Not sampled	0		0	Not sampled	?	None	No	NI	No	Well completed in 1983. Acid stimulation and hydraulic fracturing in 1983. No description of where flowback and production fluids were disposed. Also, 7,072 bbls produced water from 1991 to 1995. No description of where produced water was disposed.
1-15	Invert	Yes ^U	Yes	Yes	0	Not sampled	0		0	Not sampled	Qa	None	No	NI	No	Well completion 1983. Acid stimulation and hydraulic fracturing with KCl solution and "gel water" in Cody Formation in 1983. P&A in 1990. 19 bbls produced water in 1983. No description of where flowback, produced water, and other production fluids were disposed
B-1	Invert	Yes ^U	Yes	Yes	0	Not sampled	0		0	Not sampled	?	None	No	NI	No	Well completion and P&A in 1984. Acid stimulation in 1984 with HCl and HF solutions. Hydraulic fracturing in 1984 with undiluted diesel fuel. No description of where flowback was disposed.
33-11	KCl polymer	Yes ^L	No	Yes	0	Multiple locations ^w	0		0	Not sampled	Qa	Not evaluated	No	NI	No	Well completion in 1993. Drilling mud samples up 27,000 mg/l Cl. Acid stimulation in 1993. Hydraulic fracturing in 1993 using CO ₂ foam. 1,442 bbls produced water by Jan 1998. No description of where flowback, produced water, and other potential production fluids were disposed. Sundry notice for offsite disposal of production fluids in Jan 1998. Encana states that cuttings were buried at offsite location north of a rock out crop near Tribal Pavillion 42X-11. A nearby monitoring well 5 showed no indication of contamination.
12-11	KCl polymer	Yes ^L	No	Yes	0	Multiple locations ^w	0		0	Not sampled	Qa	Not evaluated	Yes	NI	No	Well completion in 1993. Drilling mud up to 22,000 mg/l Cl. Hydraulic fracturing with CO ₂ foam and KCl solution in 1993. No description of where flowback was disposed. No produced water until recompletion in 2004. Sundry notice for offsite disposal of production fluids in Jan 1998. Investigation recommended by WOGCC at one pit containing KCl polymer.
11-10	KCl polymer	Yes ^L	No	No	0	Multiple locations ^W	0		0	Not sampled	Qa	Not evaluated	No	NI	No	Well completion in 1993. No apparent stimulation prior to recompletion in 2004. 5,508 bbl produced water from Jan 1994 – Jan 1998. No description of where produced water was disposed. Sundry notice for offsite disposal of production fluids in Jan 1998. Encana states that although a concrete pad is at this location, there is no documentation that it was used.
42-10	KCl polymer	Yes ^L	No	Yes	0	Multiple locations ^W	0		0	Not sampled	Qa	Not evaluated	Yes	NI	No	Well completion in 1994. Acid stimulation in 1994. 3,025 bbl produced water from Jan 1994 – Jan 1998. No description of where flowback and produced water were disposed. Sundry notice for offsite disposal of production fluids in Jan 1998. Investigation recommended by WOGCC at one pit containing KCl polymer.
31-10	KCl polymer	Yes ^C	No	Yes	0	Multiple locations ^w	0		0	Not sampled	?	Not evaluated	Yes	NI	No	Well completion in 1994. Acid stimulation in 1994. 3,850 bbls produced water from Jan 1994 – Jan 1998. No description of where flowback and produced water were disposed. Sundry notice for offsite disposal of production fluids in Jan 1998.

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1000000	Below	Pit Used or Likely Used to Pippose Drilling Mud and Cuttings Onsite	Pit Used or Likely Used for Disposal of Production Fluids?	Jan	of Soil Screening	(mg/kg) a Samples	.xcavation Volume (yd²)	5	of Ground-Water g Locations	Maximum Ground-Water Contamination in Surficial Deposits (1921) and Number of Ground-Water Samples		Domestic Wells Within 600 m of Production Wells (Depth, Distance, Direction from Production well)	Stimulation Record Reviewed by WOGCC (2014)	Adequate Site Assessment a Indged by WOGCC (2015)	Further Investigation Recommended by WOGCC (2015)	
=	Used	kely l ng Mi ie	kely   oduci	itimulated Prior to Jan 1995?	Scr	1 (mg	olume	Ecxcavation Criterion (mg/kg TPH)	umber of Ground ampling Locations	ound- and and ster S	São.	S Wil	ECOLI VOG	Asse	figati 1 by V	
Production Well Abbreviation	Drilling Mud Surface Casin	or Li Onsi	124	d Pr	of Soi	m Soil ination ( of Soil )	on Ve	O (Ha	5.0	n Grantio	urficial Geology	Well Stion Dire	on R	Site	nves	
luctic revia	ing A	sed ose I	sed osal	. allate	umber o	Maximum (Contamina	vatic	avat Kg T	umber ( ampling	rimes sits one mor	夏	oduc ince,	ulati	puate ed by	her I	<b>D</b>
Prod	Surf	Pit L Disp Cutt		Stim 1995		Max	Ехса	Ecxc (mg/	N Sell	Max Control of G	<u> </u>	Dom Dist.	Stim	Adec Judg	Furt Reco	<u> </u>
23-10	KCl polymer	165	No	Yes	0	Multiple locations ^w	0		0	Not sampled	Twdr	Not evaluated	Yes	NI	No	Well completion in 1994. Acid stimulation and hydraulic fracturing with N ₂ foam in 1994. No description of where flowback was disposed. 23,700 bbls produced water from Jan 1994 – Jan 1998. Sundry notice dated 4/27/1995 requesting approval to store produced water in a 210 bbl steel tank for offsite disposal. Sundry notice for offsite disposal of prod fluids in Jan 1998. Investigation recommended by WOGCC at one pit containing KCl polymer
43-10	KCl polymer	Yes ^L	No	Yes	0	Multiple locations ^w	0		0	Not sampled	Qa	Not evaluated	Yes	NI	No	Well completion in 1994. Mud pit sample 9,500 mg/l Cl. Acid stimulation and hydraulic fracturing using N ₂ foam in 1994. 85 bbls produced water in 1995. No description of where flowback and produced water were disposed. Sundry notice for offsite disposal of production fluids in Jan 1998. Part of cuttings pit
		4														exposed due to movement of landowner road.
33-2	KCl polymer	Yes ^C	No	Yes	0	Multiple locations ^w	0		0	Not sampled	?	Not evaluated	No	NI	No	Acid stimulation in 1994. 269 bbl produced water Jan 1994 – Jan 1998. No description of where flowback and produced water was disposed. Sundry notice for offsite disposal of production fluids in Jan 1998.
23-1	KCl polymer	Yes ^L	No	Yes	0	Multiple locations ^w	0		0	Not sampled	Twdr	Not evaluated	No	NI	No	Mud pit sample 36,360 mg/l Cl. Acid stimulation in 1994. 200 bbl produced water from Jan 1994—Jan 1998. Sundry notice dated 4/27/1995 to store produced water in 70 bbl steel tank for offsite disposal. Sundry notice for offsite disposal of production fluids in Jan 1998 – unclear how production fluids were disposed of prior to this date. Investigation recommended by WOGCC at one pit containing KCl polymer
41-15	KCl Polymer	Yes ^c	No	Yes	0	Multiple locations ^w	0		0	Not sampled	?	Not evaluated	No	NI	No	Mud pit sample 35,150 mg/l Cl. Acid stimulation and hydraulic fracturing using N ₂ foam in 1994. "Let well open to test tank" Sundry notice for offsite disposal of production fluids in Jan 1998 – unclear how production fluids were disposed of prior to this date. Completion record not reviewed by WOGCC (2014).
43-6	KCl Polymer	?	No	Yes	0	Multiple locations ^W	0		0	Not sampled	?	Not evaluated	No	NI	No	Acid stimulation in 1995. No produced water until 2008. Sundry notice for offsite disposal of production fluids in Jan 1998 – unclear how production fluids were disposed of prior to this date.
23-11	KCl polymer	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
31-11X 13X-3	KCl polymer PHPA/LSND	? No	No No	No NA	0 NA	Multiple locations ^W NA	0 NA		0 NA	Not sampled NA	? NA	Not evaluated NA	NA NA	NI NA	No NA	No well site disposal of production fluids.  NA
42X-9	LSND	Yes ^L	No	No	0	Multiple locations ^W	0		0	Not sampled	Qa	Not evaluated	NA NA	NI	No	No well site disposal of production fluids.
41-11	LSND	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA Î
33-10	PHPA/LSND	?	No	No	0	Multiple locations ^W	0		0	Not sampled	?	Not evaluated	NA	NI	No	No well site disposal of production fluids.
33-3 44-3	PHPA/LSND	Yes ^L Yes ^L	No No	No No	0	Multiple locations ^W Multiple locations ^W	0		0	Not sampled	Qa Qa	Not evaluated  Not evaluated	NA NA	NI NI	No No	No well site disposal of production fluids.  No well site disposal of production fluids.
15-21X	Invert	?	No	No	0	Not sampled	0		0	Not sampled Not sampled	Qa	Not evaluated  Not evaluated	NA NA	NI	No	No well site disposal of production fluids. Disposal of "solidified" invert mud and cuttings unknown. Encara states that cuttings were "solidified"
32-10	LSND	Yes ^L	No	No	0	Multiple locations ^W	0		0	Not sampled	Qa	Not evaluated	NA	NI	No	No well site disposal of production fluids.
13-11	PHPA	Yes ^C	No	No	0	Multiple locations ^W	0		0	Not sampled	?	Not evaluated	NA	NI	No	No well site disposal of production fluids.
21-13	DeepDrill®	Yes ^C	No	No	0	Multiple locations ^W	0		0	Not sampled	?	Not evaluated	NA	NI	No	No well site disposal of production fluids.
43-2	Unknown ^R	Yes ^C	No	No	0	Multiple locations ^W	0		0	Not sampled	?	Not evaluated	NA	NI	No	No well site disposal of production fluids.
13-2	DeepDrill®	Yes ^C	No No	No	0 N/A	Multiple locations ^W	0		0	Not sampled	? N/A	Not evaluated	NA NA	NI NA	No	No well site disposal of production fluids.
24-1 32-1	LSND LSND	No Yes ^L	No No	NA No	NA 0	NA Multiple locations ^W	NA 0		NA 0	NA Not sampled	NA Twdr	NA Not evaluated	NA NA	NA NI	NA No	NA  No well site disposal of production fluids.
34-2	LSND	Yes ^C	No	No	0	Multiple locations ^W	0		0	Not sampled Not sampled	?	Not evaluated  Not evaluated	NA NA	NI	No	No well site disposal of production fluids.
12-6	DeepDrill	?	No	No	0	Multiple locations ^W	0		0	Not sampled	?	Not evaluated	NA	NI	No	No well site disposal of production fluids.
44-1	LSND	Yes ^L	No	No	0	Multiple locations ^W	0		0	Not sampled	Twdr	Not evaluated	NA	NI	No	No well site disposal of production fluids.
14-10	DeepDrill®	?	No	No	0	Multiple locations ^W	0		0	Not sampled	?	Not evaluated	NA	NI	No	No well site disposal of production fluids.

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1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5	=	sed Be	cely Use	cety Use	or to Jan	Screening	(mg/kg)   Samples	lume (y	riterion	ound-W fions	und-W in Suri and Nu ter San	<u>ā</u>	With Nells (1	Cord	Assessin GCC (2	igation by WO	
1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5	8 We	and I.	###	3.5	Ë		Soll Soll Soll Soll Soll Soll Soll Soll	. Vø	n C. H)	- 5 e	Gro from (g/1) Wa	olos	Vell ion J irec	2 K	¥e.   ≪o	vest	
1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5	ition	N G G	5 t C	55	ated	P E		Hion	atio TP	r of ng l	S (p. m.	9 8	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	e di	e e e	r In	ents
1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5	oduc bre	# Se	l as of ill	T See	1 63			EA ES	kcav g/kg	di di	nitar post Gro	igi	a g f f g	view II	n die c	rthe com	<b>a</b>
1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5	Pr. Ab					<i>L</i> =	202	0.00	Ec:	Sar		III.S	8588	Sti.			<b>D</b>
1-11   Fig.   Vegl.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.			Yes							Ů		?	Not evaluated		Yes		
11   17   17   17   17   17   17   17			Yes ^C									2			Yes ^C		
18-10   18-10   19-20   18-10   19-20   18-10   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-20   19-2																	
1941   Top   Yes   No	12-5	PHPA	?	No	No	0	Multiple locations ^W	0		0	Not sampled	?	Not evaluated	NA	?	No	No well site disposal of production fluids.
1850   Yef   No   No   Modified leastness   0   0   Not sampled   Tough   Not excluded   NA   Yef   No   No   No   well and classes and production fluids.												?					
13-10   18-80   Yes   No						$\overline{}$	*								Yesc		* *
21-19   LSSD						-				0		1 War			Yes ^C		
Fig.   PRPA										0		?					
13-19   18-80			Yes ^L			0		0		0		Twdr	Not evaluated		?		
13-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-15   18-1												Twdr			?		
23-12   END												?					
44-2    7										NA 0		NA 2					
1.50		2	2							0		2			2		
1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800   1800		LSND	Yes ^L			_		,	1,000	0		Qa		_	?		
1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5			1				SVOC: ND (n=1)		·								-
21-12   ISSD   Yes   No   No   P. Multiple locations   0   0   Not sampled   Qu   Not evaluated   NA   ? No   No well site disposal of production fluids.										0			(107m,436m SE)		?		production fluid.
17-10   LSND							*	ů		0					?		* *
12-1						_						Qa ?			YesC		
122-1   LSND   Yes   No   No   0   Multiple locations   0   0   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not sampled   Two   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   Not   No										Ů		Twdr			?		* *
33-10W   LSND							*			0					?		
41-3	22-1	LSND	Yes ^L	No	No	0	Multiple locations ^W	0		0	Not sampled	Twdr	Not evaluated	NA	?	No	No well site disposal of production fluids.
22-11													NA		NA		
43-11   LSND										·			NA		? Nt a		
11-3																	
41-10																	
13-12   W PHPA																	
11-11B   LSND																	
31-11																	
23-3   7						_											
32-11		LSND								,		i					* *
44-11		LSND															
42-9W																	
32-10B																	
13-11B																	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$																	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						_				NA 0					NA 2		
23-10C										0		_			2		
34-3B															?		
23-10BLSNDYes!NoNo0Multiple locations W 00Not sampledTwdrNot evaluatedNA?NoNo well site disposal of production fluids.33-10BLSNDYes!NoNo0Multiple locations W 00Not sampledTwdrNot evaluatedNA?NoNo well site disposal of production fluids.12-11BLSNDNoNoNANANANANANANANANANANANA43-10BLSNDYes!NoNo0Multiple locations W 00Not sampledQaNANANANANA24-11LSNDNo D NoNANANANANANANANANA31-10BLSNDNo D NoNANANANANANANANANA	34-3B		No			NA	-	NA		NA	•				NA	NA	NA
33-10B															NA		
12-11B															?		1 1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							*				•				? NIA		
24-11         LSND         No         No         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA         NA <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>IVA</td><td></td><td>2</td><td></td><td></td></t<>													IVA		2		
31-10B LSND No ^D No NA NA NA NA NA NA NA NA NA NA NA NA NA										-			NA		NA.		
	33-11B	"water based"	No	No	NA	NA		NA		NA		NA		NA	NA	NA	NA

Production Well Abbreviation	Drilling Mud Used Below Surface Casing	Pit Used or Likely Used to Dispose Drilling Mud and Cuttings Onsite	Pit Used or Likely Used for Disposal of Production Fluids?	Stimulated Prior to Jan 1995?	Number of Soil Screening Locations	Maximum Soil Contamination (mg/kg) and Number of Soil Samples	Excavation Volume (yd ² )	Ecxcavation Criterion (mg/kg TPH)	Number of Ground-Water Sampling Locations	Maximum Ground-Water Contamination in Surficial Deposits (ugi) and Number of Ground-Water Samples	Surficial Geology	Domestic Wells Within 600 m of Production Wells (Depth, Distance, Direction from Production well)	Stimulation Record Reviewed by WOGCC (2014)	Adequate Site Assessment as Judged by WOGCC (2015)	Further Investigation Recommended by WOGCC (2015)	Comments
44-11B	LSND	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
21-14	LSND	Yes ^L	No	No	0	Multiple locations ^W	0		0	Not sampled	Qa		NA	NI	No	No well site disposal of production fluids.
13-10	LSND	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
21-10B	"water based"	No ^D	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
43-11B	"water based"	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
42-10B	LSND	No ^D	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
22-11B	"water mud"	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
32-10C	LSND	No ^D	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
22-11C	LSND	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
44-4	LSND	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
12-12	"water based"	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
33-2C	LSND/PHPA	No	No	NA	NA	NA	NA	<u> </u>	NA	NA	NA	NA	NA	NA	NA	NA
13-2B	?	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
43-4	LSND	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
33-2B	LSND	No	No	NA	NA	NA	NA	<u> </u>	NA	NA	NA	NA	NA	NA	NA	NA
14-3B	DeepDrill®	No	No	NA	NA	NA	NA	<u> </u>	NA	NA	NA	NA	NA	NA	NA	NA
41-11B	?	No	No	NA	NA	NA	NA	<u> </u>	NA	NA	NA	NA	NA	NA	NA	NA
42-4B	LSND	No	No	NA	NA	NA	NA	<u> </u>	NA	NA	NA	NA	NA	NA	NA	NA
21-11B	LSND	No	No	NA	NA	NA	NA	<b>†</b>	NA	NA	NA	NA	NA	NA	NA	NA
13-3W	LSND	No	No	NA	NA	NA	NA	<b>†</b>	NA	NA	NA	NA	NA	NA	NA	NA
41-10B	LSND	No	No	NA	NA	NA	NA	<del>                                     </del>	NA	NA	NA	NA	NA	NA	NA	NA
34-28	DeepDrill®	?	No	No	0	Multiple locations ^W	0		0	Not sampled	?		NA	NI	No	No well site disposal of production fluids.
32-3	LSND	No	No	NA	NA	NA	NA	<u> </u>	NA	NA	NA	NA	NA	NA	NA	NA
43-9	DeepDrill®	No	No	NA	NA	NA	NA	<u> </u>	NA	NA	NA	NA	NA	NA	NA	NA
22-3	"water based"	No	No	NA	NA	NA	NA	<u> </u>	NA	NA	NA	NA	NA	NA	NA	NA
44-3C	?	No	No	NA	NA	NA	NA	<b>†</b>	NA	NA	NA	NA	NA	NA	NA	NA
32-2	"Gel-Chem"	No	No	NA	NA	NA	NA	†	NA	NA	NA	NA	NA	NA	NA	NA
33-12	"Gel-Chem"	No	No	NA	NA	NA	NA	t	NA	NA	NA	NA	NA	NA	NA	NA
14-21	KCL Polymer	Yes ^L	No	No	0	Multiple locations ^W	0		0	Not sampled	Twdr		NA	NI	No	Well completion in 2006. No well site disposal of production fluids. Investigation recommended by WOGCC at one pit containing KCl polymer
22-4	PHPA	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA
42-15	PHPA	Yes ^L	No	No	0	Multiple locations ^W	0		0	Not sampled	Qa	?	NA		No	No well site disposal of production fluids.
41-26	Water based	No	No	NA	NA	NA	NA		NA	NA	NA	NA	NA	NA	NA	NA

### Abbreviations

? – Unknown

VRP - Voluntary Remediation Program

PHPA - partially hydrolized polyacrylamides

LSND - low solids non-dispersed drilling mud

DeepDrill® is a product of Newpark Drilling Fluids and is described as a buffered blend of polyhydroxyl alcohols. No MSDS on this product was provided to EPA

ND – non detect (reporting limit in report)

NI – not investigated

Qa - Quaternary Deposits

Twdr - Wind River Formation

n – number of samples

NA – not applicable

#### Superscripts

- D Cuttings disposed at pit near 34-10
- C Cuttings used for tank berms/tank battery or spread on surface at location
- L Pits lined after 1993.
- U Pits unlined prior to 1993.
- W Cuttings for water-based mud sampled by Encana at 40 production wells between 2001 and 2006. All samples analyzed for TPH with highest TPH value of 645 mg/kg. Two samples were analyzed for chloride (115 and 215 mg/kg). Data set not available.

Table SI F3. Summary of detection of light hydrocarbons and organic compounds in domestic wells less than and greater than 600 m from unlined pits. Concentrations in  $\mu$ g/L unless otherwise indicated.

Well Name	Date	Methane	Ethane	Propane	GRO	DRO	DRO (SGCU)	Adamantane	1,3-Dimethyl Adamantane	Other Hydrocarbons and TICs .	References
					g production fl					1	20
PGDW05	Mar-09	16.6	NA	NA	NA	105	NA	NA	NA		EPA ²⁹
	Jan-10	5.44(J)	<10.0	<15.0	26.3/31.1	75.3/76.4	NA	<0.20(J)/<0.20(J)	1.74(J)/1.71(J)	2-methyladamantane (TIC) - 2.5 μg/L	EPA ³⁰
	Apr-11	90(B)	66(B)	<6.7	42.8(B)	68.1(B)	NA	0.12(J)	1.35(J)	1,3-dimethyladamantane + isomers (TIC) – 8.6 μg/L	EPA ³⁰ EPA ²⁷ EPA ³³
	Apr-12	53(B)	<0.27	<3.8	48	63.5	NA	<0.25	2.82	2-methyladamantane (TIC) – 3.39 μg/L cis-1,4-dimethyladamantane (TIC) – 1.37 μg/L	
	Jun-14	33	ND	ND	ND	ND	26(J)	NA	NA	isopropanol – $8.1(J)$ µg/L	WYDEQ ³⁴
	Aug-14	72	ND	ND	ND	93(J)	31(J)	NA	NA		WYDEQ ³⁴
PGDW06	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW11	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW14	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹ EPA ²⁷
	Apr-11	23(B)	<4.8	<6.7	<20.0	<20.8	NA	<0.10	< 0.10		EPA ²⁷
	Jun-14	0.54(J)	ND	ND	ND	29(J)	ND	NA	NA	isopropanol – 6.0(J) μg/L naphthalene – 0.6(J) μg/L	WYDEQ ³⁴
	Aug-14	0.2(J)	ND	ND	ND	ND	ND	NA	NA		WYDEQ ³⁴
PGDW20	Mar-09	137	NA	NA	<20	17.3	NA	NA	NA		EPA ²⁹
	Jan-10	172	10.9	<15.0	<20.0	21.7	NA	<0.20(J)	<0.20(J)	2-methyladamantane (TIC) - 0.49 μg/L	EPA ³⁰
	Oct-10	190(B)	20(B)	<4.1	<20.0/<20.0	<22.0	NA	1.35(J)/1.37(J)	0.14(J)/0.14(J)	2-methyladamantane (TIC) – 1.03/0.43 μg/L	EPA ²⁷
	Apr-11	137(B)	80(B)	<6.7	<20.0	<21.9	NA	< 0.10	< 0.10	1-isobutyladamantane (TIC) – 0.27 μg/L	EPA ²⁷
	Apr-12	111/108	8.0/7.0	<3.8/<3.8	<20.0/<20.0	<20.0/<20.0	NA	<0.25	<0.25/<0.25	2-methyladamantane (TIC) – 0.67 μg/L	EPA ³⁰ EPA ²⁷ EPA ²⁷ EPA ³³
	Jun-14	110	7	0.59(J)	ND	ND	ND	NA	NA	acetone – 1.8(J) μg/L	WYDEQ ³⁴
	Aug-14	130	8	0.24(J)	ND	43(J)	ND	NA	NA		WYDEQ ³⁴
PGDW20 (carbon trap)	Mar-09	NA	NA	NA	NA	377	NA	NA	NA		EPA ²⁹
PGDW20 (RO filter)	Jan-10	NA	NA	NA	NA	752,000 μg/kg	NA	420 μg/kg	2960 μg/kg	2-methyladamantane (TIC) – 9400 μg//kg	EPA ³⁰
LD-02	Oct-10	230(B)	. 20(B)	<4.1	<20.0	. 111	NA	0.510(J)	<0.25(J)	benzene $-0.060(J) \mu g/L$ ethylbenzene $-0.240(J) \mu g/L$ o-xylene $-0.260(J) \mu g/L$ $1,2,4$ -trimethylbenzene $-0.200(J) \mu g/L$ $1,3,5$ -trimethylbenzene $-0.210(J) \mu g/L$ isopropylbenzene $-0.350(J) \mu g/L$ methyl $tert$ -butyl ether $-0.140(J) \mu g/L$	EPA ²⁷
	Jun-14	18	0.2(J)	ND	ND	ND	ND	NA	NA		WYDEQ ³⁴
	Aug-14	12	0.43(J)	ND	ND	77(J)	ND	NA	NA	pyruvic Acid – 2060 μg/L	WYDEQ ³⁴
PGDW21	Mar-09	54.1	NA	NA	NA	NA	NA	NA	NA		EPA ²⁷
PGDW22	Mar-09	<5.00	NA	NA	<20	27.1	NA	<0.20(J)	<0.20(J)		EPA ²⁹
	Jan-10	<5.00	<10.0	<15.0	<20	154	NA	< 0.10	<0.10		EPA ³⁰
PGDW23	Mar-09	146	NA	NA	<20	<15.0	NA	NA	NA		EPA ²⁹
	Jan-10	149	<10.0	<15.0	<20	<20.0	NA	<0.20(J)	<0.20(J)		EPA ³⁰
	Apr-11	178(B)	<4.8	<6.7	<20.0	21.1(B)	NA	<0.10	<0.10	1	EPA ²⁷

Well Name	Date	Methane	Ethane	Propane	GRO	DRO	DRO (SGCU)	Adamantane	1,3-Dimethyl Adamantane	Other Hydrocarbon	References
	Apr-12	226	19	11.4	<20.0	<20.0	NA	<0.25	<0.25	<u> </u>	EPA ³³
	Jun-14	98	0.76(J)	ND	ND	21(J)	ND	NA	NA	beta-BHC – 0.06 (J) μg/L	
	Aug-14	210	0.77(J)	ND	ND	ND	ND	NA	NA		WYDEQ ³⁴ WYDEQ ³⁴
PGDW26	Mar-09	<5.00	NA	NA	NA	NA	NA	NA	NA		EDA 29
	Apr-11	27(B)	<4.8	<6.7	<20.0	47.2	NA NA	<0.10	<0.10		EPA ²⁹ EPA ²⁷
PGDW30	Mar-09	558	NA	NA	NA	46.8	NA	NA	NA		EPA 29
100	Jan-10	808	<10.0	<15.0	<20.0	35.0	NA	<0.20(J)	1.81(J)	1,3,5-trimethyladamantane (TIC) - 0.29 ug/L	EPA ²⁹ EPA ³⁰ EPA ²⁷
	Oct-10	760(B)	<3.0	<4.1	29.4	32.7	NA NA	<0.25	2.48	1,5,5 timethyladamantane (110) 0.25 ug/L	EDA 27
	Apr-11	644	76(B)	<6.7	21.6(B)	37.0	NA NA	<0.10	0.98	1 3-dimethyladamantane + isomers (TIC) - 3 96 µg/I	EDA 27
	Apr-12	384	3	<3.8	27.3	43.8	NA NA	<0.25	2.50	1,3-dimethyladamantane + isomers (TIC) - 3.96 μg/L 1,4-dimethyladamantane (TIC) – 2.33 μg/L	EPA ²⁷ EPA ³³
	Jun-14	720	0.39(J)	ND	ND ND	34(J)	21(J)	NA	NA NA	1,4-difficulty administratio (TiC) = 2.55 µg/L	EPA"
	Aug-14	1100	0.59(J) 0.61(J)	ND	ND	74(J)	ND	NA NA	NA NA		WYDEQ ³⁴
PGDW32		21.4		NA NA	NA NA	19.2	NA NA	NA NA	NA NA		WYDEQ ³⁴
PGDW32	Mar-09 Jan-10	36.3	NA <10.0	NA <15.0	22.6	<20.0	NA NA	0.30	O.20		EPA ²⁹
	Apr-11	67(B)	<10.0 <4.8	<15.0 <6.7	22.4(B)	<20.0 <20.9/<22	NA NA	0.30 0.12(J)/0.12(J)	<0.20	1-ethyl-4-methyl benzene (TIC) - 0.17 ug/L	EPA ²⁹
	Jun-14	33	0.2 (J)	0.2(J)	ND ND	ND	ND ND	NA NA	<0.10/<0.10 NA	isopropanol – 24 (J) μg/L isopropylbenzene – 0.1(J) μg/L tert-butyl alcohol – 2.0(J) μg/L	EPA ²⁵ EPA ²⁷ WYDEQ ³⁴
	Aug-14	68	ND	ND	ND	ND	ND	NA	- NA	gamma BHC (lindane) – 0.08(J) µg/L isopropylbenzene – 0.1(J) µg/L	WYDEQ ³⁴
PGDW33	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA	1 17 (715	EPA ²⁹
	Jun-14	0.44(J)	ND	ND	ND	ND	ND	NA	NA	2-butoxyethanol – 3300(J) μg/L isopropanol – 3.5(J) μg/L endosulfan II – 0.1(J) μg/L gamma BHC (lindane) – 0.1(J) μg/L	WYDEQ ³⁴
	Aug-14	0.3(J)	ND	ND	ND	ND	ND	NA	NA		WYDEQ ³⁴
PGDW34	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW35	Mar-09	21.6	NA	NA	NA	17.9	NA	NA	NA		EPA ²⁹
PGDW36	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW40	Jan-10	.98.9	<10.0	<15.0	<20.0	32.6	NA	<0.20	0.36		EPA ³⁰
PGDW41A	Jun-14	ND	ND	ND	ND	150(J)	ND	NA	NA	methylene chloride – 0.2(J) μg/L	WYDEQ ³⁴
PGDW41	Jan-10	<5.00	<10.0	<15.0	<20.0	479	NA	< 0.20	< 0.20		EPA ³⁰
	Apr-11	385	142(B)	<6.7	<20.0	132	NA	<0.25	<0.25	·	EPA ²⁷
	Jun-14	1.6(J)	0.2(J)	ND	ND	170(J)	180(J) N	<u> </u>	NA		WYDEQ ³⁴
	Aug-14	2.0(J)	ND	ND	ND	250(J)	230(J) N	<u> </u>	NA		WYDEQ ³⁴
PGDW42	Jan-10	60.0	<10.0	<15.0	<20.0	21.6	NA	<0.20(J)	<0.20(J)		EPA ³⁰
PGDW43	Jan-10	<5.00	<10.0	<15.0	<20.0	49.7	NA	<0.20	<0.20	benzene – 0.540 μg/L acenaphthylene – 0.210 μg/L naphthalene – 0.300 μg/L phenol – 0.170 μg/L	EPA ³⁰
PGDW44	Jan-10	<5.00	<10.0	<15.0	<20.0	44.3	NA	<0.20(J)	<0.20(J)	2-methylnaphthalene - 0.370(J) µg/L fluorene - 0.150(J) µg/L I-methyl naphthalene (TIC) - 0.33 µg/L 1,6-dimethyl naphthalene (TIC) - 0.42 µg/L 1,7-dimethyl naphthalene (TIC) - 0.48 µg/L 2,7-dimethyl naphthalene (TIC) - 0.25 µg/L	EPA ³⁰

Well Name	Date	Methane	Ethane	Propane	GRO	DRO	DRO (SGCU)	Adamantane	1,3-Dimethyl Adamantane	Other Hydrocarbons and TICs	References
	Apr-11	24(B)	<4.8	<6.7	<20.0	60.5(B)	NA	<0.25	<0.25		EPA ²⁷
	Jun-14	1.3(JP)	0.37(J)	0.51(J)	ND	31(J)	ND	NA	NA	isopropanol – l l (J)	WYDEQ ³⁴
		1.5(61)	0.57(0)	0.01(0)	1,5	31(0)				gamma BHC (lindane) – 0.02(J) naphthalene – 0.2(J)	WIDEQ
	Aug-14	1.4(J)	0.43(J)	0.59(J)		1	1	NA	NA		WYDEQ ³⁴
PGDW45	Jan-10	<5.00	<10.0	<15.0	<20.0	41.3	NA	<0.20(J)	<0.20(J)	1,3-dimethyladamantane + isomers – 9.5 μg/L	EPA ³⁰ EPA ²⁷
	Apr-11	24(B)	64(B)	<6.7	<20.0	32.1	NA	< 0.10	1.25	-	EPA ²⁷
	Jun-14	1(J)	ND	ND	25(J)	ND	33(J)	NA	NA	isopropanol – 15(J) μg/L gamma BHC (lindane) - 0.06(J) μg/L	WYDEQ ³⁴
PGDW46	Jan-10	<5.00	<10.0	<15.0	<20.0	25.5	NA	<0.20	<0.20	(	EPA ³⁰
PGDW47	Jan-10	<5.00	<10.0	<15.0	<20.0	26.6	NA	<0.20(J)	<0.20(J)		EPA ³⁰
PGDW48	Jan-10	<5.00	<10.0	<15.0	<20.0	<20.0	NA	<0.20	<0.20		EPA ³⁰
PGDW49	Jan-10	<5.00	<10.0	<15.0	<20.0	130	NA	<0.20	<0.20		EPA 30
1 32 12	Apr-11	24(B)	62(B)	<6.7	<20.0	51.9	NA NA	<0.10	<0.10	.+	EPA ³⁰ EPA ²⁷
	Jun-14	0.2(JP)	ND ND	ND ND	ND	110(J)	ND	NA	NA	and and a H 0 07/I) wall	EPA-
	_	0.2(JP) 0.3(JP)		ND ND	ND ND		ND	NA NA	NA NA	endosufan II – 0.07(J) μg/L	WYDEQ ³⁴
	Aug-14	0.3(JP)	ND	ND	ND	38(J)	ND	NA	NA		WYDEQ ³⁴
P108128.0W	NS										
P124049.0W P146856.0W	NS NS										
P197335.0W	NS				+						
P197336.0W	NS										
P200885.0W	NS										
P22660.0P	NS										
P22661.0P	NS										
P22662.0P P24502.0P	NS NS										
P24508.0P	NS				+	+					
P29496.0P	NS										
P31805.0W	NS										
P41320.0W	NS										
P41517.0W	NS										
P44255.0W P59499.0W	NS ·	<del></del>			1			1			
P60032.0W	NS NS							1			
P66345.0W	NS										
P69549.0W	NS										
P91293.0W	NS										
P99671.0W	NS							<u> </u>			
					luction Fluids	37.4	1 374	1 374	37.1		1 20
PGDW03	Mar-09	NA	NA	NA	NA	NA <20.0	NA	NA	NA		EPA ²⁹
	Jan-10	<5.00	<10.0	<15.0	<20.0		NA	<0.20	<0.20		EPA ³⁰
PGDW04	Mar-09 Jan-10	<5.00 <5.00	NA <10.0	NA <15.0	<20.0	<15.0 <20.0	NA NA	NA <0.20	NA <.020		EPA ²⁹ EPA ³⁰
PGDW13	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW15	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
P120203.0W	NS '	1 1 1	1411	I I I	1111	1111	1111	1111	1 1		EFA
P23056.0P	NS NS	+									

Well Name	Date	Methane	Ethane	Propane	GRO	DRO	DRO (SGCU)	Adamantane	1,3-Dimethyl Adamantane	Other Hydrocarbons and TICs	References
P65111.0W	NS										
P95171.0W	NS										
P9334.0P	NS										
P9441.0P	NS										
CR UW09/250											
		rom an Unlin		1	T	T	1	Laza	1.27		1 20
PGPW01	Mar-09	<5.00	NA	NA	NA	17.1	NA	NA	NA		EPA ²⁹
	Jan-10	NA	NA	NA	NA	<20.0	NA	< 0.20	<0.20		EPA ³⁰
PGPW02	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
	Jan-10	NA	NA	NA	NA	<20.0	NA	< 0.20	<0.20		EPA ³⁰
	Apr-12	8(B)	<2.7	<3.8	<20.0	<20.0	NA	< 0.25	<0.25		EPA ³³
PGDW01	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW02	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW09	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW10	Mar-09	<5.00	NA	NA	<20	23.1	NA	<0.20(J)	<0.20(J)		EPA ²⁹
	Jan-10	<5.00(J)	<10.0(J)	<15.0(J)	<20	<20.0	NA	<0.25	< 0.25		EPA ³⁰
PGDW12	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW16	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW17	Mar-09	10.6	NA	NA	NA	17.5	NA	NA	NA		EPA ²⁹
PGDW18	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW19	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW24	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW25	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		
	Jan-10	<5.00	<10.0	<15.0	<20	27.8	NA	<0.20	<0.20		EPA ²⁹ EPA ³⁰
PGDW28	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW29	Mar-09	<5.00	NA	NA	NA	16.2	NA	NA	NA		EPA ²⁹
PGDW31	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW37	Mar-09	NA	NA	NA	NA	NA	NA	NA	NA		EPA ²⁹
PGDW38	Mar-09	<5.00 •	·NA	NA ·	NA	19.7	NA	NA	NA		EPA ²⁹
PGDW39	Jan-10	<5.00	<10.0	<15.0	<20.0	30.0	NA	<0.20(J)	<0.20(J)		EPA ³⁰
PGDW50	Apr-12	<1.3	<2.7	<3.8	<20.0	<20.0	NA	<0.25	<0.25		EPA ³³
	1 *	1	1	1	1	1	1	1		1	1 22.11

Data (tables) from WYDEQ obtained from the Powder River Basin Resource Council in April 2015.

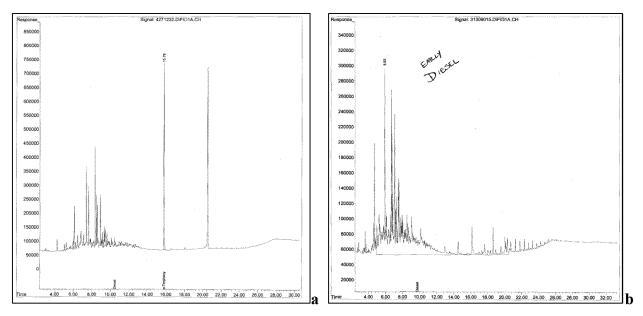
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NS – Not sampled NA – Not analyzed

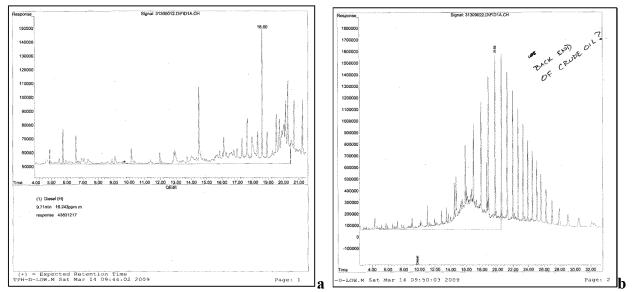
ND – Not detected. Method detection and reporting limits not known TICs – Tentatively identified compounds

J – Estimated value

B – Compound detection in blank. For EPA data, detection less than 10X value in blank. SGCU – Silica gel cleanup performed before analysis



**Figure SI F1.** Chromatograms of DRO analysis at (a) PGDW05 during Phase V sampling event, and (b) PGDW30 during Phase I sampling event. Handwritten note, "Early Diesel", by EPA Region 8 chemist.



**Figure SI F2.** Chromatograms of DRO analysis at PGDW20 during Phase I sampling event (a) aqueous sample (b) carbon trap sample. Handwritten note, "Back End of Crude Oil" by EPA Region 8 analytical chemist. During the Phase (I) sampling event, water was circulated through a carbon trap for 24 hours (cumulative water approximately 2,950 L) with detection of DRO at  $377 \mu g/L$  (EPA 200 9).

## G. Drilling Fluids Remaining in Wellbores

A review of well completion reports, drilling reports, and wireline geophysical logs indicates that invert mud consisted up to 79% oil (Unit 41X-10). At Govt 23-7, Q-BROXIN Gel, a ferrochrome lignosulfonate based gel¹⁰⁷ was used which contains high concentrations of chromium (e.g., > 16,000 mg/kg)¹⁰⁸. After 1993, water-based mud systems consisted of KCl polymer, partially hydrolized polyacrylamides (PHPA), low solids non-dispersed drilling mud (LSND), and "DeepDrill" drilling systems (Table SI C1). MSDSs indicate that "*NewPHPA*" contained 24% hydrotreated light petroleum distillate.

The contact length of drilling mud to the Wind River and Fort Union Formations was estimated by the difference in depth to surface casing and depth to top of primary cement outside production casing based on available information from cement bond logs (CBLs) and temperature logs. Production casing was not used for 16 "dry" exploration wells (no cement below surface casing with exception of plugs for abandonment) 14 of which were drilled using invert mud. CBLs were unavailable at 42 of 165 (25%) of production wells. Top of cement could not be discemed at 5 wells due to high and erratic amplitude readings characteristic of free pipe. The extent of drilling mud below casing could be estimated at 128 of 181 (71%) total production wells and at 36 of 58 (62%) of production wells where invert mud was used (Table SI C1). The elevation of surface casing and top of cement are illustrated in Figure SI F1.

Boreholes retaining drilling mud outside production casing represent vertical "line" source terms for mass flux of contaminants into a surrounding formation. However, a more complicated geometry occurs when mud is lost to a formation. For example at Tribal 1-21, invert mud was lost to the Wind River Formation at two depths (9.5 and 12.7 m³), with the latter "likely lost to a fractured zone." At USA Tribal 258 22-10, 39.7 m³ of invert mud was lost to the Fort Union Formation at two depths. Given the composition of invert mud, impact to ground water is expected but the distribution of impact would be expected to be a function of linear extent of mud below surface casing, surface area of exposure, dispersion, biodegradation, and distance (both vertical and lateral) from boreholes, and local hydraulic gradients. No monitoring wells exist in the immediate of boreholes, thus assessment of impact is not possible.

Ground water contamination from invert mud retained in boreholes would be expected to be primarily manifested by detection of elevated levels of diesel range organics (DRO). Fourteen domestic wells in the Pavillion Field were identified as having sufficient depth or proximity to production wells to be potentially impacted by invert mud retained in boreholes (Table SI G1). Twelve of these wells were sampled by EPA of which 9 were analyzed for DRO. Given distance to production well, depths of surface

casing and domestic wells, expected direction of ground water flow (east), and detection of elevated DRO, LD-02 appears to have the highest probability of impact with detection of DRO at 111  $\mu$ g/L. However, if DRO detection is due to an anthropogenic source term, differentiation from other source terms (unlined pits and stimulation) is not possible with currently available data.

Table SI G1. Domestic wells greater than intermediate depth and distance to nearest production well with invert mud

EPA/WY SEO Well Identification	Depth of Domestic Well (m bgs)	Nearby Production Well with Invert Mud	Direction from Production Well to Domestic Well	Distance (m)	Depth of Surface Casing (m bgs)	Depth of Surface Casing - Domestic Well (m)	Depth to Top of Primary Cement or Base of Borehole (m bgs)	Length of Invert Mud Below Surface Casing (m)	DRO (µg/L) except PGFM20 and EPa Phase
PGDW03	137.2	44-17	SE	427	183.8	46.6	None	1108	<20.0 (II)
		RH I	SE	382	185.9	48.7	None	1035	
PGDW04	134.1	44-17	SE	565	183.8	49.7	None	1108	<15.0 (I), < 20.0
		RH 1	SE	521	185.9	51.8	None	1035	(II)
PGDW06	115.8	1-31	SE	341	125.3	9.5	Unknown	Unknown	NA
PGDW11	unknown	44-10	NE	388	184.4	Unknown	585	585	NA
		31-15	SW	230	205.7	Unknown	Unknown	Unknown	
PGDW12	115.8	1-31	NW	491	125.3	9.5	Unknown	Unknown	NA
PGDW20	140.2	22-12	SE	172	178.6	38.4	Unknown†	Unknown	17.3 (I), 21.7 (II), <20/<20 (III), <21.9 (IV), < 20/<20 (V)
PGDW20	140.2	22-12	SE	172	178.6	38.4	Unknown†	Unknown	377 (I)
(Carbon Trap)									
PGFM20 (RO Filter sample from PGDW20)	140.2	22-12	SE	172	178.6	38.4	Unknown†	Unknown	752,000 (μg/kg) (II)
PGDW21/LD-02	185.9	22-12	SE	172	178.6	-7.3	Unknown†	Unknown	111 (III)
PGDW22	unknown	14-12	SW	261	190.1	Unknown	191	0.9	27.1 (I), 154 (II)
PGDW32	205.7	12-13	NE	173	175.6	-30.1	290	114	19.2 (I), <20.9/<22.0 (IV)
PGDW43	unknown	41-9	NW	176	184.1	Unknown	274	90	49.7 (II)
PGDW47	147.5	21-15	N	350	188.7	41.2	Unknown	Unknown	26.6 (II)
PGDW48	115.8	44-15	SW	329	189.9	74.1	198	8	<20.0J (II)
P108128.0W	115.5	44-15	W	115	189.9	74.4	198	8	NA
P124049.0W	147.5	21-15	N	384	188.7	41.2	Unknown	Unknown	NA

[†] Well schematic indicates drilling mud below surface casing.

# H – Summary of Analytical Data Sources

**Table SI H1.** Major reports summarizing data and/or data quality

Agency	Report Title	Date	Source (accessed 9/1/2015)
EPA	Site Inspection – Analytical Results Report Pavillion Area Groundwater Investigation Site, Pavillion, Fremont County, Wyoming	Aug 2009	http://www2.epa.gov/sites/production/files/documents/Pavillion_GWInvestigationARRTextAndMaps.pdf
EPA	U.S. Environmental Protection Agency (EPA 2010a). Expanded Site Investigation – Analytical Results Report Pavillion Area Groundwater Investigation, Fremont County, Wyoming	Aug 2010	http://www2.epa.gov/sites/production/files/documents/PavillionAnalyticalResultsReport.pdf
EPA	Pavillion Quality Assurance Project Plans (5 revisions)	Feb 2010	ftp://ftp.epa.gov/r8/pavilliondocs/QA Documents/QAPPs/
EPA	Audits of Data Quality (ADQ) October 2010 Sampling Event	Apr 2011	ftp://ftp.epa.gov/r8/pavilliondocs/QA Documents/Audits Of Data Quality Lab Results/Phase3/
EPA	Audits of Data Quality (ADQ) January 2010 Sampling Event	Aug 2011	ftp://ftp.epa.gov/r8/pavilliondocs/QA Documents/Audits Of Data Quality Lab Results/Phase2/ADQ-R8-PhaseII/
EPA	Audits of Data Quality (ADQ) March 2009 Sampling Event	Dec 2011	ftp://ftp.epa.gov/r8/pavilliondocs/QA Documents/Audits Of Data Quality Lab Results/Phase1/ADQ-R8-Phase1/
EPA	Audits of Data Quality (ADQ) April 2011 Sampling Event	Aug 2011	ftp://ftp.epa.gov/r8/pavilliondocs/QA Documents/Audits Of Data Quality Lab Results/Phase4/
EPA	Investigation of Ground Water Contamination near Pavillion, WY D		http://www2.epa.gov/region8/draft-investigation-ground-water-contamination-near-pavillion-wyoming
EPA	Investigation of Ground Water Contamination near Pavillion, Wyoming Phase V Sampling Event Summary of Methods and Results	Sep 2012	ftp://ftp.epa.gov/r8/pavilliondocs/phase5/PavillionSeptember2012Narrative.pdf
EPA	Groundwater Sampling Results at Locations near Pavillion, WY Pavillion Phase V (April 2012) Groundwater Quality Results and - Control (QC) Data	Sep 2012	ftp://ftp.epa.gov/r8/pavilliondocs/phase5/PavillionSeptember2012Appendices.pdf
USGS	Transmittal of Contract Laboratory Results and Evaluation of Laboratory-Specific Quality Control Measures, U.S. Environmental Protection Agency Monitoring Well MW02, Pavillion Wyoming 2012, Administrative Report Prepared for the U.S. Environmental Protection Agency. Director Approved August 30, 2012	Aug 2012	ftp://ftp.epa.gov/r8/pavilliondocs/phase5/USGS_MW02_AdministrativeReportSep2012.pdf
USGS	Sampling and Analysis Plan for the Characterization of Groundwater Quality in Two Monitoring Wells near Pavillion, WY	Sep 2012	http://pubs.usgs.gov/of/2012/1197/
USGS	Groundwater-Quality and Quality-Control Data for Two Monitoring Wells near Pavillion, Wyoming, April and May 2012	Sep 2012	http://pubs.usgs.gov/ds/718/
USGS	Analytical Report: Job Number: 280-28076-1 Job Description: EPA - Pavillion Fracking	Sep 2012	ftp://ftp.epa.gov/r8/pavilliondocs/phase5/Appendix9_J28076-1_EPA_Std_Tal_L4_Package_MiniFinalReport.pdf
EPA	Pavillion Gas Well Integrity Evaluation	Jul 23 2013	ftp://ftp.epa.gov/r8/pavilliondocs/OtherDocuments/WellAndFieldPitsEvaluationJuly2013/GasWellIntegrityEvaluation 25July2013Final.pdf
EPA	Pavillion Oil & Gas Field Pits Evaluation	Jul 25 2013	ftp://ftp.epa.gov/r8/pavilliondocs/OtherDocuments/WellAndFieldPitsEvaluationJuly2013/25July2013PavillionPitsReport4pmFinal.pdf
WOGCC P	avillion Field Well Integrity Review	Oct 2014	http://wogcc.state.wy.us/pavillionworkinggrp/PAVILLION_REPORT_1082014_Final_Report.pdf
WOGCC P	avillion Field Pit Review	Jun 2015	http://wogcc.state.wy.us/pavillionworkinggrp/PAVILLION_REPORT_1082014_Final_Report.pdf
WDEQ	Pavillion, Wyoming Area Domestic Water Wells Draft Final Report and Palatability Study	Dec 2015	http://deq.wyoming.gov/wqd/pavillion-investigation/

Table SI H2. Summary of analytical methods used and sources of data and associated information on quality control and assurance.

Parameters	Phase	Medi	Methods		Lab	Sources (links) of Analytical and Associated Information on Quality Assurance and Control ) accessed 9/1/2015)
		a				(mino) of Many item and Associated Antol mation on Quanty Associated and Control) accessed 5112015)
Major ions, alkalinity	I	W	EPA Methods 300.0 and 310.1	EPA R8	3	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase1/R8_Lab/85621LSR_Report_Alkalinity_Anions_DRO.pdf
	-  II	†-w	EPA Methods 300.0 and 310.1.	EPA R8	ļ	http://www2.epa.gov/sites/production/files/documents/PavillionAnalyticalResultsReport.pdf (data summary only)
	III	w	RSKSOPs 276v3 and 214v5. EPA Methods SW-846 6500, 350.1, and 353.2	EPA Ad	a	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/ORD GP Lab Analysis for Phase III/
	IV	w	RSKSOPs 276v3 and 214v5. EPA Methods SW-846 6500, 350.1, and 353.2	EPA Ad	a	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/ORD GP Lab TOC DIC Analysis Phase IV/ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/ORD GP Lab TOC DIC Analysis Phase IV/DICrawdata.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/ORD GP Lab TOC DIC Analysis Phase IV/EPAGP256rev. 1 SS%236030 6032 R.Wilkin Pavillion Groundwater.pdf
						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/ORD GP Lab TOC DIC Analysis Phase IV/NPDOC rawdat a.pdf
	\\ \v_{\text{v}}	-w	RSKSOPs 276v3 and 214v5. EPA Methods SW-846 6500, 350.1, and 353.2	EPA Ad	a	ftp://ftp.epa.gov/r8/pavilliondocs/phase5/PavillionSeptember2012Appendices.pdf (data summary only)
	V	w	EPA Methods 300.0, 310.1, 9056, 9060 US	GS TA		http://pubs.usgs.gov/ds/718/ (data summary only) ftp://ftp.epa.gov/r8/pavilliondocs/phase5/Appendix11_J28076-1Std_Tal_L4_Package_MiniFinalReport3.pdf ftp://ftp.epa.gov/r8/pavilliondocs/phase5/Appendix9_J28076-1_EPA_Std_Tal_L4_Package_MiniFinalReport.pdf
Dissolved Metals	I	W	EPA Methods 6010B, 6020, 7470A	EPA K		http://www2.epa.gov/sites/production/files/documents/Pavillion_GWInvestigationARRTextAndMaps.pdf (data summary only)
	I	w	EPA Methods 6010B, 6020, 7470A	EPA L		http://www2.epa.gov/sites/production/files/documents/Pavillion_GWInvestigationARRTextAndMaps.pdf (data summary only)
	II	w	EPA Methods 6010B, 6020, 7470A	EPA A4		http://www2.epa.gov/sites/production/files/documents/PavillionAnalyticalResultsReport.pdf (data summary only)
	III	W	RSKSOP 213v4 and 257v2, or 332V0 and EPA Methods 200.7 and 6020.	EPA S		ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Metals Analysis Phase III/ ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Metals Analysis Phase III/Shaw Metals Analysis Phase III/Shaw Metals Analysis Phase III/Shaw Metals Analysis Phase III/Shaw Metals Analysis Phase III/Shaw Metals Analysis Phase III-ICP Data/ICP Data 1 of 2 101110.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Metals Analysis Phase III/Shaw Metals Analysis Phase III-ICP Data/ICP Data 2 of 2 101110.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Metals Analysis Phase III/Shaw Metals Analysis Phase III-ICP Data/ICP Data 2 of 2 101110.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Metals Analysis Phase III/Shaw Metals Analysis Phase III-ICP Data/Pavillion ICP-MS Data.pdf
	IV	W	RSKSOP 213v4 and 257v2, or 332V0 and EPA Methods 200.7 and 6020.	EPA S		ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw Metals Phase IV/ ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw Metals Phase IV/7ME743SF ICP-MS 1of2.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw Metals Phase IV/7ME743SF ICP-MS 2of2.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw Metals Phase IV/7ME743SF ICP 051011 1of2.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw Metals Phase IV/7ME743SF ICP 051011 2of2.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw Metals Phase IV/7ME743SF ICP 051111 1of2.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw Metals Phase IV/7ME743SF ICP 051111 2of2.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw Metals Phase IV/7ME743SF ICP 051111 2of2.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw Metals Phase IV/7ME743SF ICP 051211.pdf
	V	W	RSKSOP 213v4 and 257v2, or 332V0 and EPA Methods 200.7 and 6020.	EPA S		ftp://ftp.epa.gov/r8/pavilliondocs/phase5/PavillionSeptember2012Appendices.pdf (data summary only)
	V	W	EPA Methods 6010B, 6020, 7470A	ЕРА С		ftp://ftp.epa.gov/r8/pavilliondocs/phase5/Appendix9_J28076-1_EPA_Std_Tal_L4_Package_MiniFinalReport.pdf ftp://ftp.epa.gov/r8/pavilliondocs/phase5/Appendix10_J28076-1Std_Tal_L4_Package_MiniFinalReport2.pdf ftp://ftp.epa.gov/r8/pavilliondocs/phase5/Appendix11_J28076-1Std_Tal_L4_Package_MiniFinalReport3.pdf
	V	W	EPA Methods 6010B, 6020, 7470A	USGS T	IA	http://pubs.usgs.gov/ds/718/ (data summary only) ftp://ftp.epa.gov/rs/pavilliondocs/phase5/Appendix10_J28076-1Std_Tal_L4_Package_MiniFinalReport2.pdf ftp://ftp.epa.gov/rs/pavilliondocs/phase5/Appendix11_J28076-1Std_Tal_L4_Package_MiniFinalReport3.pdf ftp://ftp.epa.gov/rs/pavilliondocs/phase5/Appendix9_J28076-1_EPA_Std_Tal_L4_Package_MiniFinalReport.pdf
Fixed Gases, C1-C4	I	W	ORGM-004	EPA R8	3	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase1/R8_Lab/85622Headspace8270.pdf
	II	†- <del>w</del>	ORGM-004	EPA R8	<u> </u>	http://www2.epa.gov/sites/production/files/documents/PavillionAnalyticalResultsReport.pdf (data summary only)

	III	[ w ]	RSKSOP-194v4, RSKSOP-175v5	EPA S	[	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw_Light_Hydrocarbon_and_Fixed_Gases_Phase_III-Calibration_Plots/
						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Light Hydrocarbons and Fixed Gases Phase III/
						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Light Hydrocarbon and Fixed Gases Phase III-
						Calibration Plots/calibration plots.pdf
						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Light Hydrocarbon and Fixed Gases Phase III-
						Calibration Plots/calibration table Micro 3000.pdf
						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Light Hydrocarbon and Fixed Gases Phase III-
						Calibration Plots/chromatograms and reports.pdf
						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Light Hydrocarbons and Fixed Gases Phase III/
						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Light Hydrocarbons and Fixed Gases Phase III/RSKS
						OP-194 4 Initial Calibration for Micro 3000.pdf
						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Light Hydrocarbons and Fixed Gases Phase III/RSKS
						OP-194 4 high Initial Calibration for Micro 3000.pdf
						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw Light Hydrocarbons and Fixed Gases Phase III/Refine
						ry Gas Initial Calibration for Micro 3000.pdf
	iv	. †	RSKSOP-194v4, RSKSOP-175v5	EPA S	·	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw Light Hydrocarbons and Fixed Gases Phase IV/
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						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw Light Hydrocarbons and Fixed Gases Phase IV/7OA7
						67SF ss%236030 6032Pavillion GC.pdf
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		. +	RSKSOP-175	USGS 7	Ι _Α	ftp://ftp.epa.gov/r8/pavilliondocs/phase5/Appendix9 J28076-1 EPA Std Tal L4 Package MiniFinalReport.pdf
C1-C4 Isotopes	III	W G Ga	s stripping and IRMS – No EPA	EPA I		ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/
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	IV	w	Gas stripping and IRMS – No EPA	EPA I		ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Isotech Gas Analysis Phase IV/
			Method			ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Isotech_Ground_Water_Analysis_Phase_IV/
	V	w	Gas stripping and IRMS – No EPA Method	EPA I		ftp://ftp.epa.gov/r8/pavilliondocs/phase5/PavillionSeptember2012Appendices.pdf (data summary only)
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						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw IRMS_Analysis for Phase III/Raw_Data-2.pdf
						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/Shaw IRMS Analysis for Phase III/Raw Data Summary Ta
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	II	w	EPA Contract Laboratory Program -	EPA A		http://www2.epa.gov/sites/production/files/documents/PavillionAnalyticalResultsReport.pdf (data summary only)
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						ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/R8LabDocumentation PhaseIII/SequenceNo0J18003.pdf
	IV	W	ORGM-501r1.1, EPA Methods SW-846	EPA R8	<b>,</b>	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/R8LabDocumentation PhaseIII/SequenceNo0J18003.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/R8LabDocumentation PhaseIV/Apr2011R8LabDataPkg SR11
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	III	w	ORGM-515r1.1 and EPA Methods 3520 and 8270D	EPA R8	3	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/R8LabDocumentation PhaseIII/Oct2010SVOCAnalysis-0J25006.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/R8LabDocumentation PhaseIII/Oct2010SVOCAnalysis- PavillionSpecificCompounds-0J27001.pdf
	II	PW	ORGM-515r1.1 and EPA Methods 3520 and 8270D	EPA R8	3	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase2/R8Lab/Jan20108VOCAnalysis- PavillionSpecificCompoundsFilterAndProductionWater-0B17001and0B26002.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase2/R8Lab/Jan20108VOCAnalysisProductionWater-0B19002.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase2/R8Lab/Jan20108VOCAnalysisFilter-0B19001.pdf
		W, S OI	and 8270D RGM-515r1.1 and EPA Methods 3520 and 8270D	EPA R8	3	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase1/R8_Lab/March2009SVOCAnalysis-9C23005.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase2/R8Lab/GCMS8270SemivolatilesW.O.1001002and1001003.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase2/R8Lab/Jan2010SVOCAnalysis-0C08003.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase2/R8Lab/Jan2010SVOCAnalysis-PavillionSpecificCompounds- 0C04002.pdf
SVOCs	V	W	EPA Methods 5030B and 8260B  ORGM-515r1.1 and EPA Methods 3520	USGS T EPA R8		http://pubs.usgs.gov/ds/718/ (data summary only) ftp://ftp.epa.gov/r8/pavilliondocs/phase5/Appendix6_280-28076-1_DataValidationReview.pdf ftp://ftp.epa.gov/r8/pavilliondocs/phase5/Appendix9_J28076-1_EPA_Std_Tal_L4_Package_MiniFinalReport.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase1/R8_Lab/85622Headspace8270.pdf
	v	- <del>w</del>	5035 and 8260B RSKSOP-259v1, EPA Methods SW-846 5021A and 8260B	EPA S		ftp://ftp.epa.gov/r8/pavilliondocs/phase5/PavillionSeptember2012Appendices.pdf (data summary only)
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	IV	W	RSKSOP-259v1, EPA Methods SW-846 5021A and 8260	EPA S		ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/R8LabDocumentation PhaseIV/Apr2011R8LabDataPkg Seque nceNo1D25001.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/R8LabDocumentation PhaseIV/Apr2011R8LabDataPkg Seque nceNo1D29001.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/R8LabDocumentation PhaseIV/April2011VOCAnalysis-1D29001.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw VOCs Phase IV/ ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw VOCs Phase IV/Report.pdf ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/Shaw VOCs Phase IV/Report.pdf

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		PavillionSpecificCompounds-1E18003.pdf
ORGM-515r1.1 and EPA Methods 3520	EPA R8	ftp://ftp.epa.gov/r8/pavilliondocs/phase5/PavillionSeptember2012Appendices.pdf (data summary only)
and 8270D		
EPA Methods 3520C and 8270C	USGS TA	ftp://ftp.epa.gov/r8/pavilliondocs/phase5/Appendix9_J28076-1_EPA_Std_Tal_L4_Package_MiniFinalReport.pdf
ORGM-508r1.0, EPA Methods 8015B	EPA R8	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase1/R8_Lab/85621LSR_Report_Alkalinity_Anions_DRO.pdf
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*	EPA R8	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase2/R8Lab/DROW.O.1001002and1001003and1001005.pdf
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	EPA R8	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/R8LabDocumentation_PhaseIII/SequenceNo0J12001.pdf
	EPA R8	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/R8LabDocumentation PhaseIII/PavillionNo2 LSR1010-
	EDADO	017.pdf fp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase4/R8LabDocumentation PhaseIV/Apr2011R8LabDataPkg Seque
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	EPA RS	ftp://ftp.epa.gov/r8/pavilliondocs/phase5/PavillionSeptember2012Appendices.pdf (data summary only)
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ORGM-506r1.0, EPA Method: 8015D	EPA R8	ftp://ftp.epa.gov/r8/pavilliondocs/RawLabData/Phase3/R8LabDocumentation_PhaseIII/SequenceNo0J06001.pdf
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Alkylphenols			D7458-09 and USGS Method O1433-01			
Acrylamide	V	W	Method in Development based on EPA	EPA LV		ftp://ftp.epa.gov/r8/pavilliondocs/phase5/PavillionSeptember2012Appendices.pdf (data summary only)
			Methods 8032A and 8316			
MBAS	V	W	EPA Method 425.1	EPA TA		ftp://ftp.epa.gov/r8/pavilliondocs/phase5/PavillionSeptember2012Appendices.pdf (data summary only)
	V	W	EPA Method 425.1	USGS T	A	ftp://ftp.epa.gov/r8/pavilliondocs/phase5/Appendix9 J28076-1 EPA Std Tal L4 Package MiniFinalReport.pdf
Methanol	V	W	EPA Method SW-846 8015M	EPA S		https://foiaonline.regulations.gov/foia/action/public/view/request?objectId=090004d2806a7021

#### Abbreviations

C1-C4 – methane, ethane, propane, and butane

VOCs – volatile organic compounds

SVOCs –semi-volatile organic compounds

LMWOAs - low molecular weight organic acids

MBAS -

GRO – gasoline range organic compounds

DRO – diesel range organic compounds

W-water

G - gas

S - solids

### Laboratories

A - ALS Laboratory Group, Salt Lake City, UT

A4 - A4 Scientific, The Woodlands, TX

Ada - EPA Office of Research and Development, Ada, OK

C - Chemtech

E - Energy Laboratories Inc., Billings, MT

I - Isotech Laboratories, Champaign, IL

K - KAP Laboratories, Vancouver, WA.

L - Liberty Analytical, Salt Lake City, UT

LV – EPA Office of Research and Development, Las Vegas, NV

R3 - EPA Region 3 Laboratory, Fort Meade, MD

R8 - EPA Region 8 Laboratory, Golden, CO.

S – Shaw Environmental, Ada, OK

TA - Test America, Denver, CO

Z - Zymax

### **Analytical Methods**

ORGM-501r1.1 EPA Region 8 Standard Operating Procedure used with EPA Method 8260 for VOC analysis

ORGM-506 r1.0 - EPA Region 8 Standard Operating Procedure used with EPA Method 8015 for GRO analysis

ORGM-508 r1.0 - EPA Region 8 standard operating procedure used with EPA Method 8015D for DRO analysis

ORGM-515 r1.1 – EPA Region 8 standard operating procedure used with EPA Methods 3520 and 8270D for SVOC analysis

RSKSOP-112v6 - EPA Standard Operating Procedure for Quantitative Analysis of Low Molecular Weight Acids in Aqueous Samples by HPLC

RSKSOP-175v5 - Sample Preparation and Calculations for Dissolved Gas Analysis in Water Samples Using a GC Headspace Equilibration Technique, 16 p.

RSKSOP-194v4 - Gas Analysis by Micro Gas Chromatographs (Agilent MIcro 3000), 13 p.

RSKSOP-213v4 - Standard operating procedure for operation of Perkin Elmer Optima 3300 DV ICP-OES, 21 p.

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RSKSOP-214v5 - Quality control procedures for general parameters analysis using Lachat Flow Injection analysis (FIA), 10 p.

RSKSOP-259v1 - Determination of volatile organic compounds (fuel oxygenates, aromatic and chlorinated hydrocarbons) in water using automated headspace gas chromatography/mass spectrometry TEKMAR 7000 HS-Varian 2100T GC/MS system-ION trap detector, 28 p.

RSKSOP-257v2 - Standard operating procedure for elemental analysis by ICP-MS, 16 p.

RSKSOP-299v1 – Determination of Volatile Organic Compounds (Fuel Oxygenates, Aromatic and Chlorinated Hydrocarbons) in Water Using Automated Headspace Gas Chromatography/Mass Spectrometry (Agilent 6890/5973 Quadruple GC/MS System), 25 p.

RSKSOP-276v3 - Determination of major anions in aqueous samples using capillary ion electrophoresis with indirect UV detection and Empower 2 software, 11 p.

RSKSOP-296v0 - Determination of hydrogen and oxygen isotope ratios in water samples using high temperature conversion elemental analyzer (TC/EA), a continuous flow unit, and an isotope ratio mass spectrometer (IRMS), 8 p.

RSKSOP-297v1 – Metals Speciation Determination by LC/ICP-MS, 21 p.

RSKSOP-298v1 - Arsenic Speciation Determination by LC/ICP-MS with Anion Suppression and NaOH Mobile Phase, 21 p.

RSKSOP-313v1 - Determination of R-123 using the H25-IR Infrared Refrigerant Gas Leak Detector, 12 p.

RSKSOP-314v1 - Determination of Fixed Gases using the GEM2000 and GEM2000 Plus Gas Analyzers & Extraction Monitors, 13 p.

RSKSOP-320v1 - Determination of Organic and Inorganic Vapors Using the TVA-1000B Toxic Vapor Analyzer, 18 p.

RSKSOP-330v0 - Determination of Various Fractions of Carbon in Aqueous Samples Using the Shimadzu TOC-VCPH Analyzer, 16 p.

EPA Method 200.7 - Determination of Metals and Trace Elements in Water and Wastes by Inductively Coupled Plasma-Atomic Spectrometry, Rev. 5, Jan 2001.

EPA Method 300.0 - Determination of Inorganic Anions by Ion Chromatography, Rev. 2.1, Aug. 1993.

EPA method 310.1 - Alkalinity (Titrimetric, pH 4.5), Rev. 1978.

EPA Method 350.1 - Determination of Ammonia Nitrogen by Semi-Automated Colorimetry, Rev. 2, Aug. 1993.

U.S. EPA Method 5021A - Volatile Organic Compounds in Various Sample Matrices Using Equilibrium Headspace Analysis, Rev. 1, June 2003.

U.S. EPA Method 6020 - Inductively Coupled Plasma-Mass Spectrometry, Rev. 1, Feb. 2007.

U.S. EPA Method 6500 - Dissolved Inorganic Anions in Aqueous Matrices by Capillary Electrophoresis, Rev. 0, Feb. 2007.

U.S. EPA Method 8260C - Volatile Organic Compounds by Gas Chromatography/Mass Spectrometry (GC/MS), Rev. 3, Aug. 2006.

EPA Method 8015B - Determination of Nonhalogenated Organics Using GC/FID, Rev. 2, Dec. 1996.

U.S. EPA Method 8015D - Nonhalogenated Organics Using GC/FID, Rev. 4, May 2003.

U.S. EPA Method 8270D - Determination of Semivolatile Organic Compounds by Gas Chromatography/Mass Spectrometry (GC/MS), Rev. 4, Feb. 2007.

U.S. EPA Method 8000C - Determinative Chromatographic Separations, Rev. 3, Mar. 2003.

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